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W.Va. Geological & Economic Survey

Report of Petrologic Characterization of Jackson 1369
(Columbia Gas Transmission Co. Well #11940)

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ABSTRACT

Fifty samples from WV Jac 1369 (Columbia Gas Transmission Corp. Well #11940) were studied in detail in order to characterize the Devonian shale in terms of its petrology. Mineralogical components from X-ray diffractograms, thin section point counts, petrophysical parameters of density and porosity, log-derived values of bulk density (g/cc) and gamma ray deflection (API units), loss on ignition data between 100°C-550°C and 550°C-1000°C, and total sulfur (LECO method) are graphically displayed on computer-drawn strip logs.

For correlation analyses, all samples exclusive of those which are concretions were considered. Statistical treatment was done on the basis of the entire interval and on subdivision into lithotypes. Major differences between lithotypes are in bulk density, sulfur, grain density and organic matter parameters. Additionally, a preliminary statistical comparison of this well with the previously characterized Linc 1637 (Columbia Gas Transmission Co. Well #20403) was undertaken and revealed significant regional differences in certain mineralogical and physical parameters such as porosity, log density, bulk density, sulfur, and quartz.

A classification system for lithotypes observed in the lower part of the Huron Member based on fabric elements is provided with accompanying representative plates. This classification has proven to be applicable to all Devonian shales we have encountered. A preliminary interpretation of depositional environment is included and integrated into previous models. The lower part of the Huron Member is interpreted as being deposited in less anoxic and perhaps deeper water in Jackson Co. relative to Lincoln County. Specific petrographic frac-

ture types are described from the core and related in conjunction with lithotypes in tentatively explaining the high final open flow of this well. Results of the study are summarized in the brief text and are followed by conclusions and appendices of data.

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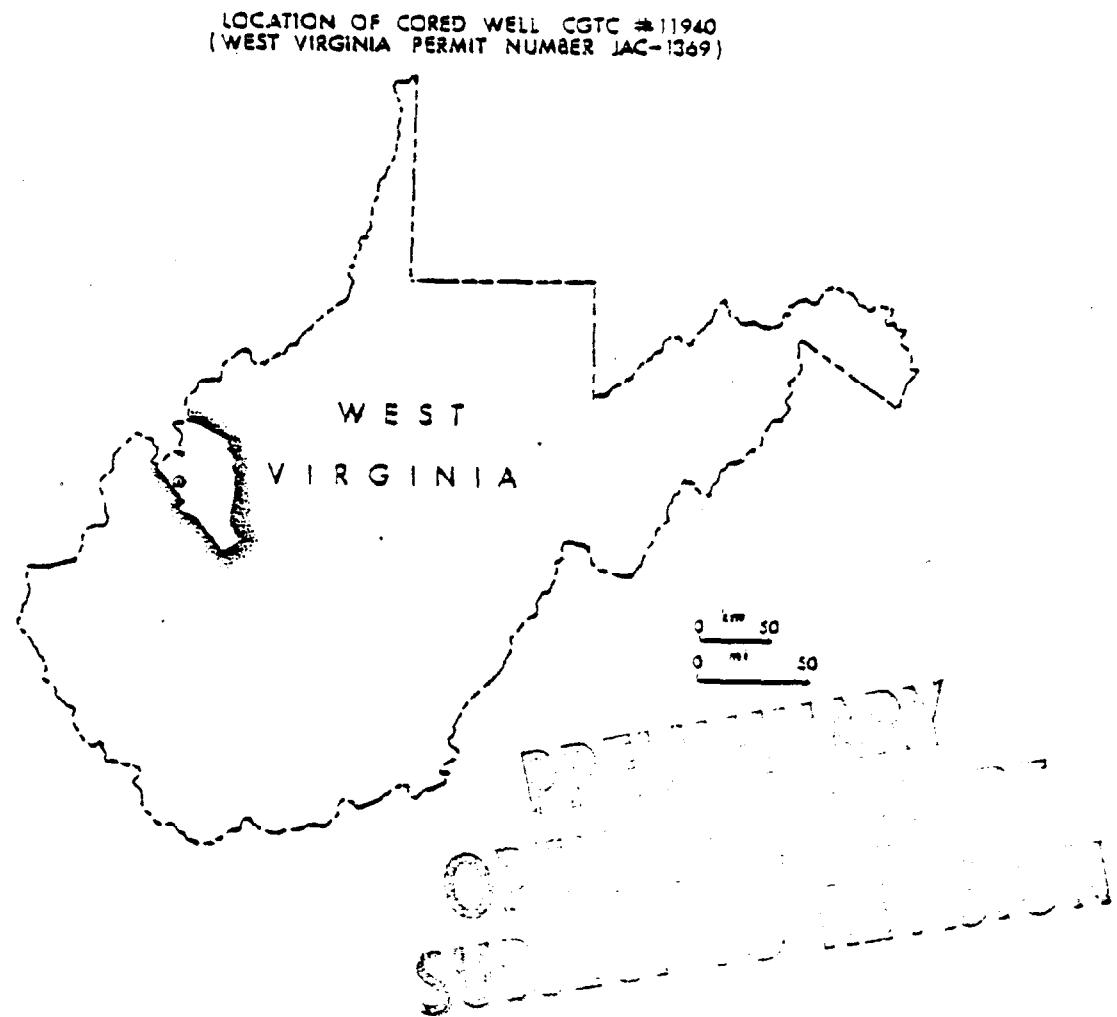


Figure 1: Location of subject well in Jackson County, West Virginia.

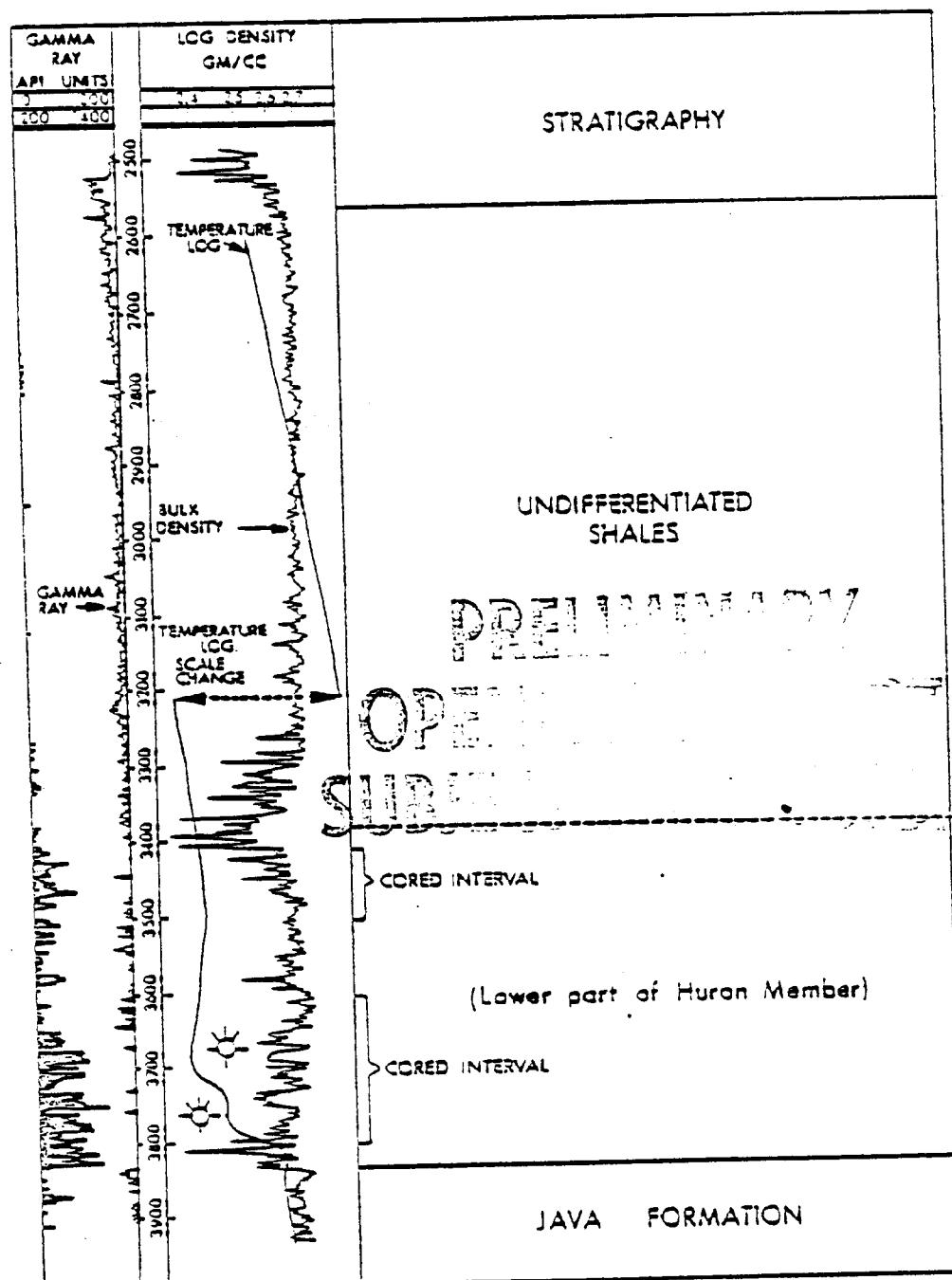


Figure 2: Gamma ray-density-temperature log profile and stratigraphic division of Jac 1369 well, Jackson County, West Virginia.

Characterization of Overall Core
Density, Porosity, and Log Parameters

Five types of density were derived for each sample from the subject well:

- 1) bulk density - measured by immersion of krylon-coated sawed blocks of whole - sample in Kerosene.
- 2) matrix density - the density of the ground whole - sample as measured by the vacuum-crucible method described by Nuhfer (1978).
- 3) grain density - the density of the crystalline component of the shales as determined from X-ray mineralogy and established mineral density values tabulated in a number of reference sources. Note that this density excludes organic matter and any amorphous (to X-ray) mineraloids.
- 4) material balance density - a density computed from the whole rock composition as established by estimates of organic matter from loss on ignition between 100°C and 550°C; from non-pyritic mineralogy as determined by X-ray diffraction and pyritic mineralogy as back-calculated from total sulfur (LECO) analyses. This was used only as a check against matrix density to locate samples with an unacceptable disparity between a directly measured matrix density and a density calculated from composition. Material balance density is not used as a correlation variable.
- 5) log density - the density taken from the bulk density log at the log depth subjectively selected as corresponding to the sample depth taken from the core.

Porosity was calculated from bulk and matrix density. Precision

of bulk and matrix density is about ± 0.01 g/cc. This yields a corresponding porosity precision of about $\pm 0.5\%$.

Discussion of Statistical Correlations from Overall Core

Bulk Density - Significant negative correlations exist between bulk density and loss on ignition 100-500°C, porosity and gamma ray log response. The correlation with loss on ignition 100-500°C reflects the predictable effect of low density organic matter on bulk density. Concentration of U and Th in organic matter is reflected in the negative correlation (-.59) with gamma ray log response. The correlation with porosity (-.37) likely reflects the lower mean porosity of the higher density (lower organic content) non-banded shales. A very high positive correlation with matrix density (+.93) is explained by the low porosity of all shale lithotypes and documents good precision in measurement of densities in the laboratory.

Matrix Density - Correlations of matrix density mimic those of bulk density because of the low porosity in the shales and are discussed above.

Grain Density - Significant negative correlations exist with thin section derived quartz-feldspar (-.42) and with kaolinite (-.42). These correlations are produced by relatively low grain density argillaceous siltstones that are included in a data matrix of sufficiently low sample number as to be greatly effected by 1 or 2 outlying points. Quartz-feldspar and kaolinite are associated probably due to the diagenetic alteration of feldspar to kaolinite. Grain density shows positive correlations with loss on ignition 100-550°C (+.58), loss on ignition 550-1000°C (+.51), total sulfur (+.52) and pyrite (+.36). The correlations with loss on ignition 550-1000°C; total sulfur, and pyrite reflect the expected increase

in grain density with an increase in pyrite content. Loss on ignition 100-550°C shows a positive correlation (+.51) with pyrite which explains the positive correlation between loss on ignition 100-550°C (organic content) and increasing grain density.

Porosity - A significant negative correlation (-.31) exists with bulk density. In material of constant matrix density, bulk density is theoretically inversely linearly related to porosity. The low correlation coefficient here is attributed to non-constant matrix density and uniformly low porosity values which are individually significantly affected by the error in measurement of even the very precise methodology used by us for porosity determinations. Additionally, the higher bulk density non-banded shales have a lower mean porosity than the lower bulk density finely laminated shales.

Log Density - Weak negative correlations with loss-on ignition 100-550°C (-.52), total sulfur (-.43), and pyrite (-.40) are produced by low density organic matter and associated pyrite. Positive correlations with bulk density (+.44) and matrix density (+.58) are surprisingly good considering that the sample depth could not be corrected to the geophysical log depth. The degree of correlation among these parameters is lower than would normally be expected. This is because core samples are point samples which are not strictly comparable to log data acquired as a function of a moving average of instrument response. Considering a gross sample size of two or three feet of borehole, a good approximation of bulk density can be derived from density log values.

Gamma Ray Log Response - Significant negative correlations between this variable and bulk density (-.59), matrix density, (-.56), and log density (-.49) are predictable as a consequence of the well

documented association of higher radioactivity and organic matter in black shales. As with the density log, the moving average response limits direct correspondence with selected point samples.

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Discussion of Statistical Correlations from Overall Core
Mineralogic and Loss on Ignition Parameters

Many variables showed significant positive and negative correlations with one another, but the relatively small sample size of the population coupled with the problem of imprecise X-ray data generated from some minerals present in low concentration produced many fortuitous correlations due to one or two outlying points. As such, bivariate scatter plots were used to determine if the trends indicated by the correlation coefficients were indeed characteristic of the lower part of the Huron Member. The following correlations although statistically significant were found to be produced by one to two outlying points and should not be taken as indicative of the lower Huron.

Quartz-feldspar (thin-section) - Ankerite	+.76
Quartz-feldspar (thin-section) - Hemi-hydrate	.75
Orthoclase - 14 A° clay	-.50
Orthoclase - Coquimbite	+.55
Gypsum - Coquimbite	+.56
Kaolinite - Illite	-.52
Ankerite - Hemi-hydrate	+.95
Plagioclase - Illite	-.49

The following correlations are interpreted from scatter plots as representative of general trends in the lower part of the Huron Member.

Quartz-feldspar (thin-section) - Illite	-.62
Quartz-feldspar (thin-section) - Kaolinite	+.68
Quartz - Illite	-.91

The correlation of thin section quartz-feldspar with illite reflects dilution of one mineral by another. Diagenetically produced kaolinite from feldspar possibly explains the kaolinite association. The strong negative correlation of K-ray quartz and illite is produced by dilution.

Loss on ignition 100-550°C - Pyrite	+ .51
Loss on ignition 550-1000°C - Pyrite	+ .50
Loss on ignition 100-550°C - Sulfur	+ .54
Loss on ignition 550-1000°C - Sulfur	+ .60

The association of loss on ignition 100-550°C with pyrite and total sulfur reflects the high pyrite content of organic rich shales within the lower part of the Huron Member. Pyrite and total sulfur correlate with loss on ignition 550-1000°C as expected, but the loss of carbonates on heating probably limits the correlation.

Characterization of Lithotypes in
Devonian Shale of Jackson 1369

The lower part of the Huron Member in Jackson 1369 contains many shale lithotypes and is not overwhelmingly dominated by any one type. In this respect, the lower Huron of this well differs from that of the lower Huron described as dominated by a single lithotype in our previous report on Linc 1637 (Nuhfer, Vinopal, Hohn, et.al., 1978). In Jackson 1369, correlation of physical and compositional variables of the stratigraphic unit as a whole tends to mask any significant correlations within a specific lithotype. Correlations by lithotype are listed in Appendix C. A shale classification based on fabric elements was first used in characterizing the Lincoln 1637 well (Nuhfer and Vinopal, 1978; Nuhfer, Vinopal, Hohn and others, 1978) and later modified in Nuhfer and Vinopal (1979). Five types of shale are defined: 1) Non-banded shale is generally devoid of preferred orientation of any visible fabric elements except for the orientation of clay laths due to compaction. Some samples show occasional thin laminae defined by varying silt content, but most appear massive in thin section and radiographs. This lithotype is usually extensively burrowed, commonly contains nodular pyrite and is not associated with gas productivity. 2) Sharply banded shale imparts a coarse linear fabric produced by alternate light and dark bands up to several cm in thickness. Boundaries between bands are sharp. In core sized samples, the bands extend across the core. Pyritized spores, large frambooidal aggregates, pyrite-filled "synaeresis cracks" and occasional nodules are present. This shale type is not associated with gas production. 3) Lenticularly

Laminated shale exhibits a linear fabric produced by alternate light and dark laminae up to a centimeter in thickness. However, the boundaries between laminae are often undulatory. Disturbation is common at laminae boundaries. In core sized samples, the laminae are more discontinuous and thicker compared to the thinly laminated shale type. This shale type may be associated with gas production depending on its organic content and lateral continuity of porous pyrite bodies. 4) Thinly laminated shale consists of uniformly thin, discontinuous laminae caused by wispy concentrations of silt, pyritic matter and organic matter. Most laminae are less than 2 mm in thickness. Laminae boundaries are even, sharp and rarely undulatory. Pyrite occurs ~~mainly~~ as very fine particles and fram-boids. Traction features and burrows are rare. This shale type is associated with gas production, gas shows, and is present in the productive lower portion of the Huron Member in Jackson County, 5). Combinations of the above types, where two or more of the above types occur within a small (hand specimen-sized) portion of the vertical profile. Additionally, two non-shale lithotypes are present in minor amounts in the lower part of the Huron Member in Jackson Co., crossbedded argillaceous siltstones and concretions.

Thinly laminated shale - Within the cored portion of the lower part of the Huron Member, thinly laminated shales comprise approximately one third of the samples collected. Thinly laminated shale is analytically distinguishable from non-banded and sharply banded shales by its higher LOI organic content. Mean organic content (5.8%) is slightly higher than that of lenticularly laminated shale (4.7%). Mean total sulfur and pyrite content is not significantly different from that of the lenticularly laminated shales, but is

higher than that of the non-banded shales. Mean matrix density and bulk density is lower than that of non-banded shale reflecting the higher organic content. However, the mean grain density is not significantly different from those of the other lithotypes indicating that mineralogic differences are not great. Mean porosity (1.3%) is not different from that of the lenticularly laminated shales (1.5%) and non-banded shales (1.0%). Log parameters of bulk density and gamma ray response do not differentiate finely laminated core samples from the other lithotypes in this well. Many of the correlations shown in Appendix C with magnitudes .50-.65 are not real, produced by the small sample size and the fact that many of the data values for minor components are zero. An example of this effect is shown by the correlation between coquimbite and illite (-.59); many of the samples have a coquimbite value of zero and only a few points induce the correlation. Truly significant correlations generally appear between sample depth, LOI (organic content) and density parameters. Loss on ignition 100-550°C shows predictable negative correlations with bulk density (-.81) with sample depth probably reflecting the correlation between LOI 100-550°C and sample depth (+.65). The thinly laminated shales in the lower portion of the core contain more organic matter.

Lenticularly laminated shales - Within the cored interval, lenticularly laminated shales comprise about one third of the samples collected and appear to be relatively more abundant in the lower portions of the core. The means of LOI organic content and sulfur fall between those of the thinly laminated and non-banded shale types. Several of the lenticularly laminated shales have an organic content equal to that of the finely-laminated shales. Most significant correlations involve LOI organic content, sample depth,

and density parameters. Density log values show no correlation with sample derived bulk density. Thin section quartz (-.64) and 14 A° clay (-.55) show negative correlations with sample depth which reflect dilution by an increasing illite content (+.68) with sample depth. LOI organic content has a moderate positive correlation (+.72) with grain density, which reflects the association between LOI organic content and high density pyrite (+.73). The negative correlation (-.59) between bulk density and porosity is not real and is due to variable matrix density. The correlations of bulk density with dolomite (+.71), gamma ray response with orthoclase (-.55) and coquimbite with pyrite (-.78), calcite ~~(+.96)~~, dolomite ~~(+.81)~~, grain density (-.80) and hemihydrate ~~(-.82)~~ are not representative and represent correlations induced by ~~a few~~ data points.

Non-banded shale - Non-banded shales comprise approximately one fourth of the samples collected and appear to be relatively more abundant in the upper and basal portions of the core. This lithotype has the lowest mean sulfur, pyrite, porosity and LOI organic content values. Correspondingly, mean bulk density and matrix density are higher than other shale lithotypes due to the lower organic content. Log characteristics (bulk density, gamma ray response) do not significantly differ from those of other lithotypes. Log density shows no correlation with sample derived bulk density, possibly because of a small data base. Pyrite shows a strong correlation (+.85) with total sulfur which is much higher than that of the other lithotypes and possibly indicates the presence of non-crystalline iron sulfides in the other lithotypes. The strong negative correlation (-.90) between quartz and illite, the two major mineral components, reflects dilution of one mineral by another.

The correlations of illite with dolomite (-.83) and bulk density with coquimbite (+.76), and matrix density with coquimbite (+.66) represent the biasing effect of one or two points on an overall trend of no correlation. Porosity shows a moderate correlation (+.61) with matrix density which is in agreement with the association of porosity and pyrite in Devonian shales described by Nuhfer and Vinopal, (1978).

Siltstones - Crossbedded siltstones with low mean porosity (1.48%) make up a minor portion of the core. The combination of appreciable argillaceous matrix and carbonate cement limits porosity.

Sharply banded shale - Sharply banded shales are present in small amounts, but the population size is inadequate for statistical treatment.

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Evaluation of Analytical Methodology

Bulk density - Precision of bulk density is better than 0.005 g/cc. It is reported to two decimal places, both being valid and reliable.

Matrix density - Precision of matrix density is better than 0.01 g/cc. Several methods of matrix determination were examined, but the vacuum crucible method devised by Nuhfer was as reproducible as any ASTM method examined and was much faster. Rock powders dried at room temperature were utilized. It was proven by examination of sample on individual thermograms that ground shales dried at high temperatures (30-100°C), even at atmospheric pressure, lose hydrocarbon material, a factor which will result in erroneously high porosity being calculated from density measurements. Comparison with material balance density shows only a few variations which might be caused by erroneous data.

Porosity - Precision is better than 0.5%; calculated from bulk and matrix density. The low range of porosity values available generally prevents linear correlations from being established with any other variables.

Loss on Ignition - Measured on a high precision (± 0.001 g) balance on samples at least 2 g in weight. Precision appears to be $\pm 5\%$ per determination, with variations being caused by sample inhomogeneity and non-uniform heating of the muffle furnace. Organic matter is approximated by LOI between 100° & 550°C, a second LOI from 550-1000°C reflects loss of CO₂ from carbonates, some S from sulfides, and some tightly bound waters in clay minerals.

X-ray diffraction mineralogy - Precision estimated as $\pm 10\%$ per determination on mineralogy $> 10\%$ in total concentration; $\pm 50\%$ on minerals present in concentration between $5\%-10\%$ and as much as $\pm 100\%$ on low concentration materials. At this time, uncertainty with respect to stoichiometric composition, amounts of any amorphous mineralloids and further lack of information with respect to effects of matrix differences (arising from compositional changes between thinly laminated lithotypes at one end, and non-banded lithotypes at the other) prevent one from making complete estimates of the accuracy of determination of each mineral. Comparisons of X-ray diffraction data with preliminary geochemical data and of X-ray diffraction-based material balance density with matrix density are still in progress.

Total Sulfur - Precision is apparently $\pm 15\%$ per determination from analyses of ground sample

Thin Section Point Counts - As discussed in Nuhfer, Vinopal and Hohn (1978), point counting of shales appears imprecise relative to estimating amounts of mineralogic and organic components in Devonian Shales. The percent of silt, assumed to be proportional to the amount of thin section quartz-feldspar, is useful in making sedimentologic interpretations and was determined for each sample. Additionally, thin section petrography was used extensively in fabric analysis of shale lithotypes and in examining crystal textures in filled fractures. Reproducability depends on consistence of microscopist. It is advisable to have only one microscopist do all of the point counts for a single well in order to yield the best between-sample comparisons.

Sample Selection - Samples must be selected and carefully prepared so that truly equivalent rock material is compared on all

tests. This was accomplished by vertical slabbing of material from the thin-section blank for petrophysical, mineralogical, and geochemical analyses. The necessity of adhering to a scheme to produce equivalent samples cannot be overemphasized. It is imperative that only a skilled, conscientious technician be entrusted with responsibility for initial subsampling. Samples which yielded apparently anomalous results were run in replicate. Where replications reconfirmed the anomalous values, the data were retained. The chance, however, still exists in these cases that an abrupt lateral variation caused inconsistent materials to be compared, producing anomalous values.

SUBSAMPLES FOR ANALYSIS

Summary and Interpretation

The 50 samples taken from the 297' core of Jac 1369 have been classified into six lithotypes based on fabric elements as seen in radiographs and negative prints (5x) of thin sections. Non-shale lithotypes; siltstones and concretions, are of minor abundance in the core. The four shale types are:

- 1) Thinly laminated
- 2) Lenticularly laminated
- 3) Sharply banded
- 4) Non-banded

The numerical order from 1 (thinly laminated) through 4 (non-banded) is a generally valid progressive order which reflects composition, with respect to decreasing organic matter and decreasing pyritic matter. This order also reflects a trend from highly ordered fabric in the finely laminated lithotype towards a more random fabric in the non-banded type. A cross section through the Cottageville Field in Jackson Co. (Patchen, 1977) shows that major gas pays are associated with the higher radioactive upper and basal portions of the lower Huron interval which contain relatively more organic rich finely laminated and lenticularly laminated shale than bounding stratigraphic zones. Because the lateral continuity is greatest in the thinly laminated lithotype, this fabric may favor lateral conduction of gas.

The subject well (Jac 1369) had a very high final open flow of 1007 MCF/day and is located at the southwestern margin of a linear trend of high natural open flow wells (Nuckols, 1978). This linear trend has been interpreted by Sundheimer (1978) as associated with

underlying basement faulting associated with the Rome Trough. Fractures seen in the partial core of 1369 appear to be a factor in establishing high productivity. However, blanket application of the term "fracture porosity" without considering the degree of permeability enhancement and porosity induced by specific petrographic fracture types creates an oversimplified model of the shale as a reservoir.

Current theories of the role of fractures in shale gas production ascribe large volumes of free gas to megoscopic and microscopic fracture systems in the shale (Science Applications Inc., 1977). Characterization of WV 1637 (Lincoln Co.) (Nuhfer, Vinopal, Hohn, et. al., 1978) failed to find any such extensive system of microfractures in the productive lower Huron ~~and Rhinestreet~~ intervals in that well. A large number of samples were examined by X-radiography and optical and scanning electron microscopy in both wells. No microfracture system was observed in the highly productive WV 1369 well described in this report. Additionally, the mean porosity of the lower portion of the Huron Member and the finely laminated lithotypes in the lower Huron is significantly lower in the Jac 1369 well than in the Linc 1637 well. If any microfracture system capable of contributing significantly to rock porosity was present in the highly productive Jac 1369, it should be reflected in higher porosity values. Permeability tests by Core Laboratories did not show permeability values for selected samples from Jac 1369 to be significantly different from shale wells characterized by lower productivity.

In contrast to any postulated system of microfractures, we feel that gas moves out of the matrix to the wellbore and to any connecting permeability enhancing fractures by diffusion through the finely

laminated and lenticularly laminated shale. Productivity in these lithotypes is favored by richer organic content, which enhances sorption capacity, and lateral continuity of fabric which favors lateral outgassing of the rock. Free gas in megascopic fractures connected to the wellbore has been commonly invoked to explain the initial years of high gas production from some shale wells. No worker, however, has proven the existence of a fracture system of sufficient volume to account for such long term production.

Schettler (1977, 1978) postulates such fractures may be depleted in shorter periods of time (perhaps in hours) and that gas diffusion from the shale matrix contributes almost exclusively to total gas production. The Jac 1369 well had an initial test of 4700 MCF but quickly blew down to a final open flow of 1007 MCF. This observation probably represents the rapid depletion of free gas from the megascopic fractures. Volume of fracture pore space should be estimated from measurements made on large numbers of actual core samples, and not carelessly invoked without further supporting data to explain long-term "free gas" production.

In the subject core, several petrographic fracture types were noted and are tentatively classified in terms of possible permeability and porosity enhancing characteristics. Where the temperature log indicated gas influx from the lower part of the Huron Member, fractures were noted in core samples that had prominent coarse hackles creating a rough surface. Slight movement along the uneven fracture surface created numerous "voids" and "vugs" that are only partially mineralized. This type of fracture was observed in samples from 3720 to 3739 feet. Other examples may have been present further down the core, but the core had been badly picked over and disarranged prior to sampling by us. These fractures are interpreted

as contributing significantly to permeability. Relatively smooth sub-vertical fractures that were infilled by carbonates were observed in this same depth interval. These fractures probably do represent an increase in permeability over that of the shale matrix, but appear to have low to moderate intercrystalline porosity. Between two such parallel smooth fractures spaced 3 cm apart, partially open cross fractures were occasionally observed. These crossfractures are not propped open by partial mineralization, but retain some porosity and a high degree of permeability as a consequence of surface roughness and movement. Near the bottom of the core at 3789 feet, horizontal mineral filled fractures were noted. These fractures are tightly cemented by large dolomite crystals that have few intercrystalline boundaries and contacts. As such, the porosity of these fractures is quite low. Permeability may still be higher than that of the shale matrix because of a greater ease of diffusion along the interfaces of the coarse crystals. Additional investigations on the nature of fracture mineralization and surface features of fractures observed in Devonian shale cores and outcrops is currently in progress.

Environments of Deposition

A general depositional model for the Devonian shales developed from vertical profile analysis of the most complete stratigraphic sequence available in a core (Lincoln - 1637) is presented in Nuhfer and Vinopal (1979). The lower part of the Huron Member in that well is interpreted as a nearshore shallow-marine shelf environment. In Line 1637, dominance of the thinly laminated lithotype, the lack of traction features and the lack of borrowing suggest a quiet anoxic environment. The lower part of the Huron Member in Jac 1369 shows a different frequency of lithotypes than that noted in the Linc 1637 core. More non-banded and lenticularly laminated shale is present in Jac 1369. Additionally, the mean quartz content of the lower Huron is lower in Jackson County. This difference in quartz content is also present in the thinly laminated lithotype. The greater relative abundance of lenticularly laminated shales and non-banded shales coupled with the lower total quartz content is interpreted as indicating an environment further from the source area in less anoxic and perhaps deeper waters for the lower Huron in Jackson County. In a deeper-water shelf environment, conditions that produce stratification and restriction of circulation, would be more frequently disrupted by the effect of impinging regional basin currents. Perhaps eustatic, climatic, or tectonic changes affected basinal circulation allowing stratification to exist for moderate periods of time resulting in bundles of finely laminated shale in the upper and lower portions of the lower part of the Huron Member in Jackson County. The destruction of stratified waters on the shelf would increase bottom circulation permitting

inhabitation by burrowing organisms and producing non-banded and lenticularly laminated shales. The lower portion of Huron Member correlates with turbidite sands to the east. Some of the sediment in the non-banded and sharply banded shales in Jac 1369 may be the distal pulses of fine silt and clay carried in by waning turbidity currents. The distance from the postulated eastern turbidite sand accumulation to Jackson County is approximately 75 miles, which is not an unreasonable distance for turbidites to move fine grained material.

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Conclusions and Recommendations

- 1) Within a specific stratigraphic unit, many varied shale lithotypes can be present with widely differing organic matter contents and fabric elements. Characterization of a stratigraphic interval should be presented in terms of specific rock lithotypes.
- 2) Comparison of depth unconnected core samples with geophysical logs indicates that point samples of different lithotypes cannot commonly be correlated to significantly different log response. As such, cable tool or air rotary samples selected for analysis from a stratigraphic unit must be carefully evaluated before interpreted as indicating significant interwell differences. Future well cores should be logged with a surface scintillometer in order to make comparison between log data and sample data more objective.
- 3) Different petrographic fracture types exist, which influence permeability and porosity to varying extents. In tentative order of permeability enhancing characteristics they are: 1) coarse, hackly, partially mineralized, vertical fractures, 2) partially mineralized cross fractures between two vertical fractures, 3) tightly mineralized sub-vertical to vertical fractures, 4) tightly mineralized horizontal fractures. Further research on the physical properties and origin of specific petrographic fracture types is in progress to order to integrate them into a reservoir model.
- 4) The highly productive Jac 1369 well is interpreted in terms of a favorable lithotype combined with a specific petrographic fracture type (coarse, hackly, partially mineralized fractures) that enhances permeability. An additional core should be taken in

the high producing zone of the Cottageville Field to determine the extent of favorable fracture types in organic rich shales below the lower Huron.

5) Statistical relationships between analyzed variables are summarized in the discussion and in the appendices. However, in general, organic content and pyritic matter are the primary factors which cause variability in the shales. Refer to Nuhfer, Vinopal, Hohn, et. al., (1978) for additional conclusions and recommendations from the characterization of Line 1637.

6) The lower part of the Huron Member in Jackson Co. shows significant differences when compared [to the same unit] in Lincoln County. Specifically less quartz, pyrite and organic matter is present in the lower portion of the Huron Member in Jackson County. Mean porosity is lower. Mean ~~bulk density~~ and log density are higher due to the overall lower organic content. These differences reflect the greater diversity (more non-banded and lenticularly laminated shales) of lithotypes present in Jackson County. The difference in lithotype abundance is due to different depositional environments with the lower portion of Huron Member interpreted as being deposited in less anoxic and perhaps deeper water in Jackson County.

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Key to Abbreviations in Appendices

SAMPLE - sample number, corrected depth in feet

LOSIG 100 - weight % loss on ignition, 100-550°C

LOSIG 500 - weight % loss on ignition, 550-1000°C

SULFUR - total weight % sulfur from LECO method

STRAT - this is simply a numerical designation (3) representing the lower Huron interval defined in the well.

BULKDEN - bulk density (g/cc) measured ~~on core sample~~

MATRXDEN - matrix density (g/cc) ~~measured on core sample~~

LOGDEN - bulk density (g/cc) ~~from density log~~

POROSITY - percent porosity ~~of samples~~ from matrix and bulk density measurements

GAMMA - API units from gamma ray log

QUARTZ - percent quartz-feldspar (silt) measured in thin section

EXP - relative amount of 14°A clay mineral by X-ray diffraction

ILL -	"	"	"	illite	"	"
-------	---	---	---	--------	---	---

COQ -	"	"	"	coquimbite	"	"
-------	---	---	---	------------	---	---

KAC -	"	"	"	kaolinite	"	"
-------	---	---	---	-----------	---	---

HEM -	"	"	"	hemi-hydrate	"	"
-------	---	---	---	--------------	---	---

ANH -	"	"	"	anhydrite	"	"
-------	---	---	---	-----------	---	---

SZM -	"	"	"	szomolnokite	"	"
-------	---	---	---	--------------	---	---

QTZ -	"	"	"	quartz	"	"
-------	---	---	---	--------	---	---

PYR -	"	"	"	pyrite	"	"
-------	---	---	---	--------	---	---

CAL -	"	"	"	calcite	"	"
-------	---	---	---	---------	---	---

DOL -	"	"	"	dolomite	"	"
-------	---	---	---	----------	---	---

ORT -	"	"	"	orthoclase	"	"
-------	---	---	---	------------	---	---

PLA -	"	"	"	plagioclase	"	"
-------	---	---	---	-------------	---	---

SID - relative amount of 14⁰A siderite by X-ray diffraction

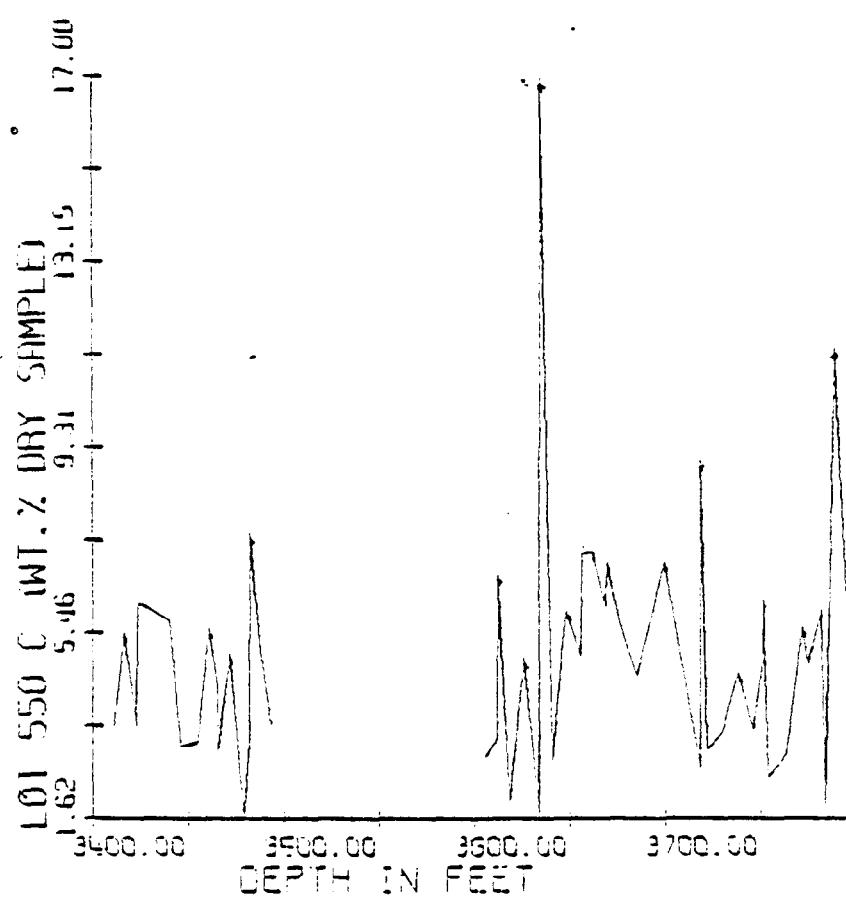
ANK - " " " ankerite " "

GRDEN - computed grain density (g/cc) of sample using compositional
percentages

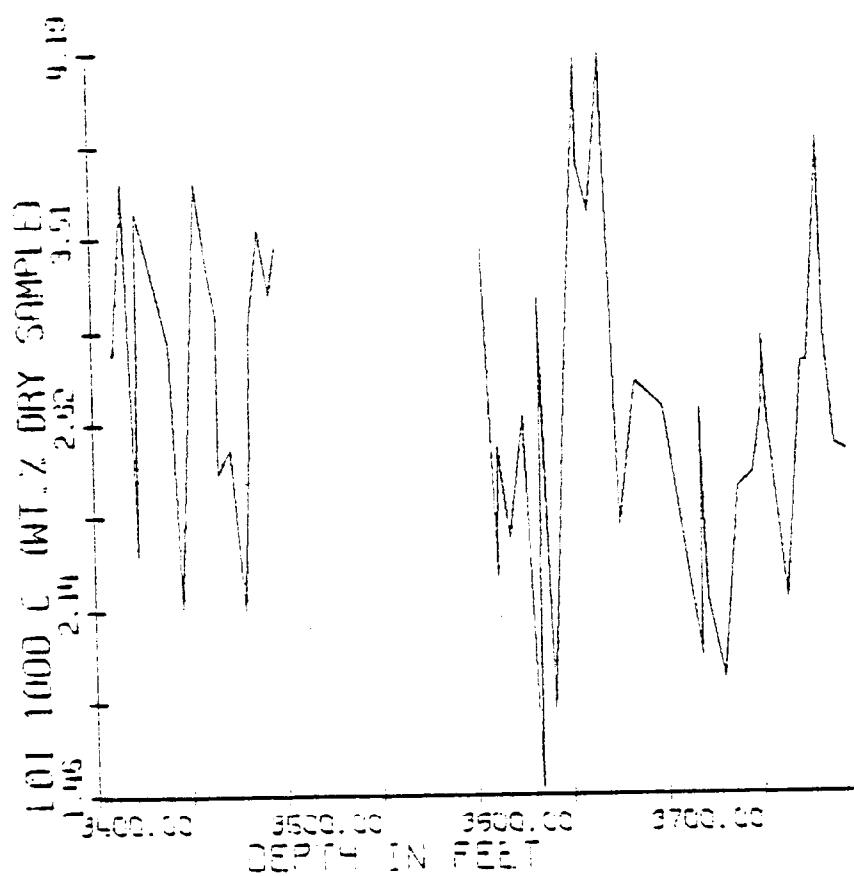
PRELIMINARY
OPEN
SUBJEC

PRELIMINARY
OCTOBER 1970
SUBMISSION
APPENDIX A
STRIP LOGS OF PARAMETERS

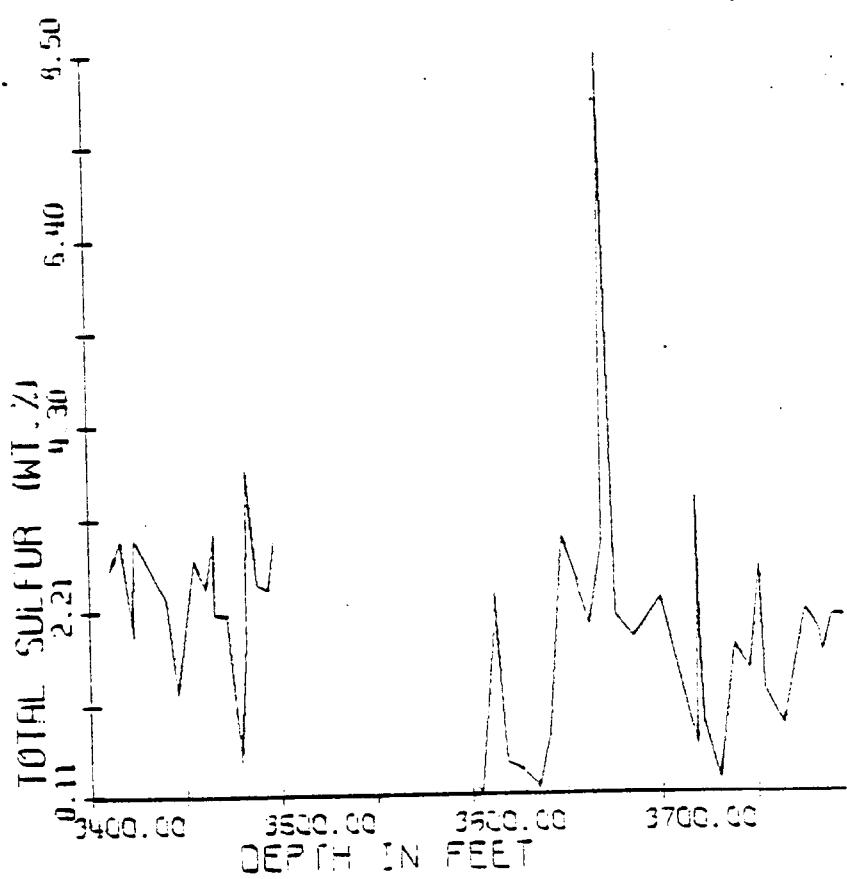
PRELIMINARY
OPEN
SUB

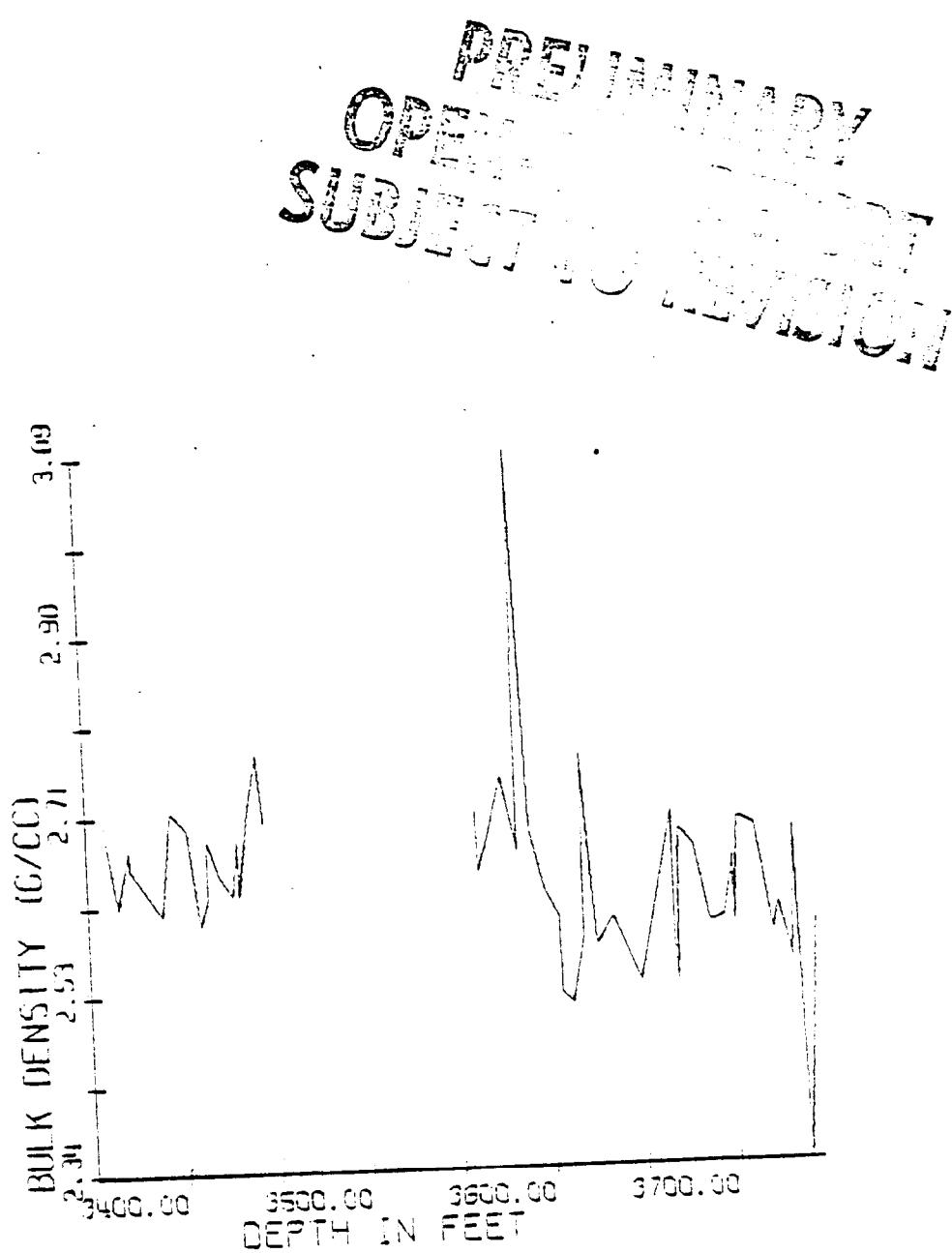


Supplementary
Section

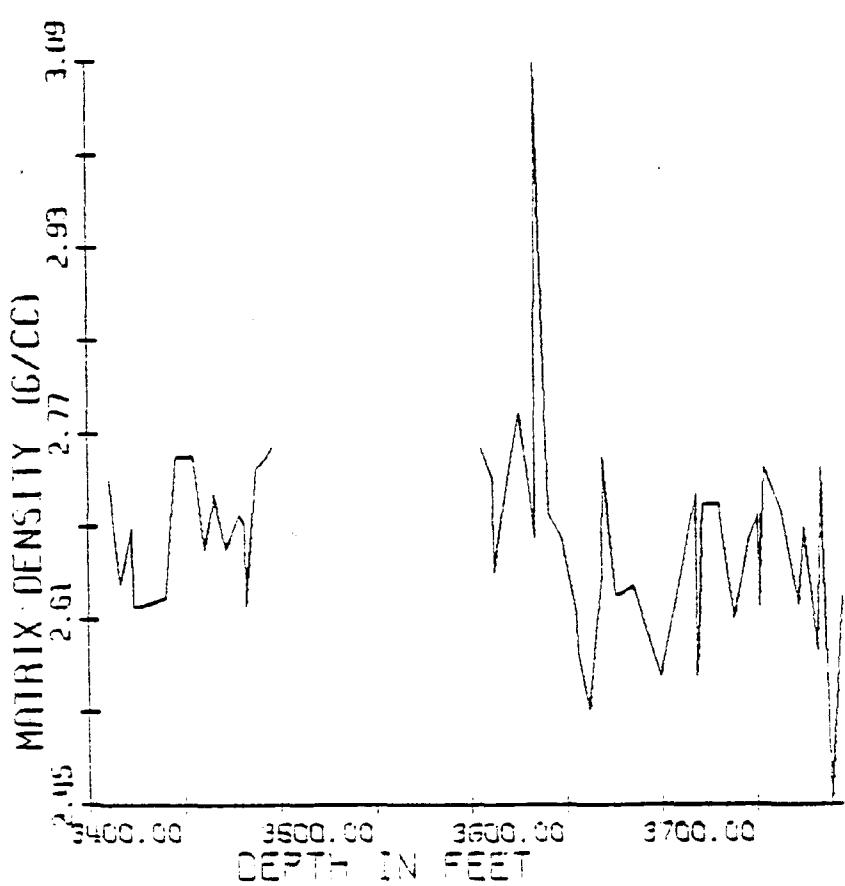


PROVISIONAL
OPEN TO REVISION
SUBJECT TO REVISION

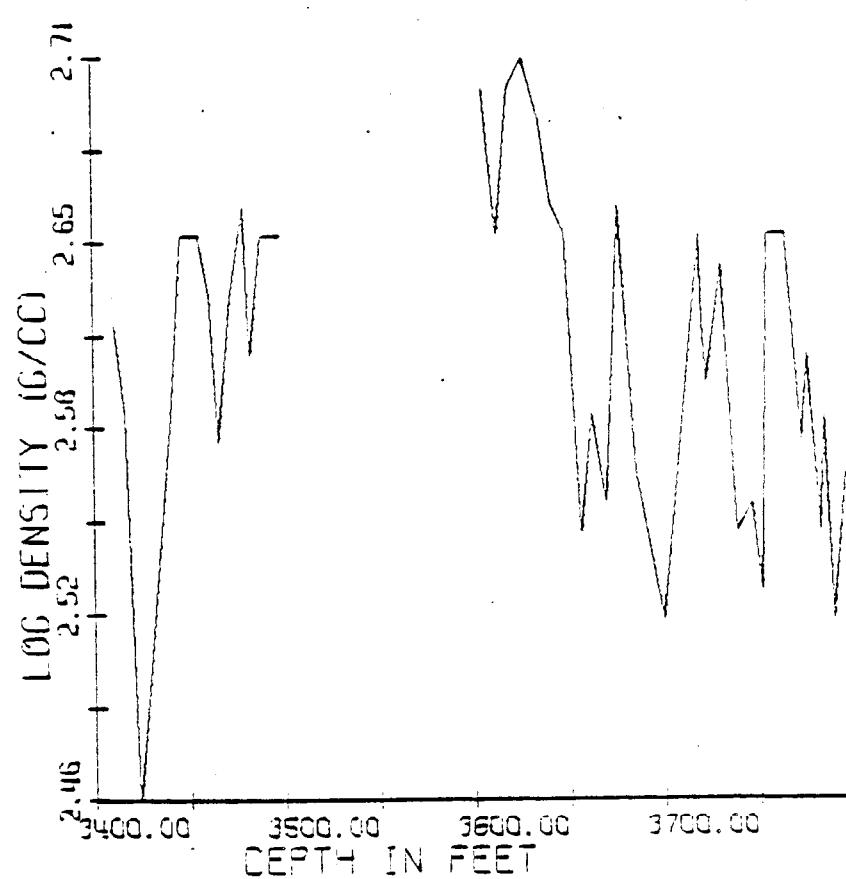




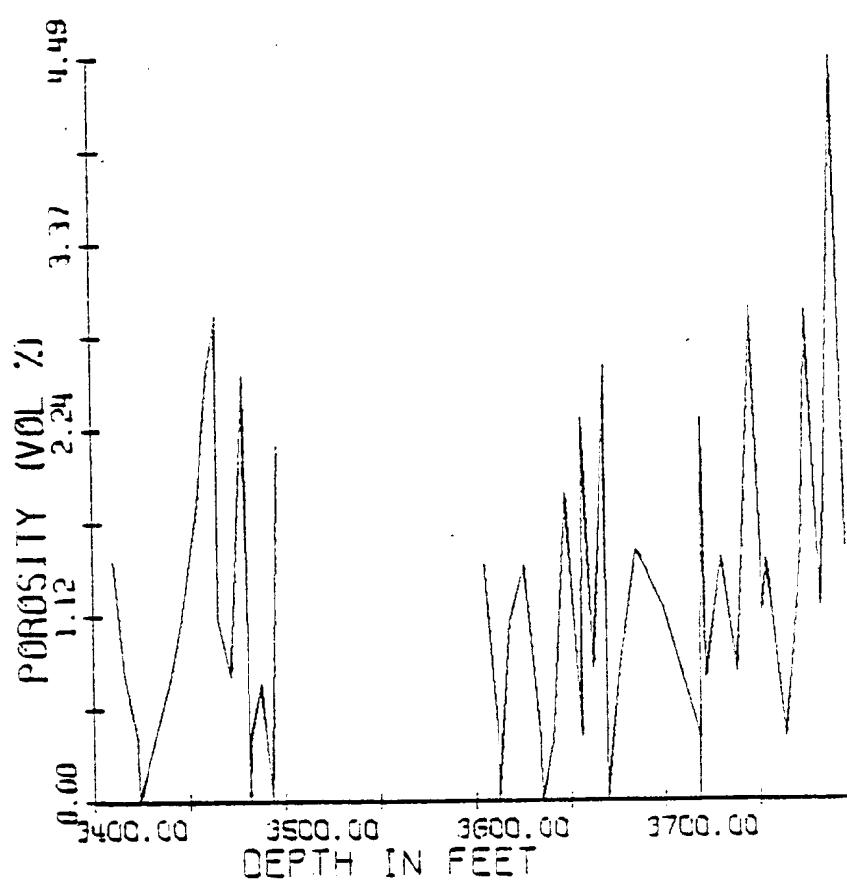
APPENDIX
OPERATION
SUBDIVISION



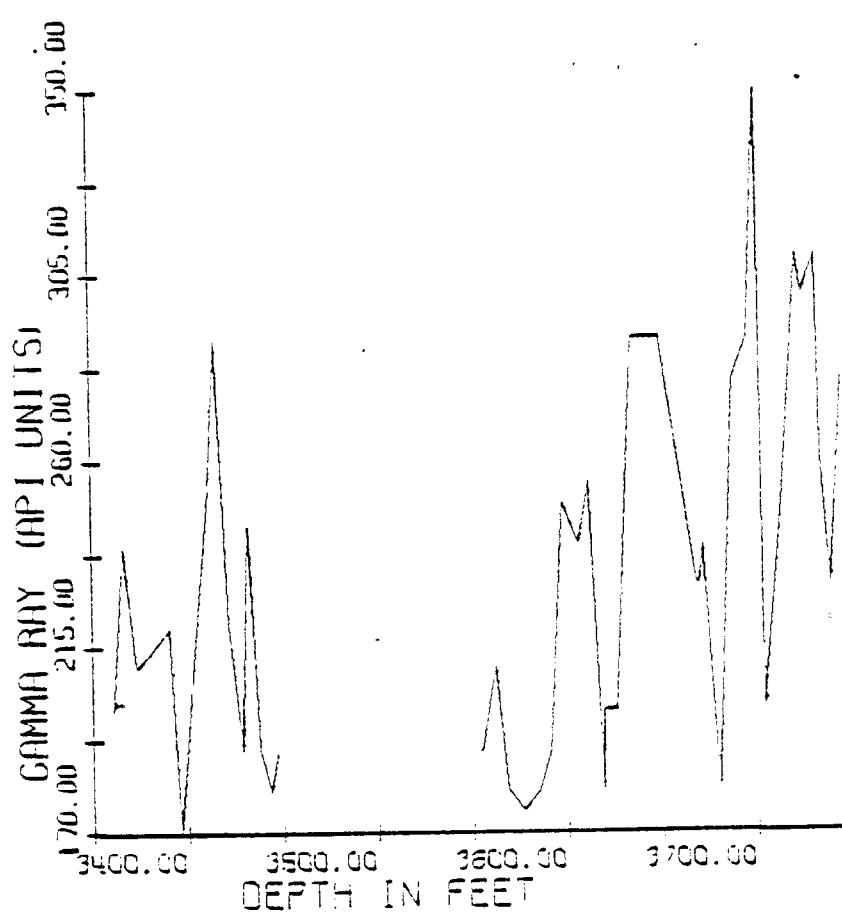
Density Log
Study of Density
in Coal



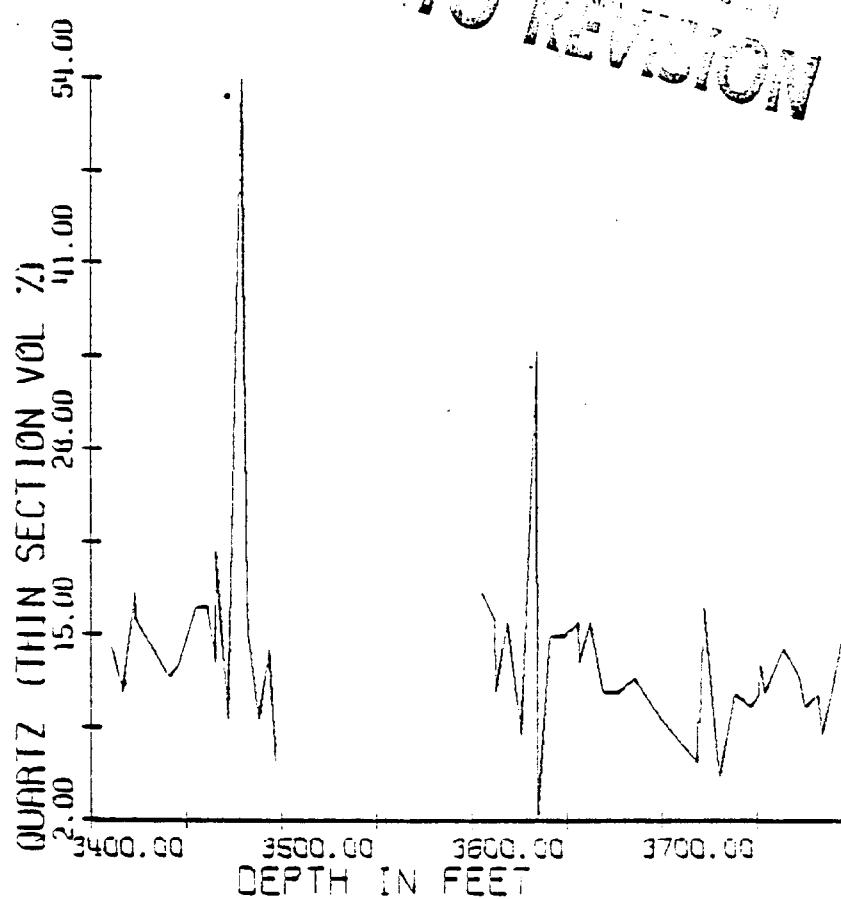
POLAROID
SOLID STATE
REVISION



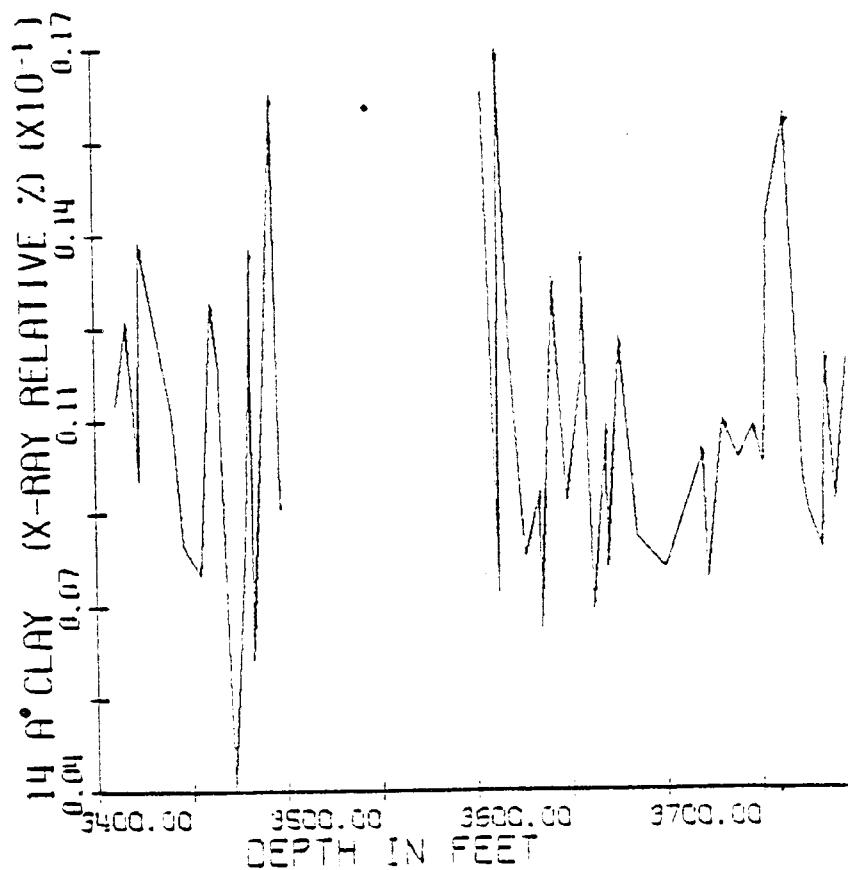
DATA SHEET
SUBJ TO READING
MOT

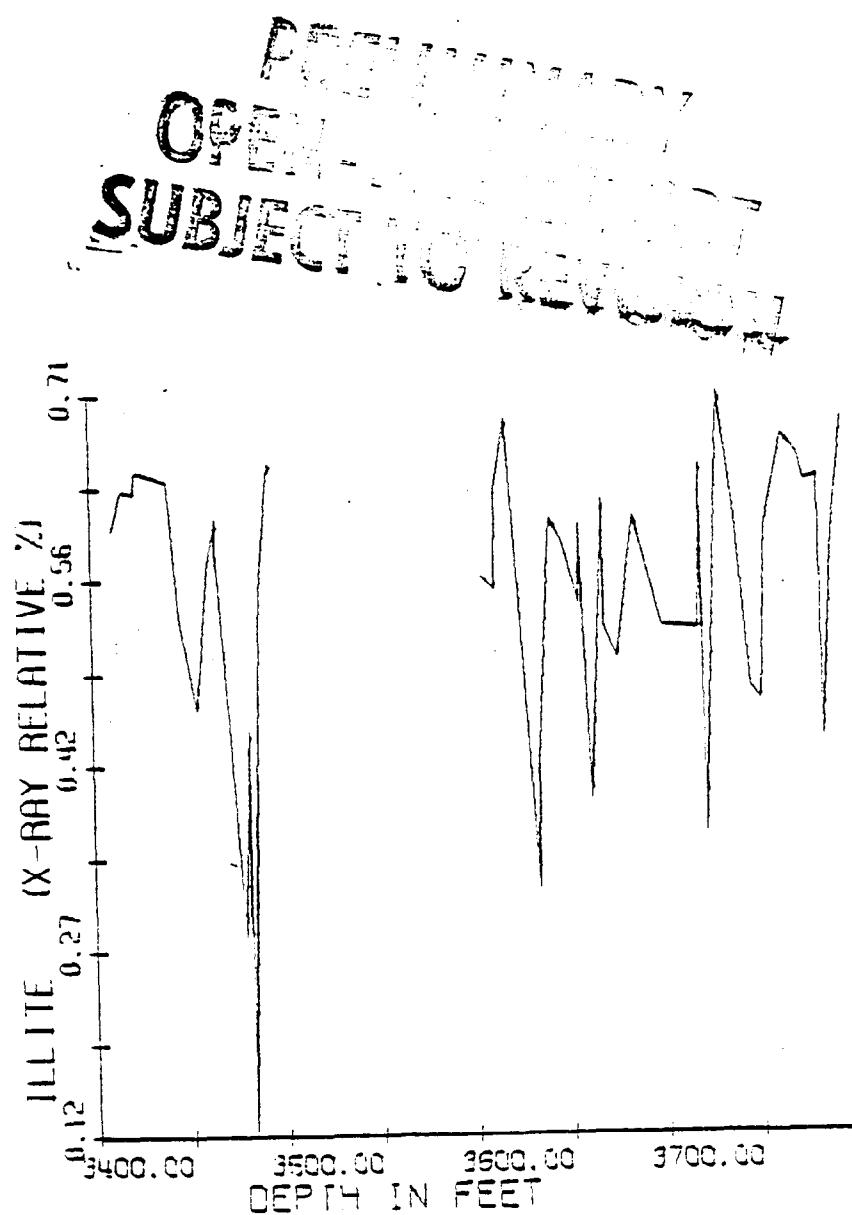


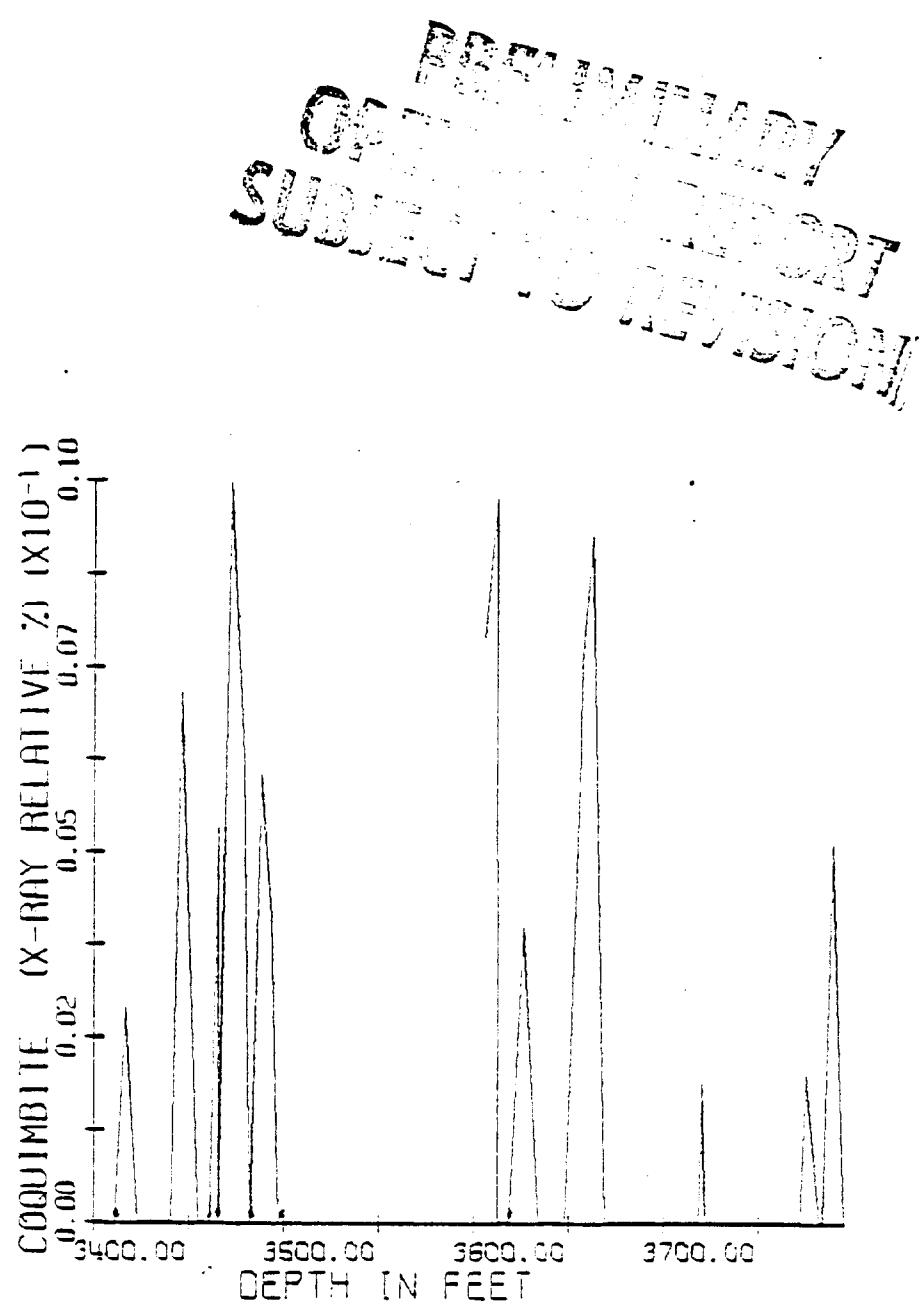
PRELIMINARY
OPEN TO DISCUSSION
SUBJECT TO REVISION



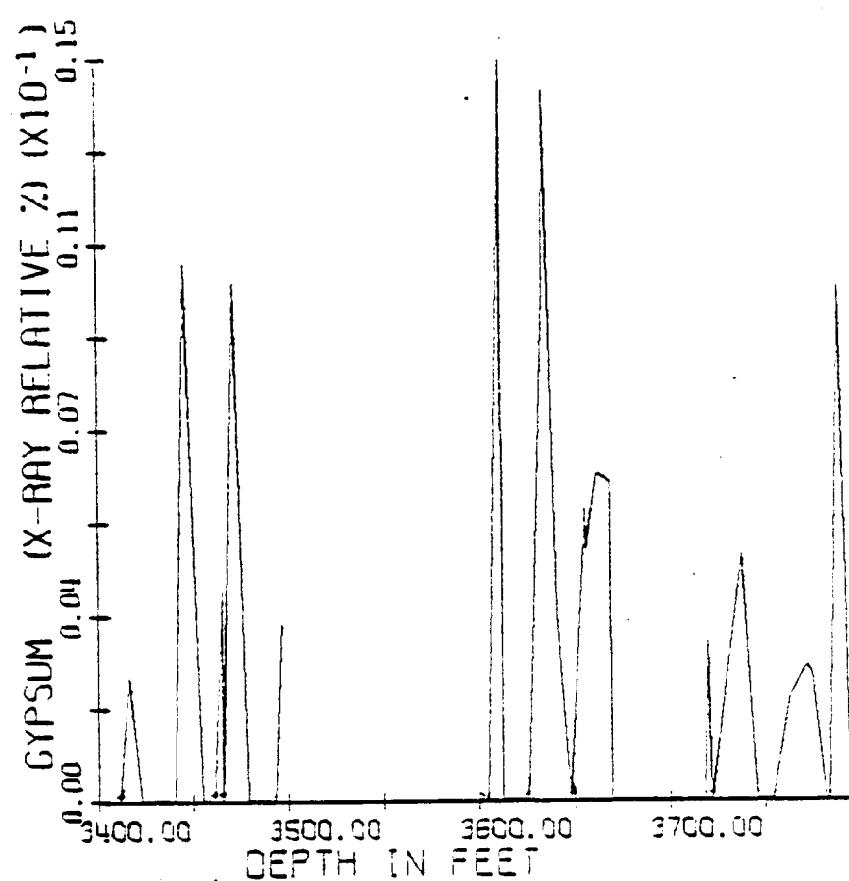
Preliminary
Geological Report
Subject to Revision



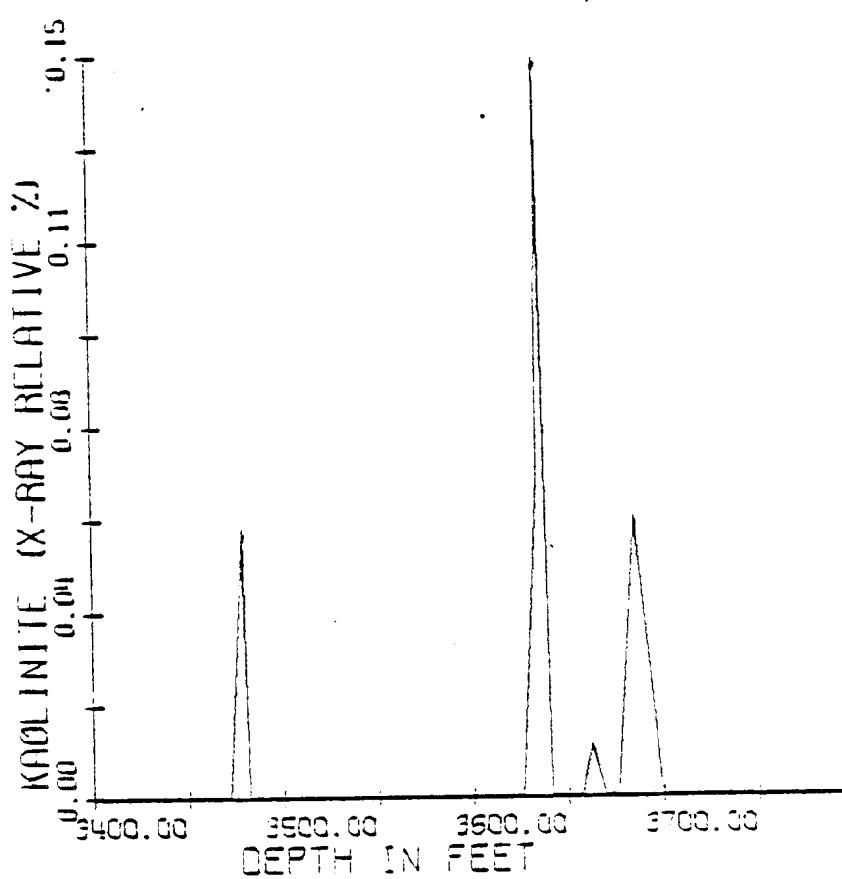




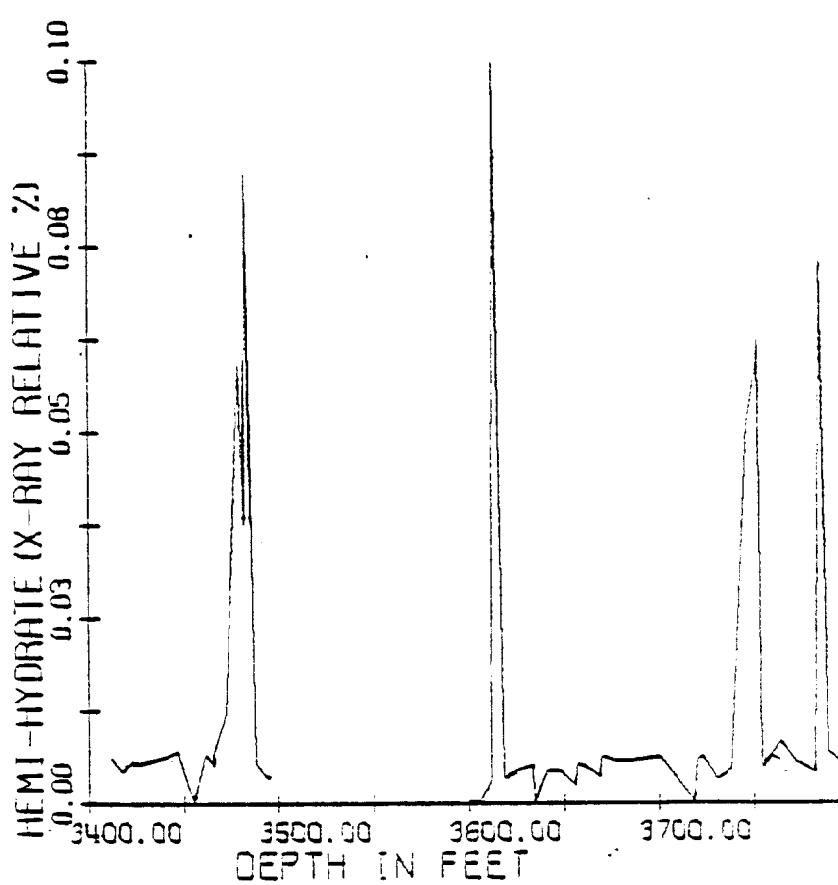
Subj to No Revision



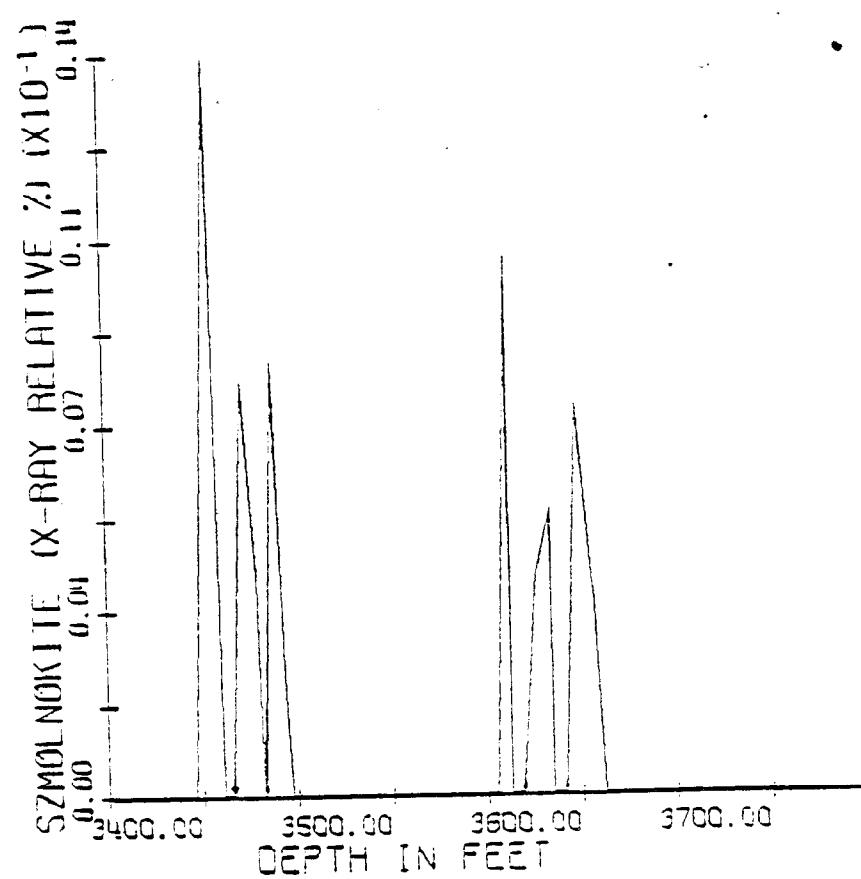
RECORDED BY
G.C.
SUBJECT TO REVISION



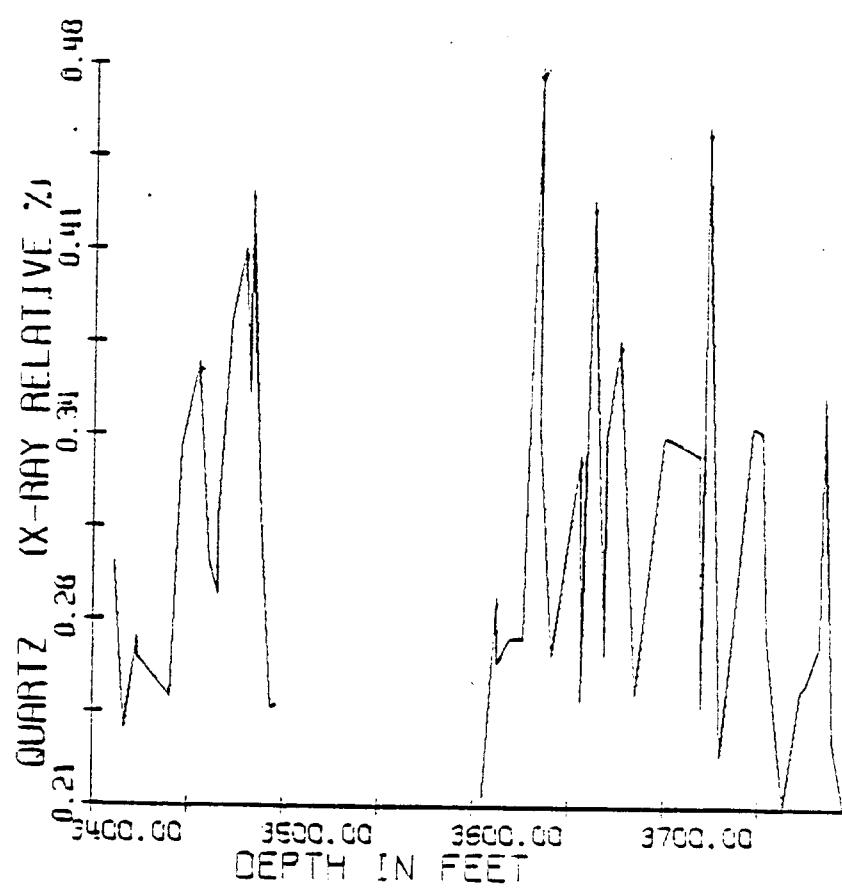
Sub-Canyon Valley

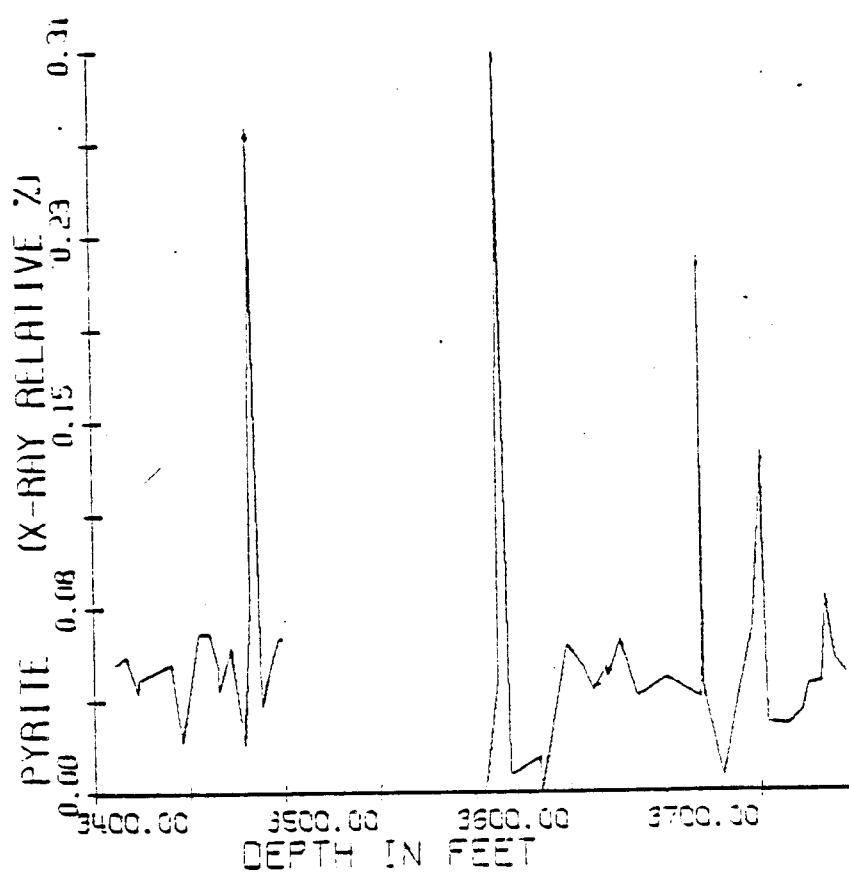


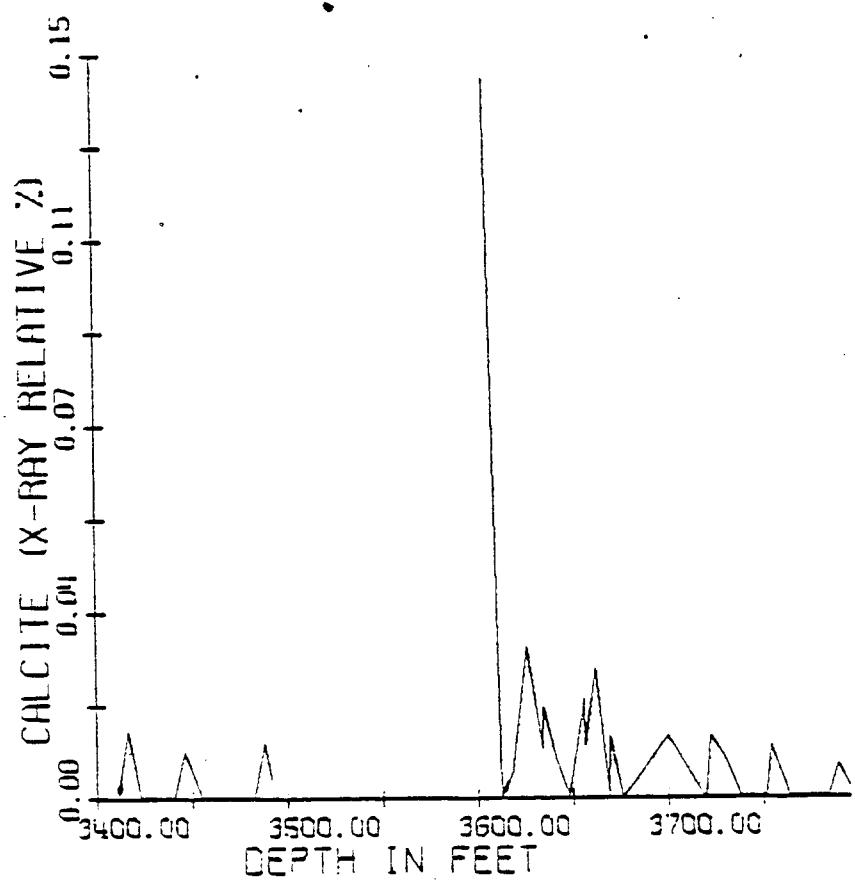
SUBJEC^T OPEN PRELIMINARY



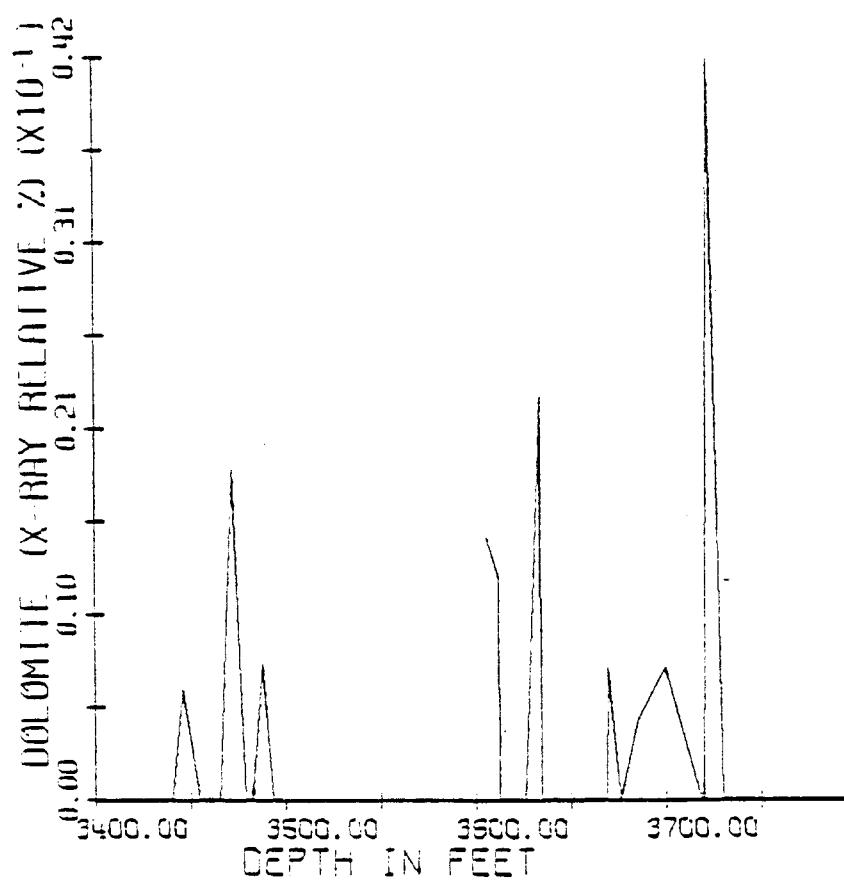
PRELIMINARY
SUSPENDED
NOT DRAWN

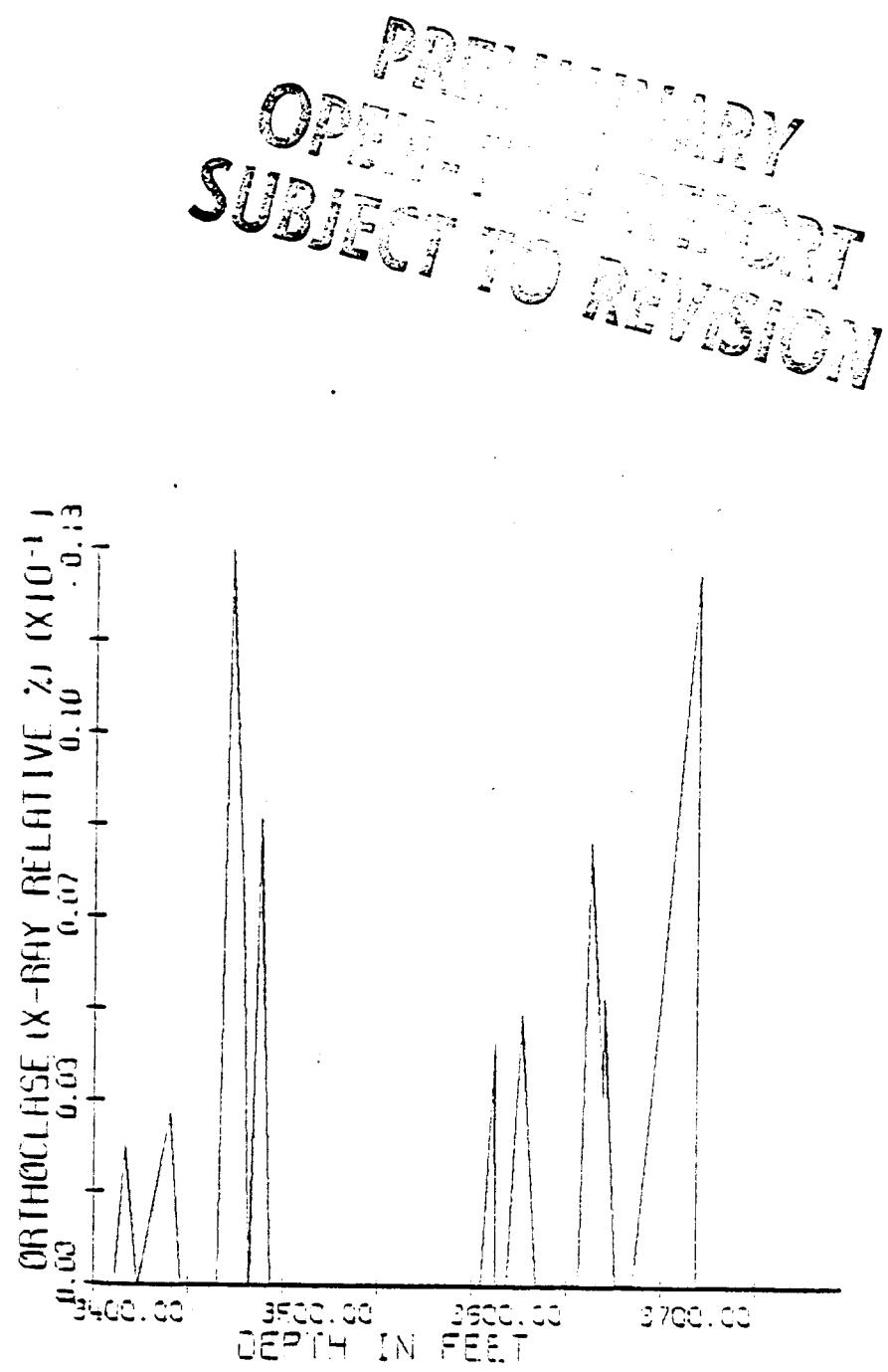




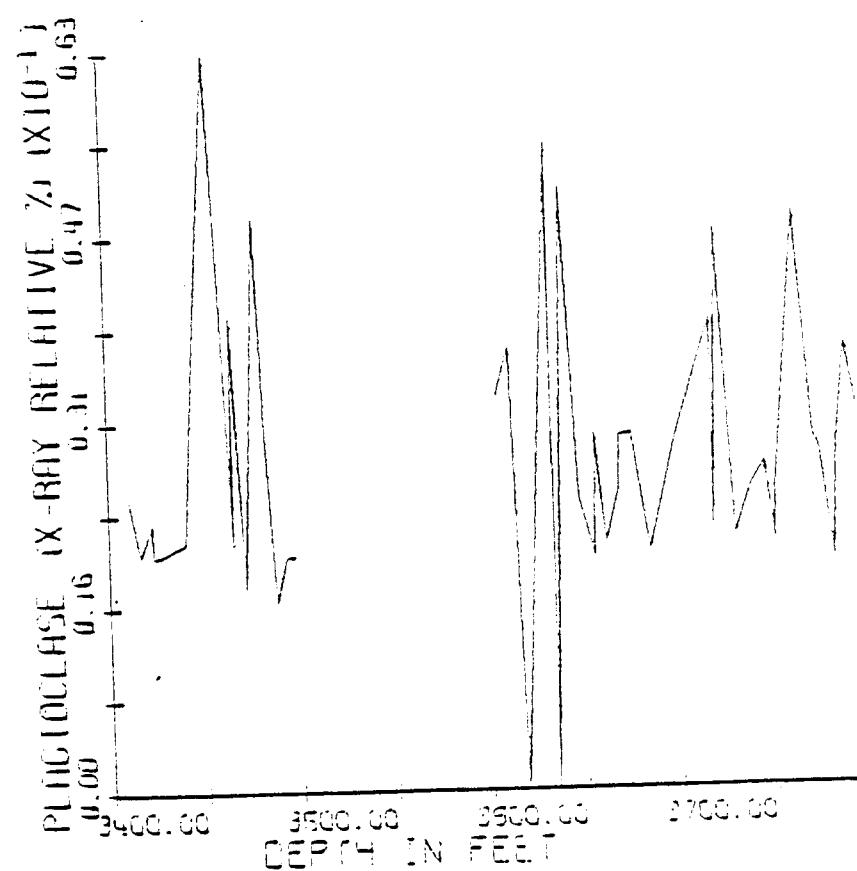


Open Hole
Subsurface
Hole

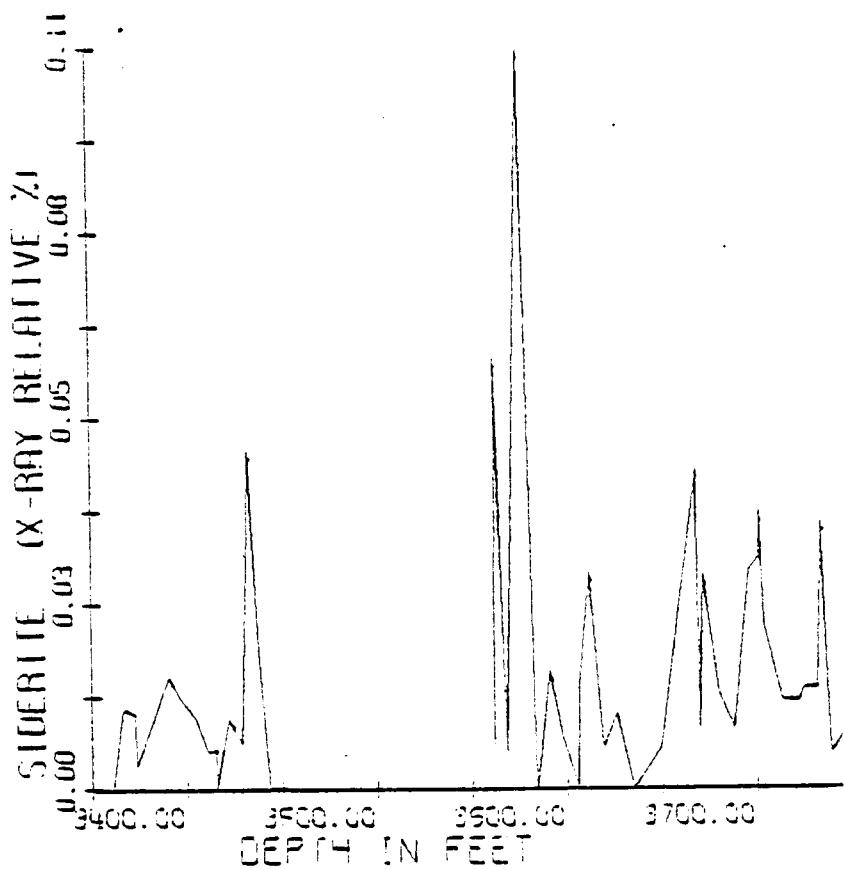




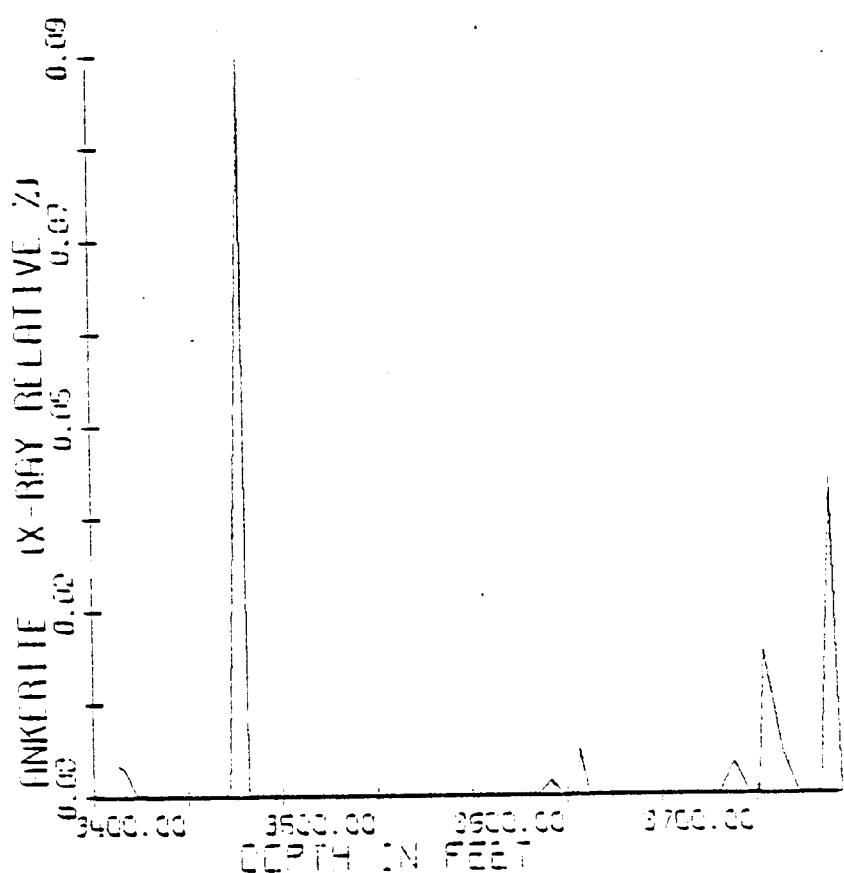
DATA
OPEN
SUBJECT TO REVIEW



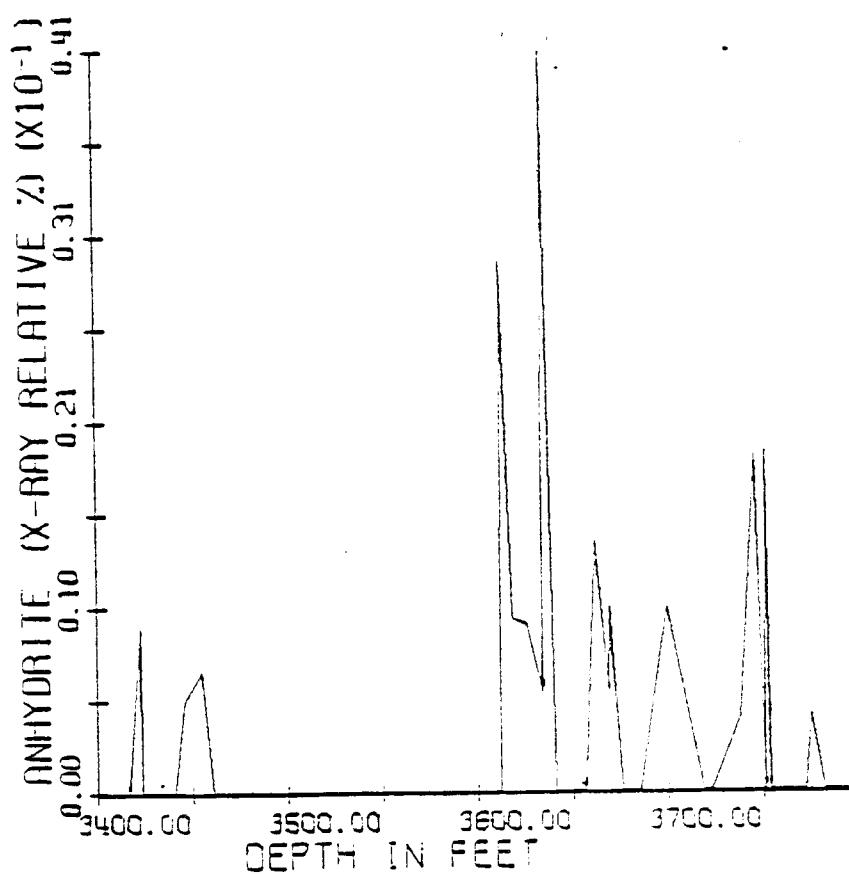
PRELIMINARY
OPEN
SUBJ [unclear]



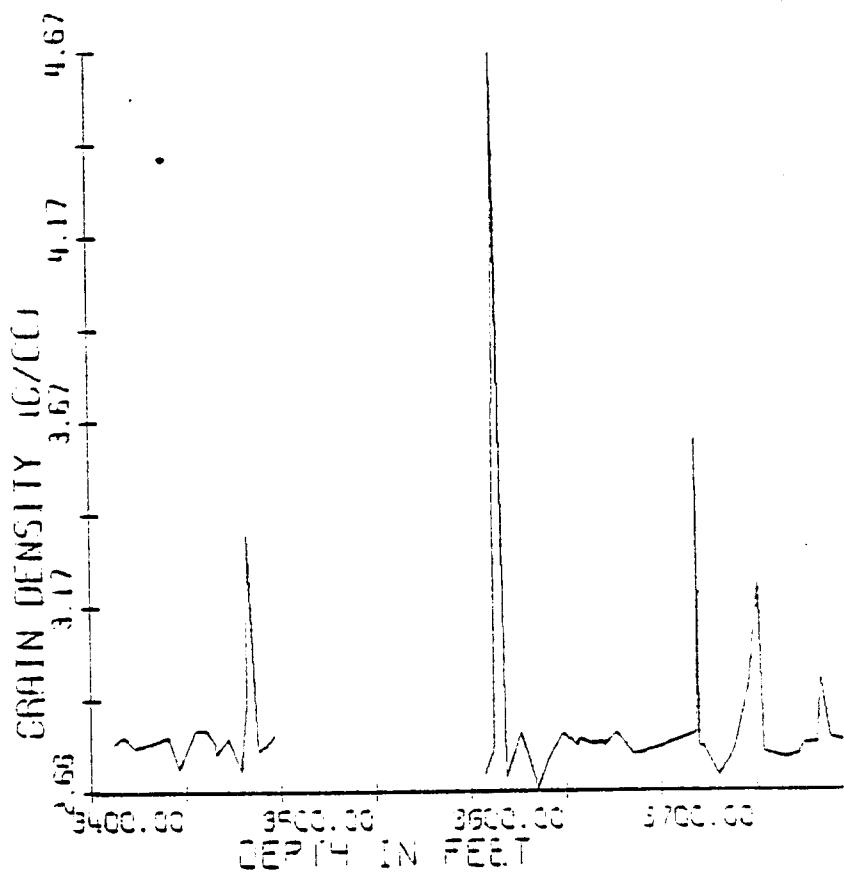
PROBLEMS
OPEN TO DISCUSSION
SUBJECT TO REVISION



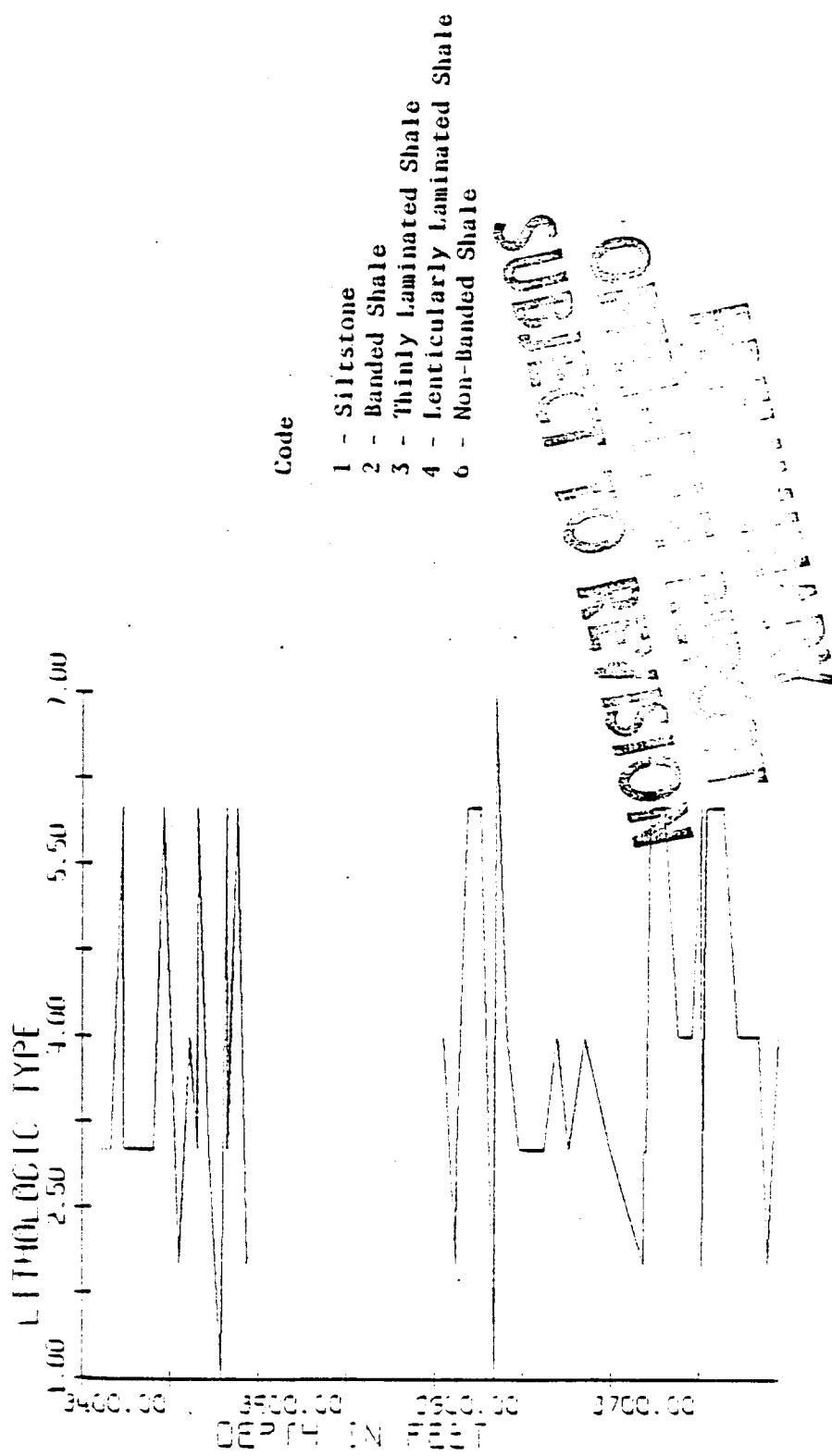
SOIL AND
SUBSTRATE
PROFILING



PRELIMINARY
OPEN-FILE REPORT
SUBJECT TO REVISION



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APPENDIX B

MEANS AND CORRELATION MATRIX - OVERALL WELL

STATISTICAL ANALYSIS SYSTEM 12156 FRIDAY, JANUARY 12, 1979 5

VARIABLE	N	MEAN	STD DEV	SUM	MINIMUM	MAXIMUM
SAMPLE	40	3603.67750000	125.91470731	144147.10000000	3411.20000000	3795.00000000
LDSIG100	40	4.54750000	1.61784718	181.90000000	1.60000000	7.20000000
LDSIG500	40	2.95500000	0.6855972	118.20000000	1.50000000	4.70000000
SULFUR	40	2.06025000	1.36897021	82.41000000	0.11000000	8.50000000
BULKDEN	40	2.64575000	0.06990424	105.83000000	2.51000000	2.70000000
MATDUDEN	40	2.67800000	0.06357713	107.12000000	2.53000000	2.79000000
LOGDE_N	40	2.60975000	0.05903554	104.39000000	2.46000000	2.71000000
POROSITY	40	1.25150000	0.83284976	50.06000000	0	2.97000000
GAMMA	40	228.00000000	42.78449276	9120.00000000	170.00000000	310.00000000
QUARTZ	40	0.14525000	0.00063809	5.81000000	0.05000000	0.54000000
EXP	40	0.01048355	0.00252602	0.41934205	0.00036185	0.01612921
ILL.	40	0.57191661	0.10068549	22.87666438	0.20053076	0.70828526
CDO	40	0.003224530	0.00332954	0.09982117	0	0.09991311
GYP	40	0.00253309	0.00369771	0.10132370	0	0.01473198
KAO	40	0.00177539	0.01606836	0.19101572	0	0.06592467
HEM	40	0.00644154	0.00888500	0.25760226	0	0.05969376
ANH	40	0.00242080	0.00399917	0.09715196	0	0.04411115
S2A	40	0.00114354	0.00352256	0.07374173	0	0.00116221
OT2	40	0.29610955	0.06804697	11.84438212	0	0.06643531
PYR	40	0.04123579	0.01744224	1.64943150	0	0.14968493
CAL	40	0.00990916	0.02400969	0.37636627	0	0.04478846
DOL	40	0.00361133	0.00813473	0.14445305	0	0.01319109
GRT	40	0.00161863	0.00308370	0.06474516	0	0.06294421
PLA	40	0.02966970	0.01235544	1.18438816	0	0.10947058
S1D	40	0.01245268	0.01759347	0.49810708	0	0.09009763
AHK	40	0.00320537	0.01440795	0.11111111	0	0.09009763

MONDAY
1/15/79
10:00 AM

STATISTICAL ANALYSIS SYSTEM 12:56 FRIDAY, JANUARY 12, 1979

VARIABLE	N	MEAN	STD. DEV.	SUM	MINIMUM	MAXIMUM
		6.68854067	2.69251824	2.64576393		

CORRELATION COEFFICIENTS / PREDICTIVE VALUE WITH HOSPITAL / N = 40

STATISTICAL ANALYSIS SYSTEM

12:56 FRIDAY, JANUARY 12, 1979

CORRELATION COEFFICIENTS / PHOB > IRI UNDER HOIHD=0 / N = 40

SAMPLE	L0SIG100	L0SIG500	SULFOR	HULDEN	MATRADEN	LUGEN	PURITY	GAMMA	UHANTZ	EXP	ILL.	ILL.	C10	
HEM	-0.18054	-0.24696	-0.26912	-0.45328	-0.36039	0.01742	0.09110	0.22243	-0.09930	0.75860	-0.616785	-0.48440	0.18987	
	0.6649	0.1246	0.26456	0.3450	0.70113	0.91532	0.51116	0.16719	0.5421	0.0001	0.6005	0.60115	0.24406	
AH11	0.40166	0.12441	0.44441	0.85392	0.92892	0.13242	0.00014	0.04476	0.09314	-0.12918	0.42671	-0.24773	-0.09608	
	0.6646	0.12441	0.44441	0.85392	0.92892	0.13242	0.00014	0.04476	0.09314	-0.12918	0.42671	-0.24773	-0.09608	
SZA	-0.2244	-0.4167	0.3205	0.4050	0.64439	0.01047	0.21527	0.24712	0.31221	-0.04718	0.20313	0.19925	0.25896	
	0.1631	0.4167	0.3205	0.4050	0.64439	0.01047	0.21527	0.24712	0.31221	-0.04718	0.20313	0.19925	0.25896	
OTZ	-0.1196	-0.3969	0.1396	0.19982	0.00153	-0.2499	0.9164	0.10980	0.17127	-0.1957	0.47906	-0.53221	0.91391	
	0.7432	-0.3969	0.1396	0.19982	0.00153	-0.2499	0.9164	0.10980	0.17127	-0.1957	0.47906	-0.53221	0.91391	
PHB	-0.26836	0.51387	0.50114	0.62448	-0.36034	-0.36034	-0.10198	-0.19530	0.10170	0.31542	-0.14718	0.39123	-0.98151	
	0.0912	0.51387	0.50114	0.62448	-0.36034	-0.36034	-0.10198	-0.19530	0.10170	0.31542	-0.14718	0.39123	-0.98151	
CAL	0.04432	-0.14838	0.14838	0.13246	-0.23243	0.19586	0.20749	0.28443	0.0749	-0.01539	0.20672	0.23716	0.47927	
	0.7466	-0.14838	0.14838	0.13246	-0.23243	0.19586	0.20749	0.28443	0.0749	-0.01539	0.20672	0.23716	0.47927	
HOM	0.0727	-0.11323	-0.28236	0.33439	0.15649	0.24894	0.17997	0.13562	-0.26903	0.19261	0.15414	-0.30654	0.26189	
	0.6556	-0.11323	-0.28236	0.33439	0.15649	0.24894	0.17997	0.13562	-0.26903	0.19261	0.15414	-0.30654	0.26189	
INT	-0.14002	0.23291	0.11124	0.16549	-0.00319	-0.01315	0.07068	-0.13773	-0.13968	0.13061	0.53247	-0.50676	0.45615	
	0.2505	0.23291	0.11124	0.16549	-0.00319	-0.01315	0.07068	-0.13773	-0.13968	0.13061	0.53247	-0.50676	0.45615	
PLA	0.04549	-0.35252	-0.37642	-0.24747	0.18702	0.15002	0.20447	0.25104	0.04398	-0.01957	0.46142	-0.46639	-0.19710	
	0.74805	-0.35252	-0.37642	-0.24747	0.18702	0.15002	0.20447	0.25104	0.04398	-0.01957	0.46142	-0.46639	-0.19710	
S10	0.13342	0.03671	-0.05430	-0.26430	0.09984	0.14277	0.18004	0.25297	0.03930	-0.15457	-0.13715	-0.18175	0.16614	
	0.1344	0.03671	-0.05430	-0.26430	0.09984	0.14277	0.18004	0.25297	0.03930	-0.15457	-0.13715	-0.18175	0.16614	
ANK	-0.11632	-0.32484	-0.29677	-0.20167	-0.29120	-0.02513	0.06882	0.19883	0.25954	0.19883	0.76190	-0.92011	0.42234	
	0.4729	-0.32484	-0.29677	-0.20167	-0.29120	-0.02513	0.06882	0.19883	0.25954	0.19883	0.76190	-0.92011	0.42234	
GROIN	-0.17858	0.58891	0.50007	0.51632	-0.27587	-0.19262	-0.20903	0.23788	0.12788	0.1125	-0.41335	-0.19271	0.94424	
	0.2302	0.58891	0.50007	0.51632	-0.27587	-0.19262	-0.20903	0.23788	0.12788	0.1125	-0.41335	-0.19271	0.94424	
GTP	KAU	HEM	ANH	S24	012	PIR	CAL	OUT.	INT.	PLA	SIN	ANK		
SAMPLE	0.09062	0.090502	-0.016654	0.01160	-0.22481	-0.11916	-0.26826	0.04432	0.07213	-0.14692	0.04549	0.15398	-0.11681	
	0.9960	0.9955	-0.02659	0.02659	0.0886	0.12477	0.16719	0.0866	0.6556	0.7505	0.7605	0.3432	-0.4729	
L0SIG100	-0.07112	-0.31620	-0.24666	0.12443	-0.13205	-0.4165	0.1390	0.51187	-0.11030	-0.24552	0.23971	-0.5523	0.32554	
	0.16100	-0.07112	-0.31620	-0.24666	0.12443	-0.13205	-0.4165	0.1390	0.51187	-0.11030	-0.24552	0.23971	-0.5523	0.32554
L0SIG500	-0.19289	-0.31221	-0.26912	0.08927	0.04050	-0.27513	0.19298	0.50014	0.19316	-0.28256	0.11124	-0.31643	0.14230	
	0.22492	-0.0498	-0.0498	0.0592	0.0592	0.08040	0.2162	0.6010	0.2135	0.0773	0.4944	0.10163	0.7430	
SULFOR	-0.10252	-0.25609	-0.1107	0.15428	0.0007	0.4740	0.9489	0.00452	0.2343	-0.3251	0.16539	-0.2379	0.0994	

STATISTICAL ANALYSIS SYSTEM 12156 FRIDAY, JANUARY 12, 1979 8

CORRELATION COEFFICIENTS / PHIN > IRI UNDER NORMALIZED / N = 40												
GYP	NAI	HEM	ANH	S2A	OTZ	PHN	CAL	DUL	UHT	PLA	S1D	ANK
BULKDEN -0.05256 -0.07434 -0.06309 -0.06033 -0.06039 0.00814 0.00813 0.00749 -0.02429 -0.30634 0.19356 0.15002 0.14277 -0.02513												
MATHDEN -0.06005 -0.07424 -0.06926 0.01742 -0.05436 -0.05439 0.24712 -0.05329 -0.05333 -0.05822 0.20746 0.1097 -0.05355 0.3555 0.03395 -0.07717												
LOGDEN 0.11008 0.14559 0.13577 0.09716 -0.09218 0.05716 -0.05716 0.04231 0.04231 0.04980 0.04980 0.28486 0.15985 0.16994 0.06282 0.06686												
POROSITY -0.09922 0.05243 0.02224 -0.12244 -0.12244 -0.12244 -0.11735 -0.11735 -0.11735 -0.11735 0.19169 0.19169 0.13773 0.09190 0.25954												
GRAD 0.54225 0.74840 0.16749 -0.42669 0.42669 0.42669 -0.17883 -0.17883 -0.17883 0.51683 0.51683 0.51683 0.51683 0.51683 0.1059												
CANHA -0.13903 -0.05182 -0.09230 -0.05421 -0.05421 -0.05421 -0.12674 -0.12674 -0.12674 -0.12674 0.1957 0.1957 0.13093 0.13411 0.13411 -0.15277												
QUANTZ 0.01721 0.06249 0.06031 0.06031 0.06031 0.06031 0.28486 0.28486 0.28486 0.28486 0.28486 0.28486 0.28486 0.28486 0.28486 0.16300												
EXP -0.33352 -0.12123 -0.16785 -0.16785 -0.16785 -0.16785 -0.34834 -0.34834 -0.34834 -0.34834 0.32311 0.32311 0.27922 0.27922 0.27922 -0.2011												
ILL. -0.22914 -0.52251 -0.0005 0.0005 0.0005 0.0005 0.24711 -0.40160 -0.40160 -0.40160 0.01601 0.01601 0.01601 0.01601 0.01601 -0.02020												
CIOO 0.530878 0.009904 0.18987 -0.00805 0.00805 0.00805 0.18987 -0.00805 0.00805 0.00805 0.11735 0.11735 0.06679 0.06679 0.06679 -0.06679												
GYP 0.00000 0.10939 -0.07274 0.05102 0.05102 0.05102 0.29699 0.29699 0.29699 0.29699 0.09129 0.09129 0.08669 0.08669 0.08669 -0.12234												
KAO 0.10499 0.00000 0.51126 0.00000 0.00000 0.00000 0.02489 0.02489 0.02489 0.02489 0.11901 0.11901 0.03921 0.03921 0.03921 -0.0653												
HEM -0.07578 0.04129 0.04129 0.00000 0.00000 0.00000 0.14936 0.14936 0.14936 0.14936 0.06816 0.06816 0.03921 0.03921 0.03921 -0.12571												
ANH 0.03410 0.02489 0.02489 0.11493 0.11493 0.11493 0.00000 0.00000 0.00000 0.00000 0.01442 0.01442 0.02048 0.02048 0.02048 -0.12454												
S2A 0.29829 0.14403 0.02698 -0.02698 -0.02698 -0.02698 0.00000 0.00000 0.00000 0.00000 0.31016 0.31016 0.16432 0.16432 0.16432 -0.0639												
OTZ 0.24513 0.40657 0.32016 0.00922 0.00922 0.00922 0.16165 0.16165 0.16165 0.16165 0.31672 0.31672 0.17626 0.17626 0.17626 -0.1430												
PHN -0.01276 -0.28094 -0.11859 0.13091 0.13091 0.13091 0.20943 0.20943 0.20943 0.20943 0.0169 0.0169 0.01996 0.01996 0.01996 -0.22970												
CAL. -0.04210 -0.03423 -0.03211 0.04643 0.04643 0.04643 0.16165 0.16165 0.16165 0.16165 0.41591 0.41591 0.27061 0.27061 0.27061 -0.06397												

CONFIDENTIAL
NOV 1979

11

STATISTICAL ANALYSIS SYSTEM 12:56 FRIDAY, JANUARY 12, 1979

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SAMPLE	-0.17954
L05IG100	0.58681
L05IG500	0.51264
SULFUR	0.51615
MULTIDEN	-0.22753
MATHDEN	-0.19992
LUGDEN	-0.29091
POROSITY	0.12799
GAMA	0.43387
QUARTZ	-0.41335

STATISTICAL ANALYSIS SYSTEM 12:56 FRIDAY, JANUARY 12, 1979 10
CORRELATION COEFFICIENTS / PROB > 1st ORDER 0.000000 / n = 40

	GHDEN
EAP	-0.19971 0.2166
LLL	0.09324 0.5610
CDD	-0.07641 0.6394
GYP	-0.11719 0.1639
KAD	-0.41709 0.0074
HEM	-0.21649 0.1797
ASH	-0.06844 0.6394
S2A	0.4824 0.2599
OTZ	-0.03425 0.8339
PTH	0.05934 0.0001
CAL	-0.38565 0.0140
DUL	-0.23973 0.1526
IRT	0.14617 0.3661
P.LA	-0.12409 0.4456
SID	0.19659 0.2240
ANK	-0.26421 0.1664
GHDEN	1.00000 0.0000

NOISY COEFFICIENTS

APPENDIX C

MEANS AND CORRELATION MATRICES BY LITHOTYPE

Lenticularly Laminated Shale

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STATISTICAL ANALYSIS SYSTEM

11:32 WEDNESDAY, JANUARY 17, 1973

VARIABLE	N	MEAN	STD DEV	SUM	MINIMUM	MAXIMUM
SAMPLE	11	36.902148182	9.33750367	405.9240000060	3461.90000000	3795.00000000
LOSS10.0	11	5.109090914	1.33750106	56.20000000	2.86000000	7.00000000
LOSS15.0	11	3.19090909	0.70349775	35.10000000	1.86000000	4.20000000
SOL.FINE	11	2.41909091	2.15014019	26.61000000	0.11000000	6.50000000
BLK.KOF's	11	2.02545455	0.06919012	28.08000000	2.55000000	2.77000000
MATERIAL	11	2.66364636	0.05690809	29.36000000	2.58000000	2.76000000
LARGE'S	11	2.39454545	0.04967165	28.54000000	2.55000000	2.70000000
POROSITY	11	1.50154545	0.943069452	16.55000000	0	2.97000000
GAGE	11	252.72727273	52.55100355	2780.00000000	180.00000000	310.00000000
SHANTZ	11	0.13000000	0.02154810	1.43000000	0.10000000	0.18000000
F.E.P.	11	0.01066353	0.00245217	0.11729880	0.00006901	0.01606754
G.I.	11	0.61227638	0.04592967	6.73504023	0.52237284	0.58648362
CID	11	0.00098018	0.00213664	0.00962400	0	0.00769147
G.Y.F	11	0.00181073	0.00231298	0.02013808	0	0.00631097
F.A.O	11	0.00528714	0.01753627	0.050161122	0	0.05816122
H.E.S	11	0.00165312	0.00183959	0.05119432	0	0.00684705
A.U.D	11	0.00222605	0.00347079	0.02444657	0	0.01936122
S.Z.1	11	0	0	0	0	0
O.I.Z.	11	0.26227515	0.03029999	2.86502664	0.20714352	0.34398397
P.Y.B	11	0.04031229	0.01647451	0.44409524	0	0.06536676
C.A.I.	11	0.01605948	0.04451258	0.17665424	0	0.14963493
D.I.L	11	0.002255403	0.01484711	0.02699443	0	0.01497757
O.C.T	11	0.003919150	0.00178785	0.00859649	0	0.00522896
P.Y.A	11	0.03044269	0.00907785	0.33486960	0.01931126	0.05113655
S.I.D	11	0.00927581	0.00521783	0.10203349	0	0.01772269
A.U.K	11	0.00052167	0.00040573835	0	0.00125294	0.001942451

NOVEMBER 1973
W.VA. GEOLOGICAL SURVEY

STATISTICAL ANALYSIS SYSTEM WEDNESDAY, JANUARY 17, 1979

WAVELENGTH	MEAN	STD. DEV.	SUM	MINIMUM	MAXIMUM
442.1	10.64511514	10.64511514	2.69251824	2.69251824	2.69251824

U-1920126022
2.78542139

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JGR File # 157
W.Va. Geological & Economic Survey

**THE
LITERARY
MAGAZINE**

STATISTICAL ANALYSIS SYSTEM
 8:32 WEDNESDAY, JANUARY 17, 1978

	CORRELATION COEFFICIENTS / PHOT > IRI UNDER NO:PHOTO = 0 / N = 13												
	SAMPLE	LOSSIG100	LOSSIG500	SULFUR	BULKDEN	MATRIXDEN	LOGICEN	POROSITY	GAMMA	QUARTZ	EXP	IRL	CIO
KAD	-0.17442	-0.12721	-0.09000	-0.12202	-0.13161	-0.16389	0.04054	0.24523	-0.12911	-0.29371	-0.01084	-0.12491	0.11441
	0.17545	0.17113	0.17924	0.18087	0.17208	0.16806	0.13101	0.14863	0.12046	0.19671	0.01084	0.12491	0.11441
HEM	-0.01496	0.25304	-0.15009	0.15009	0.15009	0.15009	0.15009	0.15009	0.15009	0.15009	0.15009	0.15009	0.15009
	0.01496	0.07613	0.07613	0.07613	0.07613	0.07613	0.07613	0.07613	0.07613	0.07613	0.07613	0.07613	0.07613
ANH	0.07011	0.16312	0.16312	0.16312	0.16312	0.16312	0.16312	0.16312	0.16312	0.16312	0.16312	0.16312	0.16312
	0.07011	0.16312	0.16312	0.16312	0.16312	0.16312	0.16312	0.16312	0.16312	0.16312	0.16312	0.16312	0.16312
SZL4	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
SHZ	-0.21716	0.43250	0.30421	0.30421	0.30421	0.30421	0.30421	0.30421	0.30421	0.30421	0.30421	0.30421	0.30421
	0.21716	-0.43250	-0.30421	-0.30421	-0.30421	-0.30421	-0.30421	-0.30421	-0.30421	-0.30421	-0.30421	-0.30421	-0.30421
PLA	-0.07144	0.72939	0.23232	0.23232	0.23232	0.23232	0.23232	0.23232	0.23232	0.23232	0.23232	0.23232	0.23232
	0.07144	-0.72939	-0.23232	-0.23232	-0.23232	-0.23232	-0.23232	-0.23232	-0.23232	-0.23232	-0.23232	-0.23232	-0.23232
CAL	-0.29919	-0.54569	0.14001	0.14001	0.14001	0.14001	0.14001	0.14001	0.14001	0.14001	0.14001	0.14001	0.14001
	0.29919	-0.54569	-0.14001	-0.14001	-0.14001	-0.14001	-0.14001	-0.14001	-0.14001	-0.14001	-0.14001	-0.14001	-0.14001
DOL	-0.30261	-0.32518	0.28940	0.28940	0.28940	0.28940	0.28940	0.28940	0.28940	0.28940	0.28940	0.28940	0.28940
	0.30261	-0.32518	-0.28940	-0.28940	-0.28940	-0.28940	-0.28940	-0.28940	-0.28940	-0.28940	-0.28940	-0.28940	-0.28940
GRD	-0.10162	0.33892	0.04539	0.04539	0.04539	0.04539	0.04539	0.04539	0.04539	0.04539	0.04539	0.04539	0.04539
	0.10162	-0.33892	-0.04539	-0.04539	-0.04539	-0.04539	-0.04539	-0.04539	-0.04539	-0.04539	-0.04539	-0.04539	-0.04539
PLA	-0.52541	-0.45000	-0.53494	-0.53494	-0.53494	-0.53494	-0.53494	-0.53494	-0.53494	-0.53494	-0.53494	-0.53494	-0.53494
	0.52541	-0.45000	-0.53494	-0.53494	-0.53494	-0.53494	-0.53494	-0.53494	-0.53494	-0.53494	-0.53494	-0.53494	-0.53494
S10	0.17109	-0.23846	0.17414	0.17414	0.17414	0.17414	0.17414	0.17414	0.17414	0.17414	0.17414	0.17414	0.17414
	0.17109	-0.23846	-0.17414	-0.17414	-0.17414	-0.17414	-0.17414	-0.17414	-0.17414	-0.17414	-0.17414	-0.17414	-0.17414
AKK	0.03041	-0.16912	-0.26313	-0.26313	-0.26313	-0.26313	-0.26313	-0.26313	-0.26313	-0.26313	-0.26313	-0.26313	-0.26313
	0.03041	-0.16912	-0.26313	-0.26313	-0.26313	-0.26313	-0.26313	-0.26313	-0.26313	-0.26313	-0.26313	-0.26313	-0.26313
GRD14	0.01142	0.16126	0.18801	0.18801	0.18801	0.18801	0.18801	0.18801	0.18801	0.18801	0.18801	0.18801	0.18801
	0.96142	-0.16126	-0.18801	-0.18801	-0.18801	-0.18801	-0.18801	-0.18801	-0.18801	-0.18801	-0.18801	-0.18801	-0.18801
GRD	0.01142	0.16126	0.18801	0.18801	0.18801	0.18801	0.18801	0.18801	0.18801	0.18801	0.18801	0.18801	0.18801
SAMPLE	0.15201	-0.01742	-0.01456	-0.01456	-0.01456	-0.01456	-0.01456	-0.01456	-0.01456	-0.01456	-0.01456	-0.01456	-0.01456
LOSSIG100	0.15201	-0.01742	-0.01456	-0.01456	-0.01456	-0.01456	-0.01456	-0.01456	-0.01456	-0.01456	-0.01456	-0.01456	-0.01456
LOSSIG500	0.15201	-0.01742	-0.01456	-0.01456	-0.01456	-0.01456	-0.01456	-0.01456	-0.01456	-0.01456	-0.01456	-0.01456	-0.01456
LOSSIG1000	0.15201	-0.01742	-0.01456	-0.01456	-0.01456	-0.01456	-0.01456	-0.01456	-0.01456	-0.01456	-0.01456	-0.01456	-0.01456

NON-
LINEAR
REGRESSION
RESULTS

STATISTICAL ANALYSIS SYSTEM 8:12 WEDNESDAY, JANUARY 17, 1979

CORRELATION COEFFICIENTS / PREDICTOR > THE UNDER NUMBER = n = 11

	GYP	RAO	HEW	ANH	SZN	WTZ	PYH	CAB	BOL	GNT	PLA	SID	ANK
SIL. FOR.	-0.13096 0.6571	-0.08262 0.8808	0.50217 0.1155	0.83380 0.0014	0.100000 1.0000	0.377471 0.6051	0.44977 0.6551	0.29617 0.765	0.68430 0.8053	0.87217 0.8065	-0.15373 0.6518	-0.26449 0.4313	-0.19779 0.55549
BULK.DR.	-0.23197 0.4310	-0.12202 0.7238	-0.18431 0.5804	0.40521 0.1862	0.100000 1.0000	0.29869 0.1122	-0.44377 0.5943	0.71237 0.6138	0.49265 0.1255	0.44982 0.1651	0.07484 0.1651	-0.02545 0.8269	-0.9408
TAUCH.DR.	-0.19701 0.5561	-0.13764 0.6966	-0.27132 0.4083	0.35849 0.2936	0.100000 1.0000	0.13617 0.6803	-0.15117 0.20359	0.61606 0.0436	0.71998 0.0125	0.39029 0.2250	0.47332 0.1284	-0.1812 0.1244	-0.20350 0.5564
LIGNEUS	-0.16809 0.6219	-0.16349 0.6304	-0.50720 0.1113	-0.38942 0.2158	0.100000 1.0000	0.35363 0.6043	-0.60263 0.0144	0.70990 0.1154	0.50721 0.1148	0.597440 0.1148	0.05722 0.0161	-0.05901 0.6056	-0.7921
POROSITY	0.14192 0.6192	0.00549 0.9831	-0.32321 0.3221	-0.18764 0.5040	0.100000 1.0000	0.31486 0.6028	-0.32516 0.4221	0.60244 0.6028	0.26435 0.2315	0.23941 0.2315	-0.14261 0.1451	-0.1081 0.1451	-0.41612 0.2006
GA.GRA	-0.22269 0.5912	0.24321 0.4863	0.37795 0.2439	-0.34055 0.1058	0.100000 1.0000	0.16548 0.6268	0.24921 0.4598	-0.41100 0.1146	0.45921 0.1554	0.500021 0.2048	0.14048 0.1164	-0.01024 0.6803	-0.9762
QUARTZ	-0.19319 0.2112	-0.12041 0.7246	-0.30946 0.3544	-0.52729 0.2444	0.100000 1.0000	0.38167 0.2444	-0.32907 0.0504	0.60131 0.2054	0.44411 0.2931	0.34863 0.2054	0.63066 0.2931	-0.15291 0.6514	-0.41223 0.2004
F.I.P	-0.23557 0.6371	-0.26377 0.3917	-0.59272 0.50546	-0.46998 0.1650	0.100000 1.0000	0.48270 0.1126	-0.52991 0.0561	0.77914 0.1124	0.47728 0.1165	0.32160 0.3348	0.64199 0.0310	0.06603 0.9860	0.04123 0.8945
H.F.	0.22249 0.4819	-0.61994 0.6194	0.04650 0.8920	-0.47319 0.1433	0.100000 1.0000	0.60472 0.0487	0.14154 0.6178	-0.41519 0.2039	0.54292 0.5295	0.52475 0.5295	0.22190 0.25118	0.35134 0.26194	0.00529 0.4877
C.H.O.	-0.23419 0.4503	-0.12491 0.1144	-0.42071 0.6020	-0.15821 0.6402	0.100000 1.0000	0.47670 0.1363	-0.78663 0.0041	0.95142 0.0023	0.20734 0.0023	0.18112 0.0023	0.06885 0.0023	-0.05268 0.6120	-0.17252 0.8770
G.Y.P	0.100000 0.60000	-0.26026 0.1336	-0.12865 0.7073	0.46924 0.4244	0.100000 1.0000	0.062221 0.8558	0.053223 0.03765	-0.28377 0.1709	0.47702 0.1709	0.32160 0.8834	0.64199 0.8834	0.52646 0.6062	0.00529 0.4877
K.A.D	-0.26926 0.4356	1.00000 0.0000	0.20351 0.5484	-0.21232 0.5300	0.100000 1.0000	0.00000 0.2014	-0.14411 0.0214	-0.14411 0.0039	0.13675 0.6841	0.18112 0.6706	0.06885 0.2521	-0.17252 0.60563	0.13809 0.6855
H.E.W	-0.13693 0.6073	0.65421 0.5342	1.00000 0.6060	0.2014 0.5526	0.100000 1.0000	0.00000 0.0695	0.78860 0.6059	-0.640234 0.0040	0.13675 0.6623	0.17745 0.6649	0.04019 0.9050	-0.12266 0.8956	0.01941 0.9758
A.U.H	0.26694 0.4274	-0.21312 0.5300	0.42942 0.5326	1.00000 0.6000	0.100000 1.0000	0.00000 0.0000	0.626093 0.0000	-0.16970 0.0000	0.19786 0.0000	0.13675 0.0000	0.12927 0.0000	0.09150 0.7890	0.13809 0.6855
S.Z.P	0.00000 1.0000	0.10000 1.0000	0.00000 0.0000	0.10000 1.0000	0.100000 1.0000	0.00000 0.0000	0.100000 0.10000	0.100000 0.10000	0.00000 0.10000	0.00000 0.10000	0.00000 0.10000	0.00000 0.10000	0.00000 0.6000
O.I.Z	0.06221 0.8558	-0.12411 0.7161	0.56956 0.6095	0.08055 0.0212	0.100000 1.0000	0.00000 0.0000	0.51145 0.1678	-0.41289 0.2003	0.62655 0.0391	0.21436 0.0413	-0.06111 0.0413	0.17875 0.5940	0.00000 0.7921
P.Y.H	0.05324 0.6164	-0.04359 0.5010	0.78860 0.5010	0.26093 0.4384	0.100000 1.0000	0.00000 0.0000	0.211045 0.01078	0.00000 0.01078	0.25872 0.4424	-0.12579 -0.7125	-0.14996 -0.6599	-0.11706 -0.1305	

UGR File # 157
W.Va. Geological & Economic Survey

NOV 1979

STATISTICAL ANALYSIS SYSTEM 6:32 WEDNESDAY, JANUARY 17, 1978

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C.R.	CORRELATION COEFFICIENTS / FROM > THE OTHER HOLE TO = 0.6 ± 0.1										ANK
	RAU	HEM	PUL	S2A	Q1Z	P1YR	CAL	BIL	URF	PLA	
-0.24977	-0.98429	-0.94724	-0.16970	0.99000	-0.41669	-0.92257	1.00000	0.92193	-0.69053	0.63160	-0.19977
0.39378	-0.98439	-0.94021	-0.61319	0.99000	-0.41669	-0.66659	0.99000	0.62610	-0.74152	0.63699	-0.64541
CAL											
-0.43102	0.13815	-0.57836	0.19723	0.99000	-0.13262	-0.69646	0.99193	1.00000	0.21132	-0.61634	-0.39470
-0.41349	0.64441	-0.64420	0.64420	0.99000	0.62655	0.25672	0.99053	0.65336	0.51326	0.51325	-0.22986
0.13942	-0.64420	0.14455	0.64455	0.99000	0.62191	0.4424	0.7912	0.65336	0.51326	0.51325	-0.1674
0.09495	0.64420	-0.64420	0.64420	0.99000	0.62191	0.4424	0.7912	0.65336	0.51326	0.51325	-0.24816
RAU											
0.05945	-0.17152	0.61014	-0.19568	0.99000	0.02336	0.12757	0.13993	0.61674	1.00000	0.35166	0.12148
0.16554	-0.12527	0.90666	0.56442	0.99000	0.9313	0.71257	0.63993	0.61674	0.63125	0.63000	0.25566
PUL											
0.29482	-0.58960	-0.13237	0.63827	0.99000	-0.02314	-0.14996	-0.15673	-0.39470	-0.27816	0.42666	0.29526
0.38448	-0.63960	-0.63960	0.63960	0.99000	0.62314	0.6559	0.64543	0.22986	0.64015	0.64889	0.63383
SID											
0.26449	-0.14609	0.01931	0.09150	0.99000	0.13905	-0.17166	-0.1399	-0.23164	-0.20950	0.15148	0.09000
0.09462	0.64455	-0.9758	0.7890	0.99000	0.53430	0.53165	0.63815	0.4427	0.55527	0.65656	0.50000
ANK											
0.09145	-0.61239	0.76352	0.60662	0.99000	0.98616	-0.95187	-0.76639	0.24423	-0.09072	0.04030	-0.09953
RAU											
0.09145	-0.61239	0.76352	0.60662	0.99000	0.98616	-0.95187	-0.76639	0.24423	-0.09072	0.04030	-0.09953

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CANADA

STATISTICAL ANALYSIS SYSTEM

0132 WEDNESDAY, JANUARY 17, 1979

CORRELATION COEFFICIENTS / FROM > 1st UNDER NO. 00000 / N = 11

QUANT	QUANT
QUARTZ	-0.1804 0.2474
FEXP	-0.54124 0.00853
HIL	0.22162 0.55116
CUD	-0.72065 0.1033
GYP	0.09748 0.1492
KAD	-0.12394 0.1171
HEM	0.76325 0.0060
AGB	0.23906 0.4390
SZP	0.10000 1.0000
ATZ	0.49725 0.1245
PVR	0.98614 0.0001
CAB	-0.65114 0.6004
OML	-0.76629 0.0059
OMT	0.21433 0.5224
PLA	-0.09072 0.3968
S1D	0.01910 0.9700
A1K	-0.09845 0.7722

UGR File # 157
W.Va. Geological & Economic Survey

Thinly Laminated Shale

SUBJECT TO
REVISION

VARIABLE	n	MEAN	STD DEV	SUM	MINIMUM		MAXIMUM
					MEAN	STD DEV	
SAMPF	13	1565.15484615	124.92864376	46347.00000000	3411.20600000	1770.20000000	
LNSG160	13	5.78464518	1.13566779	75.20000000	3.50000000	7.20000000	
LNSG500	13	3.21538462	0.53672798	41.80000000	2.00000000	4.20000000	
SUMF00	13	2.51923071	0.42281717	32.75000000	1.96000000	4.10000000	
BURKED0	13	2.59615385	0.5841305	33.75000000	2.51000000	2.69000000	
QATXDF13	13	2.62921677	0.05780161	34.18000000	2.51000000	2.71000000	
ENIGEN0	13	2.50538462	0.05511958	33.61000000	2.46000000	2.66000000	
PROBSETV	13	1.25538462	0.87020702	16.32000000	0	2.95000000	
GAMMA	13	237.10769231	29.19870036	3085.00000000	200.00000000	290.00000000	
ODARIZ	13	0.12615385	0.02693772	1.64000000	0.09000000	0.16000000	
FAP	13	0.01015481	0.002548003	0.13457353	0.00436185	0.01357118	
LLA,	13	0.38770184	0.08320847	7.38012390	0.38665892	0.65141105	
CIN	13	0.00331070	0.00383618	0.04301910	0	0.00991111	
GVP	13	0.01281410	0.00132676	0.01771113	0	0.01031004	
KAO	13	0.00084296	0.001030911	0.01053845	0	0.01095845	
HEH	13	0.00571014	0.00212597	0.07449181	0.00221950	0.01245159	
AJH	13	0.00188434	0.00466220	0.02449637	0	0.01411115	
SZS	13	0.00181851	0.00304905	0.02364062	0	0.00807455	
PF2	13	0.30692362	0.06365916	3.98476703	0.23512810	0.43075671	
PFH	13	0.05280546	0.00652350	0.68647614	0.04206218	0.06282867	
CAL	13	0.00642918	0.00929542	0.08355929	0	0.02664491	
00L	13	0.00202165	0.00543964	0.02629147	0	0.01874654	
QRT	13	0.00495514	0.00410244	0.03191676	0	0.01319109	
PLA	13	0.0299620	0.00492114	0.31156054	0.01742623	0.01414445	
SID	13	0.004999171	0.00848722	0.12949224	0	0.01224109	
AUT	13	0.00399162	0.00194989	0.01289162	0	0.00561650	

DATA
10000
1000
100
10
1

STATISTICAL ANALYSIS SYSTEM 8:32 WEDNESDAY, JANUARY 17, 1973

VARIANT	STDEV	SUM	MINIMA	MAXIMUM
GRDN	2.0121518	0.01556825	2.79239377	2.0343613

CORRELATION COEFFICIENTS / PHASE > INT UNITS HU=0 / N = 13

SAMPLE	L01G100	L01G500	SULFOR	MULKIN MATHADEN	LOGDEN POROSITY	GARNA	QUARTZ	EXP	INT.	COR
SAMPLE	1.00000	0.65254	-0.12691	-0.55480	-0.80912	-0.63109	0.14212	0.29254	-0.10775	0.09749
L01G100	0.65254	1.00000	0.60491	0.60008	0.60008	0.64433	0.4725	0.3321	0.7261	0.62285
L01G500	0.60491	0.60008	1.00000	0.43962	-0.43962	0.60004	0.25457	-0.23912	-0.62912	0.61034
L01G500	0.60008	0.43962	0.43962	1.00000	0.39093	0.39093	0.24284	0.17302	0.07201	0.17441
L01G500	0.39093	0.39093	0.39093	1.00000	0.1877	0.21438	0.57838	0.42420	0.57119	0.49514
SULFOR	0.1877	0.1877	0.1877	0.21438	1.00000	0.56716	0.28769	0.19152	0.18517	0.18517
SULFOR	0.1877	0.1877	0.1877	0.56716	1.00000	0.7405	0.74114	0.54441	0.49569	0.49569
GRDN	0.64433	0.64433	0.64433	0.64433	0.64433	1.00000	0.86693	0.82035	0.21606	0.07987
GRDN	0.64433	0.64433	0.64433	0.64433	0.64433	0.86693	1.00000	0.86693	0.79573	0.24669
GRDN	0.64433	0.64433	0.64433	0.64433	0.64433	0.82035	0.86693	1.00000	0.79573	0.40441
GRDN	0.64433	0.64433	0.64433	0.64433	0.64433	0.86693	0.79573	0.79573	1.00000	0.23261
GRDN	0.64433	0.64433	0.64433	0.64433	0.64433	0.79573	0.79573	0.79573	0.79573	1.00000
GARN	0.14212	0.14212	0.14212	0.14212	0.14212	0.14212	0.14212	0.14212	0.14212	0.14212
QUARTZ	-0.16715	-0.16715	-0.16715	-0.16715	-0.16715	-0.16715	-0.16715	-0.16715	-0.16715	-0.16715
EXP	-0.15869	-0.15869	-0.15869	-0.15869	-0.15869	-0.15869	-0.15869	-0.15869	-0.15869	-0.15869
GRDN	0.61141	0.61141	0.61141	0.61141	0.61141	0.61141	0.61141	0.61141	0.61141	0.61141

RECALCULATED DATA

STAKISTICAL ANALYSIS SYSTEM WEDNESDAY, JANUARY 17, 1973

8:12 WEDNESDAY, JANUARY 11, 1979

SOMMARIO DELLA COSTITUZIONE 11

CMB	CORRELATION COEFFICIENTS										QUARTZ	EXP	IT-1
	SAC-PFT	LASIG100	LASIG500	SULFUR	WILKINSON	MATTHEWS	LOGOEN	POROSITY	GAMMA	CHI			
0.21272	0.21472	0.21354	-0.21343	-0.21343	-0.44012	-0.55582	0.073592	-0.16064	0.145202	0.37752	-0.14411	-0.63734	0.16745
0.21273	0.21473	0.21355	-0.21344	-0.21343	-0.61012	-0.61012	0.073592	-0.16064	0.145202	0.37753	-0.24566	-0.62354	0.17116
-0.21294	-0.21474	-0.21374	-0.21374	-0.21374	0.207292	0.207292	-0.051920	-0.24207	-0.60553	-0.64410	-0.24207	-0.29094	0.23119
-0.21453	0.21591	0.21411	0.21411	0.21411	0.50599	0.50599	0.24524	0.4256	-0.60281	-0.61715	-0.64410	-0.35350	0.44312
0.19144	0.19144	0.19144	0.19144	0.19144	-0.57629	-0.57629	-0.198160	-0.123125	0.48797	0.60799	-0.45162	-0.22809	0.24536
0.19145	0.19145	0.19145	0.19145	0.19145	-0.61150	-0.61150	-0.198160	-0.123125	0.48797	0.60799	-0.45162	-0.22809	0.24536
0.11190	-0.01196	0.11196	0.11196	0.11196	0.41431	0.41431	0.204926	0.280129	0.020632	0.03894	-0.42977	-0.25024	0.40554
0.11191	-0.01197	0.11197	0.11197	0.11197	0.41432	0.41432	0.204926	0.280129	0.020632	0.03894	-0.42977	-0.25024	0.40554
0.34293	0.05110	-0.16227	-0.16227	-0.16227	-0.20692	-0.20692	-0.212412	-0.24341	0.27741	0.40866	-0.64080	-0.94802	0.14683
0.25144	0.06631	-0.59572	-0.59572	-0.59572	-0.49174	-0.49174	-0.24341	-0.27742	0.61744	0.6236	-0.61013	-0.68002	0.14683
-0.24232	-0.49736	-0.49736	-0.49736	-0.49736	-0.27472	-0.27472	-0.59507	-0.09040	-0.36024	-0.17462	-0.42203	-0.91301	-0.14077
-0.42253	0.12511	0.23621	0.23621	0.23621	0.4683	0.4683	0.090421	0.55497	0.22647	0.44310	-0.42203	-0.6464	0.14077
0.35043	0.12732	0.44291	0.44291	0.44291	-0.20522	-0.20522	-0.60109	-0.23809	0.38559	0.31425	-0.09298	-0.42816	0.44937
0.29249	0.12636	0.41614	0.41614	0.41614	-0.50122	-0.50122	-0.60109	-0.23809	0.38559	0.31425	-0.29557	-0.60823	0.44937
-0.39991	-0.49932	-0.49932	-0.49932	-0.49932	0.13119	0.13119	0.06411	0.05121	0.04801	0.05037	-0.76889	-0.46184	0.39467
-0.39990	-0.49932	-0.49932	-0.49932	-0.49932	0.13120	0.13120	0.06411	0.05121	0.04801	0.05037	-0.76889	-0.46184	0.39467
-0.04946	0.11874	0.11874	0.11874	0.11874	-0.49493	-0.49493	-0.30612	-0.11111	0.26951	0.09862	-0.32358	-0.70321	0.55996
-0.04947	0.11875	0.11875	0.11875	0.11875	-0.49494	-0.49494	-0.30612	-0.11111	0.26951	0.09862	-0.32358	-0.70321	0.55996
0.65089	0.05058	0.18629	0.18629	0.18629	0.11740	0.11740	0.12466	-0.09115	0.25706	0.19804	0.042754	0.29213	0.07758
0.65090	0.05058	0.18630	0.18630	0.18630	0.11741	0.11741	0.12466	-0.09115	0.25706	0.19804	0.042754	0.29213	0.07758
-0.17339	-0.09098	-0.26369	-0.26369	-0.26369	0.07409	0.07409	0.18059	0.29751	0.206128	-0.07779	-0.31086	-0.17153	-0.26066
-0.17340	-0.09099	-0.26370	-0.26370	-0.26370	0.07409	0.07409	0.18059	0.29751	0.206128	-0.07779	-0.31086	-0.17153	-0.26066
0.65632	-0.76910	-0.3842	-0.3842	-0.3842	0.0099	0.0099	0.5116	0.32355	0.20606	-0.07779	-0.31086	-0.17153	-0.26066
CMB	KAO	HEM	AWH	AWH	:24	:24	0.072	0.072	PLA	DOL	DOL	PLA	ANK

UGR File # 157

W.Va. Geological & Economic Survey

STATISTICAL ANALYSIS SYSTEM 0:32 WEDNESDAY, JANUARY 17, 1973

CORRELATION COEFFICIENTS / FROM > THE UNDER HORIZONTAL / N = 13													
	GAP	KAL	0E-4	AMH	S2W	012	HTR	CAL	DUL	GRT	PLA	S1D	ANK
S.DIST.MC	-0.43504	-0.62376	-0.31221	-0.36093	0.61114	-0.48414	0.22090	-0.21572	-0.44044	-0.32076	-0.1044	0.18629	
	-0.62619	-0.62341	-0.31221	-0.36093	0.61114	-0.48414	0.22090	-0.21572	-0.44044	-0.32076	-0.1044	0.5423	
WULE.DT.H	-0.15042	-0.24914	0.20114	-0.57829	0.14729	-0.20694	0.48325	-0.53420	0.73149	-0.63735	-0.50192	0.2262	
	-0.6053	-0.1323	0.5044	-0.57829	0.14729	-0.20694	0.48325	-0.53420	0.73149	-0.63735	-0.50192	0.9415	
A4.FACADE.H	-0.14461	-0.28392	0.19149	-0.65546	0.20756	-0.25442	0.59431	-0.66192	0.81441	-0.20600	-0.29645	0.5669	
	-0.62881	-0.28392	0.19149	-0.65546	0.20756	-0.25442	0.59431	-0.66192	0.81441	-0.20600	-0.29645	0.1246	
LUD.DEN	0.09376	0.05592	0.24224	-0.19831	0.26019	0.24344	0.55707	-0.23899	0.92519	0.45211	0.47234	0.3311	
	0.7606	0.69552	0.24224	-0.19831	0.26019	0.24344	0.55707	-0.23899	0.92519	0.45211	0.47234	0.9145	
PERCENT.VY	0.01811	-0.16064	-0.02149	-0.15212	0.04116	-0.37742	0.09040	-0.21899	-0.17812	-0.31453	0.45619	-0.02083	
	0.6093	0.60000	-0.02149	-0.15212	0.04116	-0.37742	0.09040	-0.21899	-0.17812	-0.31453	0.45619	0.25706	
GAC.MA	0.14312	0.18016	-0.24297	0.48777	-0.02063	0.02141	-0.36037	0.34559	0.08004	0.94865	0.2874	0.3965	
	0.6395	0.35195	-0.24297	0.48777	-0.02063	0.02141	-0.36037	0.34559	0.08004	0.94865	0.2874	0.10604	
MIN.GCFZ	-0.01145	0.17732	-0.60521	0.06787	0.05894	0.05894	0.05894	-0.14229	-0.05537	0.25113	0.25112	-0.02083	
	0.6165	0.2035	-0.60521	0.06787	0.05894	0.05894	0.05894	-0.14229	-0.05537	0.25113	0.25112	0.3965	
FAP	-0.50262	-0.14158	-0.54409	-0.42912	-0.42912	-0.00803	-0.0205	-0.09488	-0.70809	-0.26643	0.21635	-0.27596	
	-0.0774	0.21200	-0.54409	-0.42912	-0.42912	-0.00803	-0.0205	-0.09488	-0.70809	-0.26643	0.21635	0.4754	
LIL.	-0.53002	-0.65354	-0.29083	-0.43292	-0.23024	-0.98002	-0.9135	-0.42813	-0.76438	-0.10151	0.15969	-0.48801	
	0.0623	-0.60521	-0.29083	-0.43292	-0.23024	-0.98002	-0.9135	-0.42813	-0.76438	-0.10151	0.15969	0.29213	
C90	0.96212	0.462745	0.21119	0.22809	0.40324	0.41364	0.40407	0.49937	0.39467	0.5466	0.36640	0.42634	
	0.0001	0.61116	0.462745	0.21119	0.22809	0.40324	0.41364	0.40407	0.49937	0.39467	0.5466	0.7511	
G10	1.00000	0.12222	0.15987	0.11267	0.4793	0.40735	0.37319	0.36290	0.54239	0.62255	0.40314	0.9165	
	0.00000	0.12222	0.15987	0.11267	0.4793	0.40735	0.37319	0.36290	0.54239	0.62255	0.40314	0.9165	
R40	0.37324	0.00000	-0.12625	0.76811	-0.17920	0.58495	-0.19484	0.65344	-0.11161	0.42998	-0.19260	0.00114	
	0.2734	0.00000	-0.12625	0.76811	-0.17920	0.58495	-0.19484	0.65344	-0.11161	0.42998	-0.19260	0.61682	
III.C	0.37507	-0.12625	1.00000	-0.53369	0.32574	0.24592	0.26774	-0.4132	0.00001	0.00001	0.7273	0.07624	
	0.2050	-0.12625	1.00000	-0.53369	0.32574	0.24592	0.26774	-0.4132	0.00001	0.00001	0.7273	0.07624	
A.10	0.41267	0.78811	-0.05360	1.00000	-0.29144	0.59345	-0.27266	0.67229	0.09433	0.46532	0.57632	-0.22266	
	0.316	0.00000	-0.05360	1.00000	-0.29144	0.59345	-0.27266	0.67229	0.09433	0.46532	0.57632	0.46468	
S2.S	0.41782	-0.17920	0.32274	-0.26114	1.00000	0.19046	0.51119	-0.01439	0.52683	0.32292	-0.22307	-0.01177	
	0.6093	0.55880	0.32274	-0.26114	1.00000	0.19046	0.51119	-0.01439	0.52683	0.32292	-0.22307	0.96976	
IV.Z	0.40270	0.30427	0.24592	0.59345	0.19046	1.00000	0.01625	0.36965	0.42992	0.59660	0.15165	-0.41340	
	0.1725	0.0357	0.24592	0.59345	0.19046	1.00000	0.01625	0.36965	0.42992	0.59660	0.15165	0.1603	
V.YC	-0.01191	-0.49491	0.26774	-0.57349	0.51119	0.00000	1.00000	0.01625	0.36965	0.42992	0.59660	0.23614	
	0.0104	0.08550	0.26774	-0.57349	0.51119	0.00000	1.00000	0.01625	0.36965	0.42992	0.59660	0.74486	

UGR File # 157
W.Va. Geological & Economic SurveyMOUNTAIN CLOUDS
MOUNTAIN CLOUDS

UGR File # 157.
W.Va. Geological & Economic Survey

STATISTICAL ANALYSIS SYSTEM WEDNESDAY, JANUARY 17, 1979

CORRELATION COEFFICIENTS / PHNU > IRT UNDER H0: HU = 1.0										AUK	
GTR	KAU	WIL	ANH	SZB	WZ	PHN	CAL	HUN	GRT	PLA	SID
0.65293 0.62310	0.65334 0.61555	-0.64342 -0.61655	0.64341 0.60832	-0.60729 0.62209	0.64962 0.60832	-0.64729 0.62592	0.64467 0.60434	-0.61261 0.62592	0.64467 0.60434	-0.65644 0.60944	0.68166 0.61216
CAL	0.65555 0.62310	0.65334 0.61655	-0.64342 -0.62209	0.64341 0.60832	-0.60729 0.62592	0.64962 0.62592	-0.64729 0.62592	0.61261 0.62592	0.64467 0.60434	-0.65644 0.60944	0.68166 0.61216
WIL	0.65555 0.62310	0.65334 0.61655	-0.64342 -0.62209	0.64341 0.60832	-0.60729 0.62592	0.64962 0.62592	-0.64729 0.62592	0.61261 0.62592	0.64467 0.60434	-0.65644 0.60944	0.68166 0.61216
ANH	0.65555 0.62310	0.65334 0.61655	-0.64342 -0.62209	0.64341 0.60832	-0.60729 0.62592	0.64962 0.62592	-0.64729 0.62592	0.61261 0.62592	0.64467 0.60434	-0.65644 0.60944	0.68166 0.61216
SZB	0.65555 0.62310	0.65334 0.61655	-0.64342 -0.62209	0.64341 0.60832	-0.60729 0.62592	0.64962 0.62592	-0.64729 0.62592	0.61261 0.62592	0.64467 0.60434	-0.65644 0.60944	0.68166 0.61216
WZ	0.65555 0.62310	0.65334 0.61655	-0.64342 -0.62209	0.64341 0.60832	-0.60729 0.62592	0.64962 0.62592	-0.64729 0.62592	0.61261 0.62592	0.64467 0.60434	-0.65644 0.60944	0.68166 0.61216
PHN	0.65555 0.62310	0.65334 0.61655	-0.64342 -0.62209	0.64341 0.60832	-0.60729 0.62592	0.64962 0.62592	-0.64729 0.62592	0.61261 0.62592	0.64467 0.60434	-0.65644 0.60944	0.68166 0.61216
CAL	0.65555 0.62310	0.65334 0.61655	-0.64342 -0.62209	0.64341 0.60832	-0.60729 0.62592	0.64962 0.62592	-0.64729 0.62592	0.61261 0.62592	0.64467 0.60434	-0.65644 0.60944	0.68166 0.61216
HUN	0.65555 0.62310	0.65334 0.61655	-0.64342 -0.62209	0.64341 0.60832	-0.60729 0.62592	0.64962 0.62592	-0.64729 0.62592	0.61261 0.62592	0.64467 0.60434	-0.65644 0.60944	0.68166 0.61216
GRT	0.65555 0.62310	0.65334 0.61655	-0.64342 -0.62209	0.64341 0.60832	-0.60729 0.62592	0.64962 0.62592	-0.64729 0.62592	0.61261 0.62592	0.64467 0.60434	-0.65644 0.60944	0.68166 0.61216
PLA	0.65555 0.62310	0.65334 0.61655	-0.64342 -0.62209	0.64341 0.60832	-0.60729 0.62592	0.64962 0.62592	-0.64729 0.62592	0.61261 0.62592	0.64467 0.60434	-0.65644 0.60944	0.68166 0.61216
SID	0.65555 0.62310	0.65334 0.61655	-0.64342 -0.62209	0.64341 0.60832	-0.60729 0.62592	0.64962 0.62592	-0.64729 0.62592	0.61261 0.62592	0.64467 0.60434	-0.65644 0.60944	0.68166 0.61216
AUK	0.65555 0.62310	0.65334 0.61655	-0.64342 -0.62209	0.64341 0.60832	-0.60729 0.62592	0.64962 0.62592	-0.64729 0.62592	0.61261 0.62592	0.64467 0.60434	-0.65644 0.60944	0.68166 0.61216
GRT	0.65555 0.62310	0.65334 0.61655	-0.64342 -0.62209	0.64341 0.60832	-0.60729 0.62592	0.64962 0.62592	-0.64729 0.62592	0.61261 0.62592	0.64467 0.60434	-0.65644 0.60944	0.68166 0.61216

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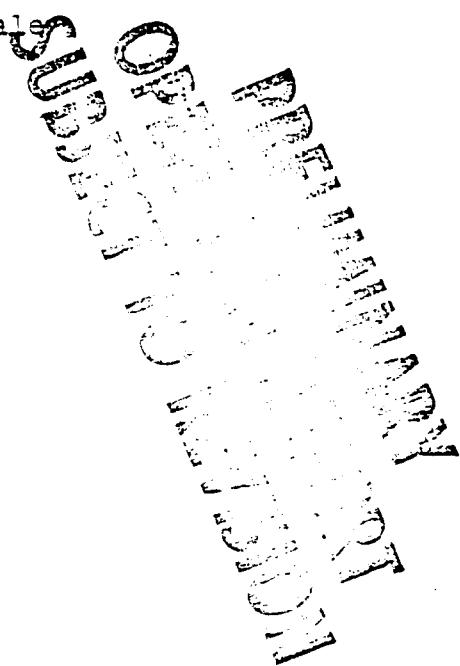
STATISTICAL ANALYSIS SYSTEM
9:32 WEDNESDAY, JANUARY 17, 1979

COEFFICIENTS / FROM > THE DATA ROTATION / N = 13

	CORR.
QUARTZ	-0.1170
K.F.P.	-0.0126 0.4143
IL.D.	-0.0532 0.8624
COO	-0.12066 0.6946
G.Y.P.	-0.13124 0.6643
KAO	-0.17149 0.5554
DLA	0.22224 0.4655
A.II	-0.31566 0.2934
S.L.A	0.3994 0.2975
O.II	-0.00354 0.9908
P.T.P.	0.04071 0.0063
C.A.I.	-0.26780 0.3402
W.H.	0.09221 0.7521
ORT	0.11443 0.7464
P.L.A	-0.04452 0.4877
S.I.D	0.25640 0.3900
A.O.K	0.14316 0.6419

UGR File # 157
W.Va. Geological & Economic Survey

Non-Banded Shale



STATISTICAL ANALYSIS SYSTEM

6:12 WEDNESDAY, JANUARY 17, 1979

VARIABLE	α	at AU	STD DEV	SUM	MINIMUM	MAXIMUM
SAMPLE	1.0	1603.69000000	136.92607454	36016.90000000	3423.10000000	1763.50000000
0.0516100	1.0	3.16000000	1.00465583	33.60000000	1.90000000	5.10000000
0.0516500	1.0	2.49000000	0.47246399	24.90000000	1.90000000	3.50000000
SOLID	1.0	4.20600000	0.78017377	12.06000000	0.25000000	2.50000000
0.0161000	1.0	2.10000000	0.02357023	27.00000000	2.61000000	2.75000000
0.0161000	1.0	2.12700000	0.02907844	27.27000000	2.69000000	2.79000000
0.0161000	1.0	2.62300000	0.07093816	26.29000000	2.46000000	2.71000000
0.0161000	1.0	0.98700000	0.12000132	9.87000000	0.37000000	1.48000000
0.0161000	1.0	208.50000000	39.4405321	2005.00000000	170.00000000	290.00000000
GARBA	1.0	0.11300000	0.04984420	1.32000000	0.05000000	0.21000000
0.0161000	1.0	0.01000941	0.00250581	0.10809407	0.00708339	0.01566459
FXP	1.0	0.58524792	0.10304139	5.85247924	0.35886100	0.70826526
11.1.	1.0	0.00110975	0.002485310	0.01709349	0	0.00714147
CIO	1.0	0.00153467	0.00337735	0.01534674	0	0.01074979
GYC	1.0	0	0	0	0	0
KAO	1.0	0	0	0.00314906	0.00839464	0
0.0161000	1.0	0.00544366	0.00174612	0.05643656	0.03562292	0.00959291
AGH	1.0	0.00356228	0.00436309	0.01270567	0	0.00050519
SZP	1.0	0.00121857	0.00267351	2.93415374	0.20695710	0.45875344
0VZ	1.0	0.29341537	0.07010430	0.25177831	0.00530797	0.04200360
PVA	1.0	0.02517783	0.01377745	0.08793913	0	0.0393436
CAL	1.0	0.00679391	0.00918730	0.05589978	0	0.04178846
OOL	1.0	0.00556939	0.01105755	0.01321102	0	0.00815980
0RT	1.0	0.00132110	0.00290531	0.29347362	0	0.04868214
PLA	1.0	0.029343736	0.015208508	0.4279471	0	0.1094058
SID	1.0	0.02421947	0.01125705	0.2687071	0	0.01749521
AOK	1.0	0.00226671	0.00559332	0	0	0

STATISTICAL ANALYSIS SYSTEM

8:32 WEDNESDAY, JANUARY 17, 1973

VARIANT	n	MEAN	STD DEV	SUM	MINIMUM	MAXIMUM
GROUT	10	2.7618959	0.01922511	27.6189587	2.70918556	2.63508205

CORRELATION COEFFICIENTS / PROB > 100 UNDER H0: H = 10

	SAMPLE	LUSIGOOD	SULFOR	BULKDENS	RATIODEN	LOGDEN	POROSITY	GAMMA	QUARTZ	EXP.	ILG.	COD
SAMPLE	1.00000 -0.26899 -0.24899 -0.23542 -0.67900 -0.20937 -0.07518 0.44485 0.02042 -0.37273 0.45270 0.06698 -0.49108	-0.60000 -0.4525 -0.5128 -0.6306 -0.56347 -0.5166 -0.49364 0.49554 -0.62606 0.10889 0.65541 -0.1495										
LUSIGOOD	0.26899 1.00000 0.24899 0.23542 0.67900 0.20937 0.07518 0.44485 0.02042 -0.37273 0.45270 0.06698 -0.49108	-0.26899 1.00000 0.24899 0.23542 -0.67900 -0.20937 -0.07518 0.44485 0.02042 -0.37273 0.45270 0.06698 -0.49108										
BULKDENS	0.24899 0.23542 1.00000 0.23542 0.67900 0.20937 0.07518 0.44485 0.02042 -0.37273 0.45270 0.06698 -0.49108	-0.23542 0.24899 1.00000 0.23542 0.67900 0.20937 0.07518 0.44485 0.02042 -0.37273 0.45270 0.06698 -0.49108										
RATIODEN	0.23542 0.23542 0.24899 1.00000 0.23542 0.67900 0.20937 0.07518 0.44485 0.02042 -0.37273 0.45270 0.06698 -0.49108	-0.23542 0.23542 0.24899 1.00000 0.23542 0.67900 0.20937 0.07518 0.44485 0.02042 -0.37273 0.45270 0.06698 -0.49108										
SULFOR	0.67900 0.24899 0.23542 0.24899 1.00000 0.23542 0.67900 0.20937 0.07518 0.44485 0.02042 -0.37273 0.45270 0.06698 -0.49108	-0.24899 0.67900 0.23542 0.24899 1.00000 0.23542 0.67900 0.20937 0.07518 0.44485 0.02042 -0.37273 0.45270 0.06698 -0.49108										
LOGDEN	0.20937 0.07518 0.02042 0.02042 0.44485 1.00000 0.23542 0.67900 0.20937 0.07518 0.44485 0.02042 -0.37273 0.45270 0.06698 -0.49108	-0.07518 0.20937 0.02042 0.02042 0.44485 1.00000 0.23542 0.67900 0.20937 0.07518 0.44485 0.02042 -0.37273 0.45270 0.06698 -0.49108										
POROSITY	0.07518 0.02042 0.44485 0.44485 0.02042 0.20937 1.00000 0.23542 0.67900 0.20937 0.07518 0.44485 0.02042 -0.37273 0.45270 0.06698 -0.49108	-0.02042 0.07518 0.44485 0.44485 0.02042 0.20937 1.00000 0.23542 0.67900 0.20937 0.07518 0.44485 0.02042 -0.37273 0.45270 0.06698 -0.49108										
GAMMA	0.44485 0.02042 -0.37273 0.45270 0.06698 -0.49108 0.20937 1.00000 0.23542 0.67900 0.20937 0.07518 0.44485 0.02042 -0.37273 0.45270 0.06698 -0.49108	-0.02042 0.44485 0.02042 -0.37273 0.45270 0.06698 -0.49108 1.00000 0.23542 0.67900 0.20937 0.07518 0.44485 0.02042 -0.37273 0.45270 0.06698 -0.49108										
EXP.	0.02042 0.02042 0.44485 0.44485 0.02042 0.20937 0.07518 0.20937 1.00000 0.23542 0.67900 0.20937 0.07518 0.44485 0.02042 -0.37273 0.45270 0.06698 -0.49108	-0.02042 0.02042 0.44485 0.44485 0.02042 0.20937 0.07518 0.20937 1.00000 0.23542 0.67900 0.20937 0.07518 0.44485 0.02042 -0.37273 0.45270 0.06698 -0.49108										
ILG.	0.45270 0.06698 -0.49108 0.06698 0.20937 0.07518 0.44485 0.44485 0.02042 1.00000 0.23542 0.67900 0.20937 0.07518 0.44485 0.02042 -0.37273 0.45270 0.06698 -0.49108	-0.06698 0.45270 0.06698 -0.49108 0.06698 0.20937 0.07518 0.44485 0.44485 0.02042 1.00000 0.23542 0.67900 0.20937 0.07518 0.44485 0.02042 -0.37273 0.45270 0.06698 -0.49108										
COD	0.06698 -0.49108 0.06698 0.20937 0.07518 0.44485 0.44485 0.02042 0.02042 0.44485 1.00000 0.23542 0.67900 0.20937 0.07518 0.44485 0.02042 -0.37273 0.45270 0.06698 -0.49108	-0.49108 0.06698 -0.49108 0.06698 0.20937 0.07518 0.44485 0.44485 0.02042 0.02042 1.00000 0.23542 0.67900 0.20937 0.07518 0.44485 0.02042 -0.37273 0.45270 0.06698 -0.49108										

RESULTS OF DATA

NOVEMBER 1972

STATISTICAL ANALYSIS SYSTEM 4:32 WEDNESDAY, JANUARY 17, 1976

UGR File # 157
W.Va. Geological & Economic Survey

CORRELATION COEFFICIENTS / PROB > THE UNDER HOLEMU=0 / N = 10													
	SALINE	LOS16500	LOS16509	SULFUR	HOLLOW	MATERIAL	LIGHT	MURDITY	CAPRA	QUARTZ	EXP.	Li.L.	COD
KAD	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.1.0000	0.1.0000	0.1.0000	0.1.0000	0.1.0000	0.1.0000	0.1.0000	0.1.0000	0.1.0000	0.1.0000	0.1.0000	0.1.0000	0.1.0000
ITEM	-0.21021	-0.04019	-0.15548	0.01918	0.04048	-0.23328	-0.34081	-0.62321	0.63481	0.59258	0.09043	-0.33091	0.10291
	0.5593	0.9112	0.6676	0.2628	0.5541	0.31352	0.05452	0.63481	0.63481	0.63481	0.63481	0.63481	0.63481
AHL	-0.32673	0.03587	-0.15110	-0.19841	0.24162	0.25664	-0.00467	0.06020	-0.53877	0.02604	-0.40524	0.18494	0.12110
	0.32676	0.9216	0.61510	0.3864	0.44192	0.52529	0.9898	0.8888	0.1061	0.9188	0.2513	0.64098	0.5260
SZN	-0.25890	0.91919	0.04668	0.37023	0.61917	0.50583	0.24635	-0.02663	-0.29482	-0.14437	-0.19279	-0.20198	0.63245
	0.4844	0.0021	0.0020	0.2923	0.0508	0.1863	0.4225	0.59417	0.40683	0.6902	0.51921	0.51559	0.63245
OTZ	-0.17609	-0.01691	0.0316	0.22606	0.13276	0.13666	0.06856	-0.12639	0.19744	0.19744	0.127203	-0.62830	0.19882
	0.6265	0.9632	0.32773	0.62539	0.62539	0.62539	0.62539	0.62539	0.62539	0.62539	0.62539	0.62539	0.62539
PYR	-0.41121	0.08403	0.24430	0.94734	-0.14121	-0.15704	-0.73113	-0.60057	0.67751	0.62345	0.1345	-0.37347	0.0703
	0.3178	0.81174	0.44739	0.00230	0.69171	0.31112	0.0206	0.0619	0.0314	0.0314	0.0314	0.2638	0.6303
CAL	0.17211	0.571382	0.39235	-0.12424	0.90226	0.56111	0.55904	0.51459	-0.51409	-0.56216	-0.1668	-0.40731	0.40731
	0.6340	0.0828	0.2526	0.2896	0.0052	0.00013	0.0929	0.1280	0.1280	0.1280	0.1280	0.1531	0.1531
IMI.	0.18834	-0.02622	-0.12049	-0.65671	-0.04898	-0.13516	-0.19982	-0.23663	0.20046	0.21295	-0.16141	-0.02767	-0.0198
	0.6063	0.9422	0.7402	0.7402	0.6931	0.7084	0.6826	0.5104	0.5767	0.5347	0.1795	0.0031	0.6918
DET	-0.1392	0.05638	0.04316	0.31385	0.96486	0.54494	0.3949	0.00009	-0.39732	-0.44295	-0.16498	-0.21280	0.62493
	0.5044	0.0016	0.0021	0.31458	0.03159	0.1034	0.3891	0.9999	0.3874	0.3874	0.1668	0.1531	0.1531
PLA	0.19071	-0.03941	-0.28453	0.03504	0.00408	-0.04676	-0.20511	-0.25294	0.61264	0.27300	0.32894	-0.47446	-0.05259
	0.5971	0.9113	0.4253	0.4253	0.6553	0.7903	0.5311	0.4808	0.6559	0.4454	0.36364	0.1659	0.08633
SID	0.19146	0.0022	0.35242	0.384102	0.75567	0.75962	0.49119	0.34658	-0.34066	-0.44659	-0.31551	0.2445	0.39119
	0.60194	-0.31449	0.16471	-0.14759	-0.04176	0.05961	0.11112	0.20989	0.613684	0.613684	0.604662	0.14291	-0.4505
AJK	0.52018	0.3449	0.6449	0.6449	0.9045	0.9045	0.8701	0.71113	0.5044	0.5265	0.15032	0.66937	0.4505
	0.11149	0.60523	0.60523	0.61153	0.4085	0.1060	0.24971	0.54138	0.19969	0.16423	0.22099	0.60377	0.14160
GHDEN	-0.11529	0.60616	0.60616	0.61153	0.61153	0.61153	0.61153	0.61153	0.5802	0.61623	0.25397	0.60645	0.6964
	0.2065	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
GYP	KAD	HEM	ANH	SZN	0.62	PYN	CAL	0.01	0.01	PLA	SID	ANK	
SAPPK	-0.25092	0.0000	-0.21021	-0.3116	-0.25090	-0.17609	-0.41176	0.17233	0.18081	-0.23990	0.19071	0.19746	0.50184
	0.24543	1.0000	-0.5539	0.3116	0.24543	0.62625	0.21378	0.50944	0.50944	0.50944	0.50944	0.50944	0.1394
LOS16100	-0.19577	0.0000	-0.3114	0.3114	0.19748	-0.19748	-0.1683	0.06103	0.51392	-0.36223	0.45659	0.60225	0.3446
	0.7775	0.9216	0.3114	0.3114	0.9216	0.9216	0.9216	0.9216	0.9216	0.9216	0.9216	0.9216	0.3449
LOS16500	-0.43112	0.0000	-0.15548	-0.15548	0.15548	0.15548	0.15548	0.15548	0.15548	0.15548	0.15548	0.15548	0.15548

STATISTICAL ANALYSIS SYSTEM
432 WEDNESDAY, JANUARY 17, 1979UGR File # 157
W.Va. Geological & Economic Survey

CORRELATION COEFFICIENTS / PRED > 101 WHICH HAVING N = 10												
	GYP	KAO	HEA	S24	OT2	PYN	CAL	UNI	INT	PLA	S10	ANK
SULFUR	-0.629624	0.500000	0.391641	-0.308114	0.37023	0.228329	0.41744	-0.47219	-0.1506	0.33185	0.08504	-0.01559
BULKDEN	0.63914	0.500000	0.404049	0.24367	0.49763	0.40506	0.12639	0.36771	0.2696	0.8153	0.27132	-0.961
MATHADEN	0.64684	0.500000	0.49118	0.64976	0.60506	0.12665	0.10172	0.00226	0.34816	0.60506	0.0115	-0.0476
LUDCEN	0.64134	0.500000	0.400000	0.23228	0.52663	0.20503	0.05945	-0.2504	0.66313	0.13576	0.54430	-0.75963
QUARTZ	0.67041	0.500000	0.340091	-0.304667	0.28632	0.1225	0.13739	0.1113	0.55904	0.10982	0.30649	0.40710
POROSITY	0.68231	0.500000	0.20542	0.20202	0.26646	0.10741	0.60577	0.51459	0.23663	0.00006	0.25294	0.34658
EXP	0.68581	0.500000	0.34448	-0.51677	0.51684	0.19784	0.29482	0.1083	0.51402	0.29946	0.30752	0.31066
GRNA	0.63443	0.500000	0.6498	-0.1081	0.4083	0.6032	0.6751	0.1245	0.5787	0.31254	0.1594	0.9265
HEA	-0.13882	0.500000	0.5352	0.3098	0.1225	0.13739	0.1113	0.55904	0.10982	0.30649	0.40710	0.31113
OT2	0.60241	0.500000	0.20542	0.20202	0.26646	0.10741	0.60577	0.51459	0.23663	0.00006	0.25294	0.34658
PYN	-0.20549	0.500000	0.34448	-0.51677	0.51684	0.19784	0.29482	0.1083	0.51402	0.29946	0.30752	0.31066
CAL	-0.62316	0.500000	0.330001	0.18664	0.20188	0.092893	-0.37337	-0.48731	-0.82767	-0.21280	-0.47446	-0.46559
UNI	-0.63316	0.500000	0.330001	0.6351	0.6096	0.5159	-0.0054	-0.2878	-0.60531	-0.65550	-0.17179	-0.1954
INT	0.54246	0.500000	0.19991	0.12730	0.62264	0.19341	-0.07803	0.46303	-0.01128	0.62499	-0.02258	-0.27007
KAO	0.60771	0.500000	0.7614	0.62264	0.59524	0.5303	0.52924	0.631769	0.91738	0.6533	0.8853	-0.4505
GYP	1.00000	0.500000	0.31973	0.50939	0.24463	0.06816	-0.23094	0.05103	-0.4544	0.2958	0.25613	-1.4096
HEA	0.31921	0.500000	0.60000	0.33194	0.5126	0.8516	0.5214	0.6843	0.9009	0.5234	0.4110	-0.6358
OT2	0.31926	0.500000	0.60000	0.33193	0.5126	0.8516	0.5214	0.6843	0.9009	0.5234	0.4110	-0.6358
PYN	0.05919	0.500000	0.33893	1.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
AHL	0.68703	0.500000	0.33994	1.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
S74	-0.22445	0.500000	0.19122	-0.05182	1.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
OT2	0.064516	0.500000	0.25496	-0.20586	0.33195	1.00000	0.40421	0.00000	0.00000	0.00000	0.00000	0.00000
PYN	-0.23064	0.500000	0.3049	-0.41527	0.60492	1.00000	0.2454	0.00000	0.00000	0.00000	0.00000	0.00000

STATISTICAL ANALYSIS SYSTEM
8:32 WEDNESDAY, JANUARY 17, 1979

UGR File # 157
W.Va. Geological & Economic Survey

CORRELATION COEFFICIENTS / PROB > IRI UNDER H0: H = 10												
	RAW	ITEM	AMH	S2H	OT2	PH	CAT.	HGT	OT1	PLA	SID	ANK
CAL.	-0.05001 0.6843	0.00000 -0.63453	0.23193 0.64731	0.49656 0.1443	0.16885 0.6013	-0.40435 -0.2465	1.00000 0.0000	0.16988 0.6409	0.54263 0.1055	-0.08297 0.68167	0.92943 0.0001	-0.03285 0.9282
PHL.	-0.04544 0.9088	0.00000 0.5223	0.23017 0.3636	-0.12216 -0.6673	-0.04497 0.0006	0.98723 0.4167	0.28978 0.6409	0.16048 0.9451	0.39798 0.2559	0.39798 0.6701	0.39798 0.5913	-0.19294
OT1	-0.22958 0.55234	0.00000 0.10000	0.18662 0.6017	-0.18662 0.9603	0.99187 0.0001	0.02424 0.9431	0.03222 0.8861	0.54107 0.6451	0.02540 1.00000	0.29958 0.4004	0.46575 0.1749	-0.29493 0.5701
PLA	0.73515 0.47430	0.00000 0.10000	0.32531 0.6033	-0.54624 -0.1021	-0.36549 0.1903	0.32539 0.1892	0.45247 0.3589	-0.08327 0.4004	0.19708 0.2559	-0.29958 0.4004	0.0205 0.9042	0.15331 0.6724
SID	-0.17139 0.61359	0.00000 0.10000	0.17646 0.6256	0.33435 0.3435	0.41006 0.2392	0.04952 0.9132	0.31160 0.3608	0.92941 0.8001	0.29739 0.8201	0.46375 0.1749	0.04205 0.3682	0.00000 0.9086
ANK	-0.14095 0.6977	0.00000 0.10000	0.4913 0.8943	-0.36792 0.7953	-0.20053 0.5186	0.24096 0.5024	0.06033 0.0512	0.03285 0.9282	-0.03285 0.5933	-0.19294 0.5701	0.00000 0.9086	0.00000 0.6724
GHT H	-0.42124 0.2254	0.00000 0.10000	0.27866 0.4356	0.09286 0.9938	0.43111 0.2105	0.28261 0.1546	0.40280 0.1251	0.51892 0.55062	0.28261 0.1251	0.46381 0.33860	0.46381 0.61110	0.46381 0.8949
GRADEN												
SAMPLE	-0.11443 0.7529											
LOSS1000	0.05053 0.0636											
LOSS5000	0.22944 0.4153											
SURF W	0.29411 0.4065											
BULKDEN	0.54138 0.1060											
NATURDEN	0.38138 0.2769											
LNGDEN	-0.19969 0.5602											
POROSITY	-0.16424 0.6503											
GRAMA	0.42990 0.5397											

SEARCHED
INDEXED
FILED
NOV 1 1979

STATISTICAL ANALYSIS SYSTEM
4:32 WEDNESDAY, JANUARY 17, 1979

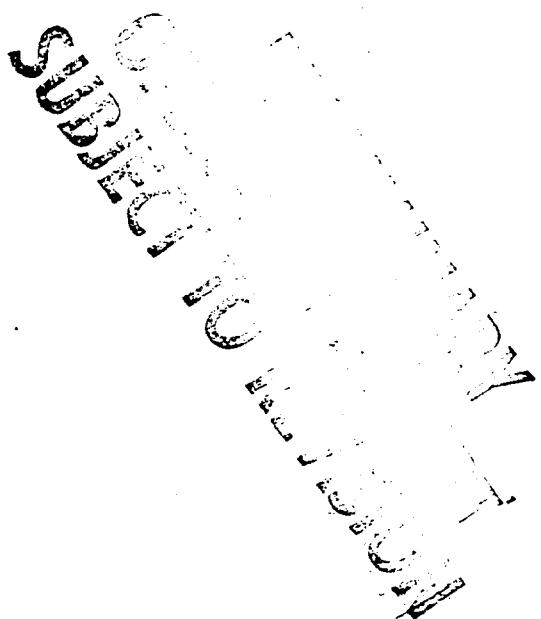
CORRELATION COEFFICIENTS / PION > TAU UNDER ROTATION / N = 10

	GROUT
QUARTZ	0.07111 0.64338
F.M.P.	-0.26910 0.41748
FLA.	-0.60377 0.66445
CDO	0.14169 0.69644
GYP	-0.42123 0.2254
KAI	0.00009 1.0000
HT.P.	0.27864 0.43556
AIR	0.00262 0.99338
SZA	0.42371 0.62165
HT.Z.	0.26264 0.4288
P1K	0.48280 0.1546
CAL	0.51802 0.1251
DOI.	0.24890 0.5062
ORT	0.46384 0.41669
PLA	0.54927 0.3366
SIO	0.67246 0.63310
AIR	0.04611 0.6989

UGR File # 157

W. Va. Geological Survey

Banded Shale



STATISTICAL ANALYSIS SYSTEM

WEDNESDAY, JANUARY 17, 1979

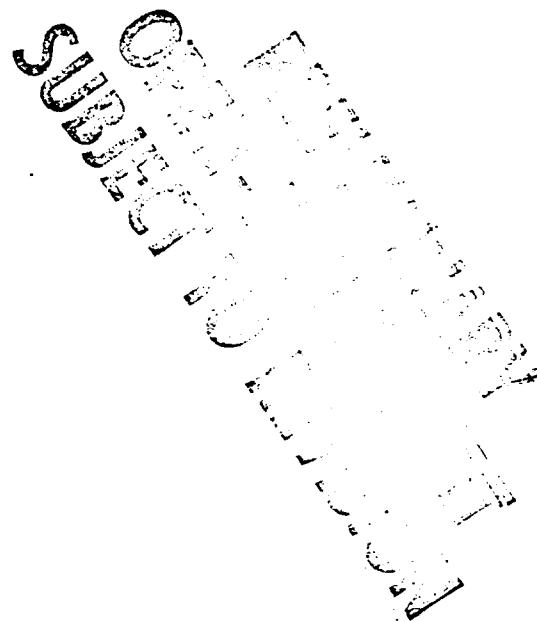
6:12

JGR File # 157
W.Va. Geological & Economic Survey

VARIABLE	F	MEAN	STANDARD DEVIATION	MEANING VALUE	MEANING VALUE	STD ERROR OF MEAN	SUM	VARIANCE	C.V.
SAPPHIRE	351.4	-4.2500000	1.455	-0.0000000	161.2	-1000000.0	1405	700000.0	1.930
TASSELITE	1.4	-4.0000000	0.185	1.41	3	-2000000.0	0.0102819	-6.000	5.770
LUDLUM	1.4	-2.0000000	0.621	2.527	2	-1000000.0	0.0101912	-6.000	1.412
SULFOR	1.4	-2.6750000	0.441	1.131	1	-1000000.0	0.0100660	-6.000	1.150
HULLIKER	2.7	-2.2500000	0.317	5.936	2	-700000.0	0.0101892	6.000	1.459
MATIGOR	2.7	-2.4750000	0.301	5.830	2	-700000.0	0.0101892	6.000	1.459
LOGITE	2.7	-0.9000000	0.300	6.530	2	-500000.0	0.0066241	6.000	1.900
POMONITE	2.7	-0.9000000	0.300	6.530	2	-500000.0	0.0066241	6.000	1.900
GAMMA	18.25	-4.4850000	1.80	-0.0000000	220	-1000000.0	0.0000000	111.1	1.129
QUARTZ	6	-1.7250000	0.4494660	-0.6619390	20	-1000000.0	0.0000000	3.000	34.591
FYR	0.010	2.597	0.001395	0.0017421	0	-1000000.0	0.0000000	0.0000000	15.391
ALL	0.578	1.012	0.0412972	0.4611081	0	-1000000.0	0.0000000	0.0000000	151.811
CuO	0.001	1.496	0.0013948	0.0000000	0	-1000000.0	0.0000000	0.0000000	151.811
GrP	0.001	1.591	0.0009316	0.0000000	0	-1000000.0	0.0000000	0.0000000	151.811
KAl	0.001	0.000	0.0000000	0.0000000	0	-1000000.0	0.0000000	0.0000000	151.811
HeK	0.001	2.419	0.0000000	0.0000000	0	-1000000.0	0.0000000	0.0000000	151.811
A.III	0.001	2.423	0.0000000	0.0000000	0	-1000000.0	0.0000000	0.0000000	151.811
S.Z.I	0.001	2.424	0.0000000	0.0000000	0	-1000000.0	0.0000000	0.0000000	151.811
S.Y.Z	0.001	2.427	0.0000000	0.0000000	0	-1000000.0	0.0000000	0.0000000	151.811
CAL	0.001	4.666	0.0051313	0.0000000	0	-1000000.0	0.0000000	0.0000000	151.811
hol	0.001	1.972	0.0002639	0.0000000	0	-1000000.0	0.0000000	0.0000000	151.811
onef	0.001	1.618	0.0002196	0.0000000	0	-1000000.0	0.0000000	0.0000000	151.811
pta	0.001	1.618	0.0002062	0.0000000	0	-1000000.0	0.0000000	0.0000000	151.811
AsP	0.001	4.404	0.0005028	0.0000000	0	-1000000.0	0.0000000	0.0000000	151.811
AsK	0.001	4.228	0.02503472	0.0000000	0	-1000000.0	0.0000000	0.0000000	151.811
GrGe.n	2.814	1.228	0.0000000	0.0000000	0	-1000000.0	0.0000000	0.0000000	151.811

11.277291

Siltstone



STATISTICAL ANALYSIS SYSTEM 6412 WEDNESDAY, JANUARY 17, 1979

VARIABLE	N	MEAN	STANDARD DEVIATION	MINIMUM VALUE	MAXIMUM VALUE	STD. ERROR OF MEAN	SUM	VARIANCE	C.V.
SAMPLE	1556	-55000000.0	104.617261.6	3479.0000000	1614.1000000	17.3200000	7111.1000000	12628.002000	1.084
LOSSIG10	2	1.656600000	0.070166.8	1.600000000	1.600000000	0.0500000	3.3000000	0.0050000	4.245
LOSSIG20	2	1.600000000	0.422640.7	1.550000000	1.600000000	0.1800000	3.1600000	0.1800000	23.570
LOSSIG30	2	1.600000000	0.212320.3	1.520000000	1.600000000	0.1000000	3.1200000	0.0450000	58.926
SURF9	2	2.650000000	0.024244.7	2.600000000	2.600000000	0.0120000	5.1200000	0.0090000	51.067
WALL9	2	2.690000000	0.024242.4	2.600000000	2.600000000	0.0120000	5.1800000	0.0090000	50.526
ATRAXIN	2	2.675000000	0.024232.0	2.600000000	2.600000000	0.0120000	5.1500000	0.0090000	50.793
LOGON9	2	2.675000000	0.024232.0	2.600000000	2.600000000	0.0120000	5.1500000	0.0090000	50.793
POROS11	2	1.480000000	1.50716.9	1.400000000	1.400000000	0.1000000	2.9600000	2.46400.0	1.662
GARN1A	2	1.65.0000000	0.445000.0	1.600000000	1.600000000	0.0200000	3.2000000	0.0060000	3.022
QUARTZ	2	0.0096040	0.134560.9	0.0096040	0.0096040	0.0050000	0.0182000	0.0000000	0.0000000
E4P	2	0.291629.7	0.024189.4	0.205307.6	0.321521.7	0.017592.3	0.559625.9	0.0000000	0.0000000
E6L	2	0.063074.5	0.0064189.4	0.0000000	0.061946.6	0.003204.9	0.1000000	0.0000000	0.0000000
CJO	2	0.005966.5	0.000737.0	0.0000000	0.000932.9	0.000304.5	0.0000000	0.0000000	0.0000000
GYP	2	0.060949.0	0.007370.4	0.0000000	0.055713.9	0.001974.6	0.0000000	0.0000000	0.0000000
KAL	2	0.031218.8	0.038800.6	0.0000000	0.052713.7	0.005969.4	0.0000000	0.0000000	0.0000000
HEH	2	0.002419.8	0.003086.4	0.0000000	0.0000000	0.000564.7	0.0000000	0.0000000	0.0000000
AHH	2	0.034924.9	0.004924.5	0.003472.9	0.005637.0	0.000645.0	0.0000000	0.0000000	0.0000000
S2P	2	0.416456.2	0.042544.4	0.042544.4	0.426216.3	0.013642.5	0.0000000	0.0000000	0.0000000
Q1Z	2	0.016455.5	0.002321.2	0.004703.4	0.009247.6	0.000227.2	0.0000000	0.0000000	0.0000000
PYR	2	0.0016455.8	0.006205.6	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
CAL	2	0.011358.7	0.016007.9	0.0000000	0.0000000	0.002151.7	0.0000000	0.0000000	0.0000000
QUT	2	0.003148.1	0.004677.6	0.0000000	0.0000000	0.006429.6	0.0000000	0.0000000	0.0000000
P1A	2	0.051215.5	0.00412.2	0.0000000	0.0000000	0.000307.5	0.0000000	0.0000000	0.0000000
S1D	2	0.045038.9	0.00312.0	0.0000000	0.0000000	0.00066664.0	0.0000000	0.0000000	0.0000000
AK	2	0.045038.9	0.00312.0	0.0000000	0.0000000	0.0009097.6	0.0000000	0.0000000	0.0000000
GRDN	2	2.714251.7	0.010263.1	2.701878.6	2.727371.6	0.012746.5	5.429250.3	0.0000000	0.0000000

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W.VA. GEOLOGICAL & ECONOMIC SURVEY

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APPENDIX D

RAW DATA FOR ALL SAMPLES

STATISTICAL ANALYSIS SYSTEM 1245 FRIDAY, JANUARY 12, 1979

UGR File # 157
W.Va. Geological & Economic Survey

	L	H	S	B	A	P	C	G	T	F	I	C	G	G	K	H	K	H	
4	S	I	S	B	A	P	C	G	T	F	I	C	G	G	K	H	K	H	
5	A	C	S	B	A	P	C	G	T	F	I	C	G	G	K	H	K	H	
6	H	E	F	D	D	F	E	H	F	P	E	C	G	G	K	H	K	H	
7	S	F	E	H	H	H	E	V	A	E	P	C	G	G	K	H	K	H	
8	1	1472.0	1.9	2.5	0.21	2.63	2.68	3.69	2.39	1.90	0.53	S	0.008094226	0.3195729	0.00619489	0.00000000	0.0100933	0.05597241	0.0052710
9	2	1634.1	1.9	2.5	0.21	2.63	2.68	3.69	2.39	1.90	0.53	P	0.00944223	0.3195729	0.00619489	0.00000000	0.0100933	0.05597241	0.0052710

	A	H	S	B	A	P	C	G	T	F	I	C	G	G	K	H	K	H
4	S	H	S	B	A	P	C	G	T	F	I	C	G	G	K	H	K	H
5	A	H	S	B	A	P	C	G	T	F	I	C	G	G	K	H	K	H
6	1	0.0000000	0.00446172	0.4127476	0.0127435	0.480176	0.00976716	0.00000000	0.00000000	0.00000000	0.0459221	0.00666644	0.00000000	0.00000000	2.72237	0.00000000	2.70188	0.00000000
7	2	0.0056377	0.0056377	0.0056377	0.0056377	0.0056377	0.0056377	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000

	L	H	S	B	A	P	C	G	T	F	I	C	G	G	K	H	K	H
1	3455.0	1.2	1.1	2.44	2.70	2.75	2.65	1.62	2.74	0.17	P	0.0000215	0.460107	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000
2	3491.6	1.6	1.5	2.01	2.30	2.16	2.65	2.02	1.90	0.06	S	0.0000236	0.655662	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000
3	3491.0	1.6	1.5	2.01	2.30	2.16	2.65	2.02	1.90	0.06	S	0.0000239	0.644522	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000
4	3491.1	1.6	1.5	2.01	2.30	2.16	2.65	2.02	1.90	0.06	S	0.0000243	0.652471	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000
5	3612.1	1.3	2.1	2.71	2.71	2.71	2.65	0.32	2.10	0.16	P	0.0000243	0.524081	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000
6	3710.6	2.6	2.0	0.63	2.71	2.72	2.65	0.32	2.30	0.06	A	0.0000240	0.530045	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000
7	3751.3	6.2	3.1	2.68	2.68	2.68	2.65	1.14	3.60	0.13	A	0.0000240	0.530045	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000
8	3751.3	6.2	3.1	2.68	2.68	2.68	2.65	1.14	3.60	0.13	A	0.0000240	0.530045	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000
9	0	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	PLA	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000
0	0	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	PLA	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000
1	0	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	PLA	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000
2	0	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	PLA	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000
3	0	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	PLA	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000
4	0	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	PLA	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000
5	0	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	PLA	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000
6	0	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	PLA	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000
7	0	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	PLA	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000
8	0	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	PLA	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000
9	0	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	PLA	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000
0	0	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	PLA	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000

MOLINE

STATISTICAL ANALYSIS SYSTEM 12145 FRIDAY, JANUARY 12, 1979 2

STATISTICAL ANALYSIS SYSTEM 1245 FRIDAY, JANUARY 12, 1979 3

OHS SAMPLE	LDS1G100			LDS1G500			SULFUR BULKDEN MATRIX			LUDDEIN PURITY			QUARTZ WT%			EXP			ILL.			CH4			GYP		
	LIT	TYPE	4	LIT	TYPE	4	LIT	TYPE	4	LIT	TYPE	4	LIT	TYPE	4	LIT	TYPE	4	LIT	TYPE	4	LIT	TYPE	4	LIT	TYPE	4
22	1461.0	3.5	2.4	2.46	2.76	2.61	2.62	2.70	2.65	2.90	3.15	5	4.17	5	4.12	4.09	4.06	5.72609	0.572609	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000		
23	1460.5	3.5	2.4	2.41	2.70	2.65	2.65	2.66	2.56	2.80	3.15	5	4.18	5	4.06	4.075	4.56239	0.56239	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
24	1460.5	3.5	2.4	2.41	2.69	2.65	2.56	2.66	2.69	2.90	3.15	5	4.18	5	4.06	4.075	4.29690	0.62391	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
25	1461.0	3.5	2.4	2.42	2.70	2.65	2.75	2.66	2.69	2.90	3.15	5	4.18	5	4.06	4.075	4.52247	0.52247	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
26	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	4.61077	0.61077	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
27	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	4.61451	0.61451	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
28	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	4.64266	0.64266	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
29	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	4.65493	0.65493	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
30	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	4.68730	0.68730	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
31	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	4.71019	0.71019	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
32	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	4.74522	0.74522	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
33	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	4.78484	0.78484	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
34	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	4.81587	0.81587	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
35	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	4.84684	0.84684	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
36	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	4.87747	0.87747	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
37	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	4.90801	0.90801	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
38	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	4.93851	0.93851	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
39	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	4.96852	0.96852	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
40	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	5.00268	0.00268	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
41	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	5.03282	0.03282	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
42	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	5.06395	0.06395	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
43	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	5.09509	0.09509	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
44	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	5.12621	0.12621	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
45	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	5.15733	0.15733	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
46	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	5.18845	0.18845	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
47	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	5.21957	0.21957	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
48	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	5.25069	0.25069	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
49	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	5.28181	0.28181	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
50	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	5.31293	0.31293	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
51	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	5.34405	0.34405	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
52	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	5.37517	0.37517	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
53	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	5.40629	0.40629	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
54	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	5.43741	0.43741	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
55	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	5.46853	0.46853	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
56	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	5.50065	0.50065	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
57	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	5.53177	0.53177	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
58	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	5.56289	0.56289	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
59	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	5.59401	0.59401	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
60	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	5.62513	0.62513	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000	0.0000000			
61	1461.0	3.5	2.4	2.41	2.69	2.65	2.74	2.66	2.71	2.90	3.15	5	4.18	5	4.06	4.075	5.65625	0.6									

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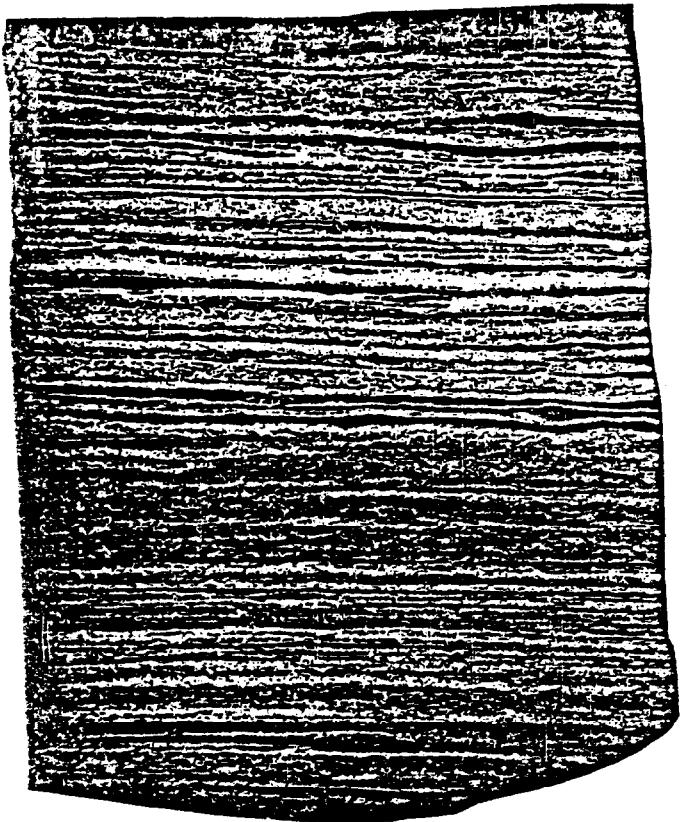
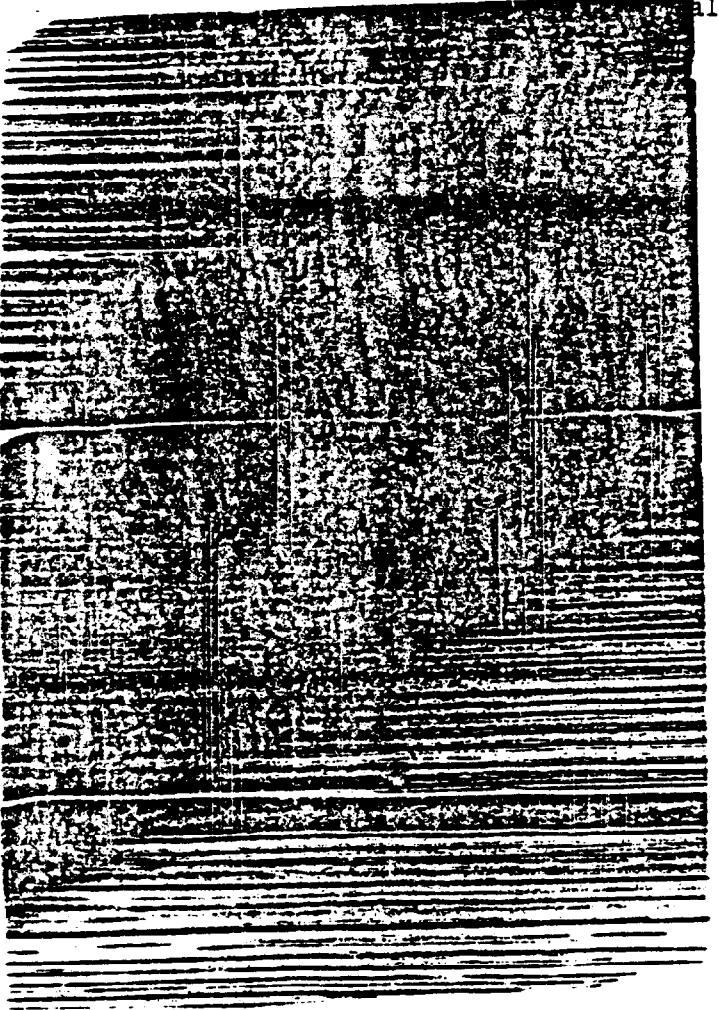
STATISTICAL ANALYSIS SYSTEM 1245 FRIDAY, JANUARY 12, 1979 4

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APPENDIX E
REPRESENTATIVE ILLUSTRATIONS

LITHOTYPES

1. Thinly Laminated Shale Type (A) Radiograph positive print - depth 3699.5 (1x); (B) negative-print image of thin section - depth 3411.2 (5x). Greater continuity of laminae shown in radiograph is possibly explained by greater thickness of sample slab (2 mm for radiograph, 20 μ m for thin section). Darker laminae in radiographs reflect increasing concentrations of pyritic matter. These appear as lightest tones on direct negative print image of thin sections. Wispy silt streaks appear as dark laminae in B. Burrows and traction features are generally lacking in finely laminated shale type. This lithotype comprises about 25% of the samples interval. We believe the lateral continuity provided by this fabric permits better migration of gas through available pore space in the pyritic organic laminae, the silty lenses and laminae, and perhaps through the illite-quartz matrix itself. The higher organic content of these shales may also permit greater amounts of adsorbed gas to exist within this lithotype. Most samples of thinly laminated shale were not in the gas producing zone indicated by the temperature log, but many pieces of core were removed prior to sampling by us. Organic rich shale types (thinly laminated and lenticularly laminated) with moderate to high lateral fabric continuity coupled with a favorable petrographic fracture type is tentatively concluded to explain the extremely high production of Jac 1369.

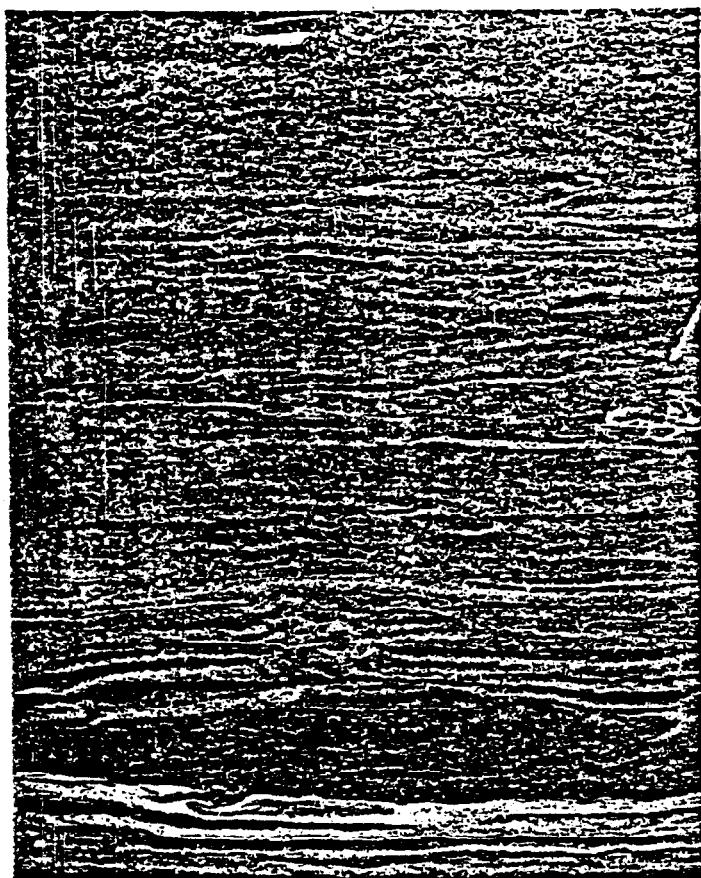
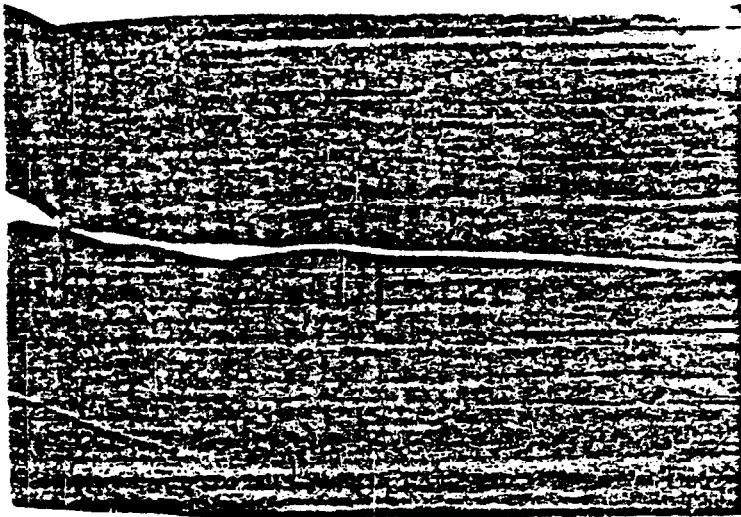


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SUSPENDED
REVIEW
NOTICE
LAW

Summary
of
thin
section
lithology

2. Lenticularly Laminated Shale Type (A) Positive print from X-radiograph-depth 3782 (1x); (B) Negative-print image of thin section-depth 3605 (5x). Lenticularly laminated shale shows less lateral continuity than thinly laminated shale but the linear fabric may enhance gas migration through available pore space if porosity increasing pyritic wisps (dark streaks on A) and appreciable organic matter are present. Organic content of lenticularly laminated shale (4.7%) is slightly less than that of thinly laminated shales (5.8%) in Jac 1369. This lithotype is more abundant in the lower portion of the core composing 25% of the interval and is probably associated with productivity due to favorable petrographic fracture types and its high organic matter content.

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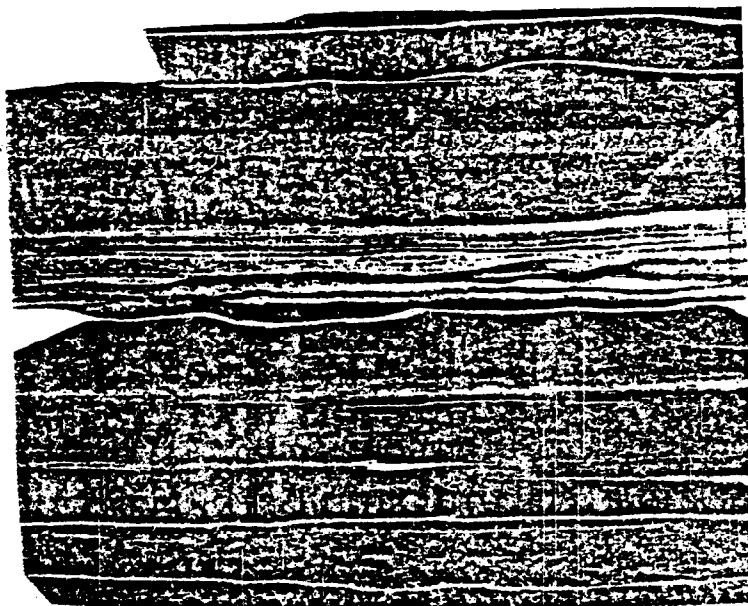
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Open to Inspection
SUBJECT TO EXAMINATION

3. Banded Shale Type (A) Radiograph positive - depth 3641 (1x);
(B) Negative-print image of thin section - depth 3641 (5x). Banded shales comprise 12% of the sample interval and are more abundant in the upper and lower portion of the interval. Individual bands commonly show internal structures such as laminations. Organic matter content of adjacent bands can vary greatly.

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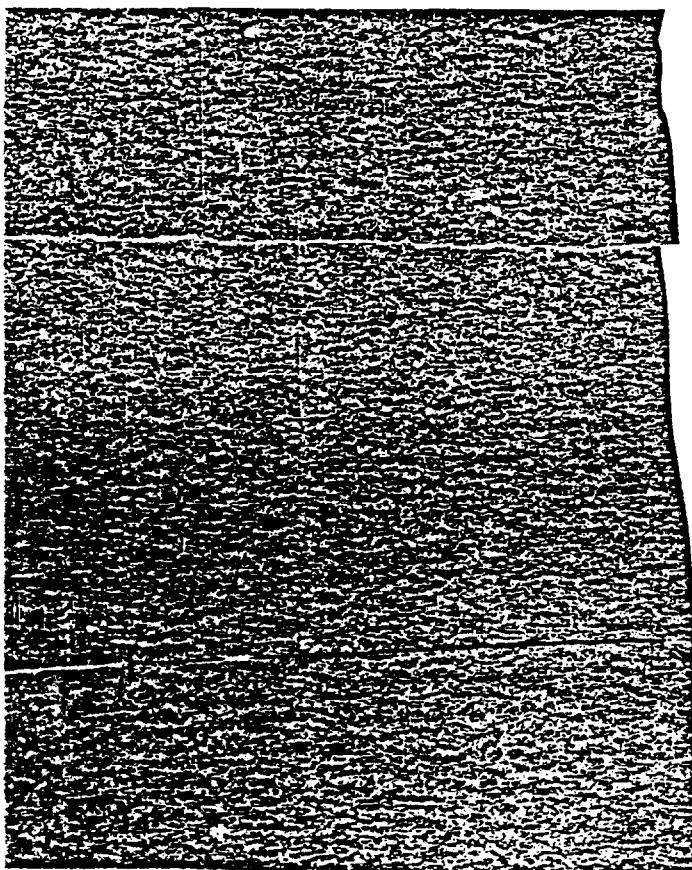
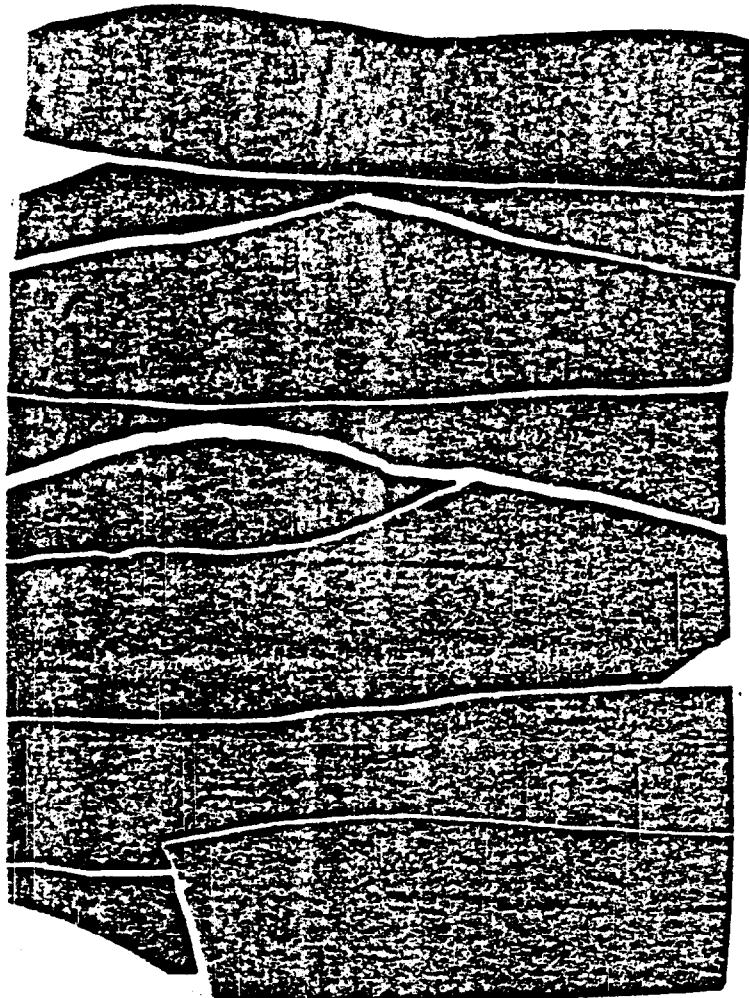
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**PROTESTANT CHURCH OF
THE UNITED STATES**

Subject
27
only

4. Non-banded Shale Type (A) Positive print from X-radiograph - depth 3754 (1x). (B) Negative print from thin section - depth 3455 (5x). Particles of silt, pyrite, and organic matter are dispersed and not concentrated so as to produce a linear fabric. Burrowing, particularly evident in A is responsible in many cases for destruction of such fabric and conversion of laminated types toward nonbanded. Some non-banded shales show little evidence of bioturbation (B) and perhaps represent an original non-laminated fabric reflecting extremely rapid deposition. Non-banded shales comprise 25% of the cored interval.

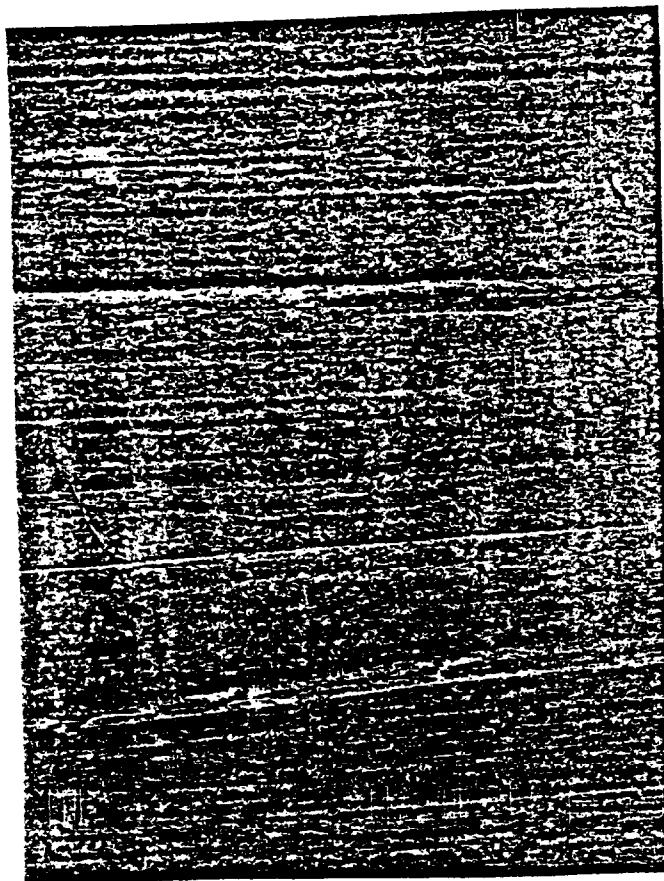
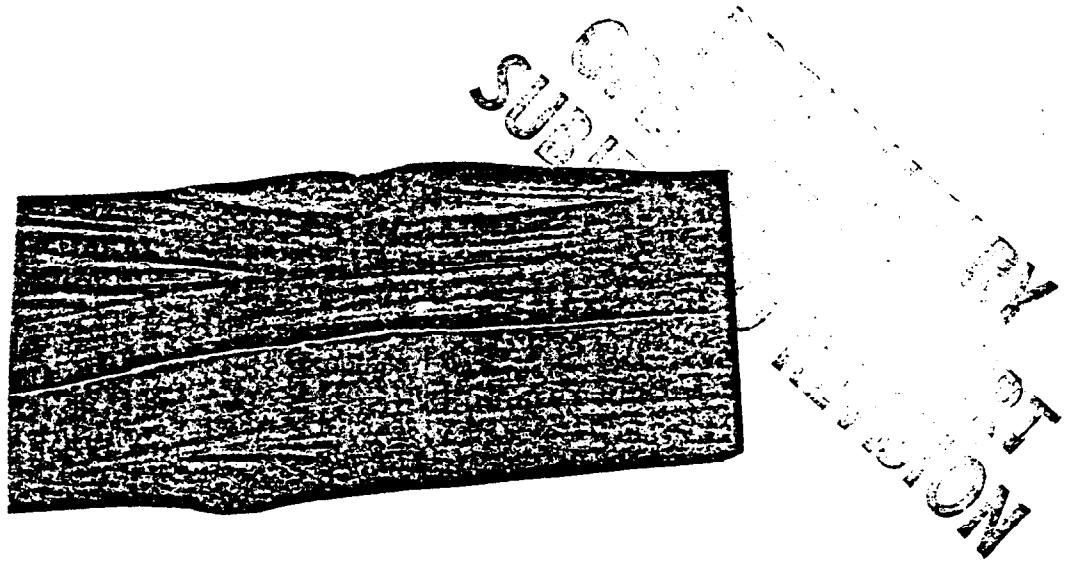


Subsamples
No. 1
100

Oil Shale
Sedimentology
Sedimentology

5. Siltstones (A) Positive print from X-radiograph - depth 363⁴ (1x). (B) Negative-print image of thin section - depth 363⁴ (5x). Siltstones comprise only about 4% of the cored interval. They are tightly cemented by carbonate and have a high (30%) clay matrix content. Low porosity (1.48%) and organic content (1.65%) offers little potential for gas productivity. Concretions (not illustrated) account for the remainder of the samples.

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Subject:
FRACTURES

6) Coarse, hackly vertical fracture from zone of gas production noted on temperature log. Radiating hackles have a maximum relief of 5 mm. Slickensided surfaces are evidence for slight vertical movement after initial fracturing. Such movement created highly permeable vugs which are only partially mineralized. This fracture type is interpreted as contributing significantly to the high final open flow (1007 MCF) of Jac 1369. Other examples were noted in a 20 foot interval and appeared to be unrelated to any specific lithotype. Specimen is from a core depth of 3720 feet. Width of core is 4 inches.

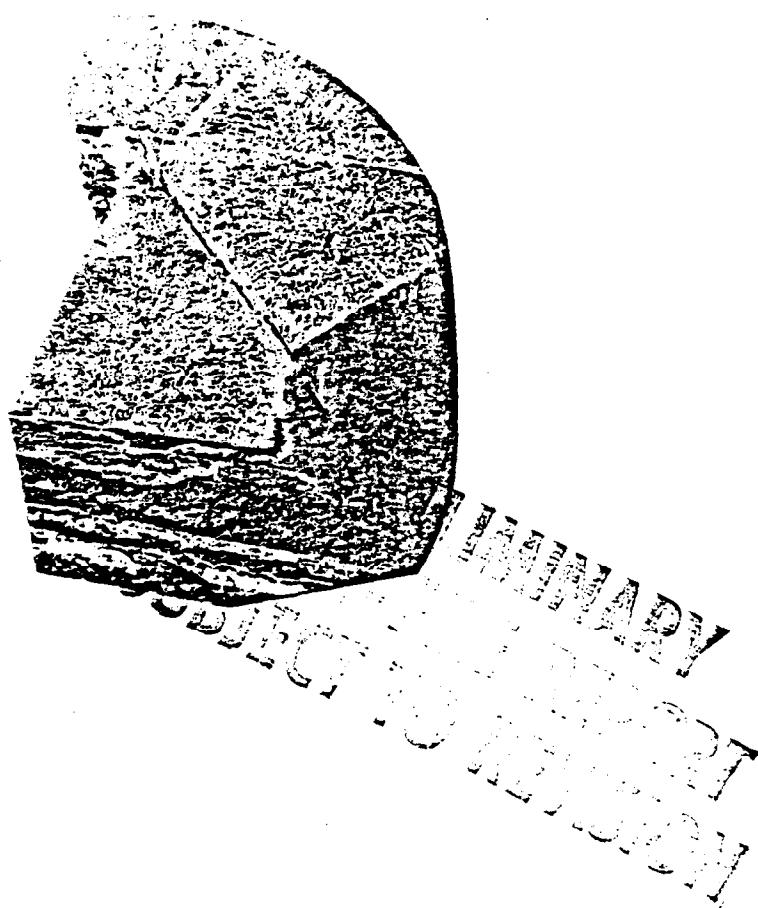
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W.Va. Geological & Economic Survey /27,

Substitutionary
Geology



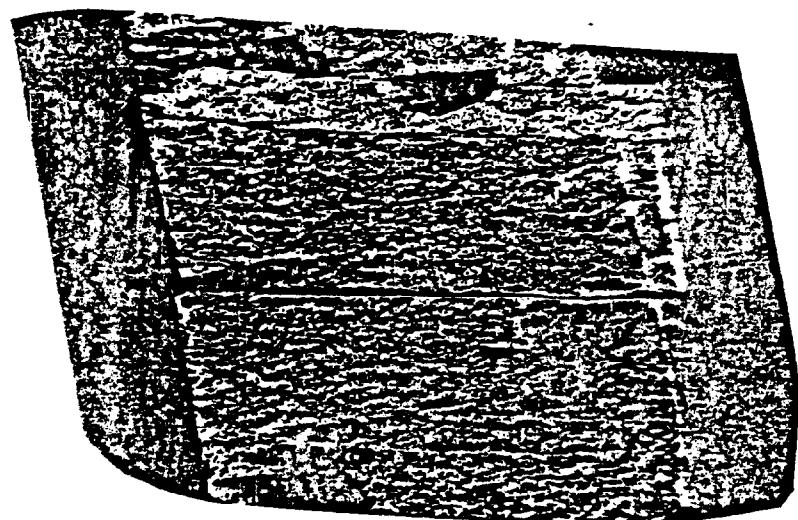
7) Cross fracture developed between two vertical, parallel, tightly mineralized fractures. Surface roughness of the cross fracture combined with slight offsetting created permeable vugs which were slightly infilled by carbonate. Examples of this fracture type were noted in the pay zone of Jac 1369 . Although the length of the fracture is a few centimeters (bounded by the filled vertical fractures) it may extend vertically ~~for~~ some distance. Specimen is from a core depth of 372⁴ feet. Width of core is 4 inches.

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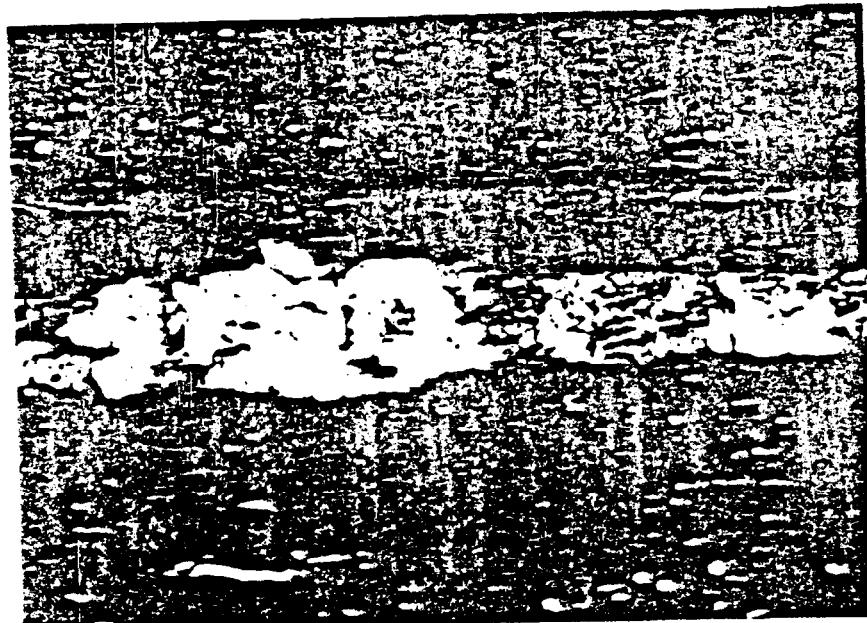
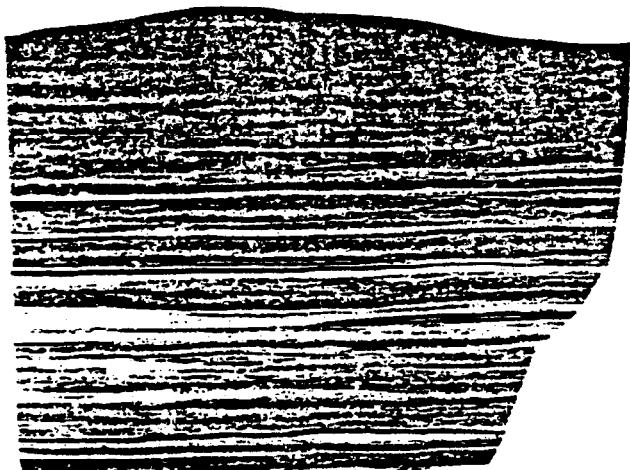
8) Vertical to sub-vertical smooth fracture that is tightly mineralized. The smoothness of the fracture prevents the development of vugs if slight offsetting occurs. Even though the fracture is tightly mineralized with little pore space present, permeability may be higher than that of the shale matrix. This fracture type is interpreted as being far less important in establishing the high production of Jac 4369 than the two previously described fracture types. Specimen is from a core depth of 3730 feet. Width of core is 4 inches.

Open
Subject
to
Review



9) Horizontal mineralized fractures as seen in radiograph print (5x). Fractures are very dark 1 mm thick discontinuous bands parallel to stratification. Accompanying photomicrograph shows tightly mineralized nature of fracture. These fractures are from an unproductive zone as indicated by the temperature log. The tight mineralization combined with a horizontal orientation prevents these fractures from draining gas out of an appreciable volume of the shale matrix. Specimen is from a core depth of 3739 feet.

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Preliminary
Edition



APPENDIX F
UNIVARIATE AND MULTIVARIATE ANALYSIS

ANOVA and MANOVA

Univariate analyses of variance (ANOVA: table 1) treats each variable in isolation; an important advantage in the use of multivariate analysis of variance (MANOVA) lies in the fact that all of the variables are treated simultaneously, and therefore error co-variation can be extracted from the data and between-group differences enhanced. Figure 1 of this section illustrates this fact. ANOVA for each of the variates 1 and 2 may show no significant difference between the two groups of points; note the close placement of the means and great overlap of the groups as projected on each axis. However, when the within-group covariance (i.e. "trend") is taken into account, and the points projected on an axis separating the mean in bivariate space, then group separability becomes obvious, and will in fact test as significant.

A second advantage lies in the fact that multivariate data sets commonly have more than two variables, and so a method that projects the sample coordinates onto a few axes allows one to visually assess group separability and study the relative positions of individual samples. MANOVA involves calculation of a set of "eigenvectors" (also called "canonical variates"), representing the axes separating the group means in a multivariate space. The first axis will provide the greatest separation, the second will provide the next greatest, and so forth. Given K groups, MANOVA will calculate a maximum of K-1 axes. The eigenvector representing each axis comprises a number of weighting coefficients, one for each variable, useful for evaluating the relative contribution of each variable

to the group differences along each axis. Matrix multiplication of the eigenvectors by the input data provides the projections of the samples on the axes for subsequent plotting.

Input to MANOVA includes specification of a model, that is, the classification variables that define group membership. For example, the lithologic types comprise a classification variable, and each sample is assigned to the appropriate group. MANOVA calculates a number of statistics, including measures of variance and covariance, and eigenvectors, and tests the null hypothesis that there exists no differences in group means, e.g. the model that the lithologic types show significant differences among lithologic types. One can call this a "lithologic effect".

RESULTS

Both classification variables lithologic type (Table 2) and core (Table 3), were found to be highly significant in the MANOVA. The eigenvectors - with entries for each variable multiplied by the square root of the within-groups error - give some indication of the differences between the two cores and among the three lithologic types. The first eigenvector accounts for 91.97% of the between-groups variation when testing the model's lithologic types. The major discriminators appear to be bulk density, sulfur, grain density, porosity, petrographic quartz, and illite, in descending order of importance (Table 4). Because only two cores comprise the data, the model testing for a core-effect yields a single eigenvector. Major differences between cores can be attributed to expandable-layer clays, porosity, log density, bulk density, and sulfur, in descending order.

Projection of the sample points on the axes calculated from the lithologic effect (Figure 2) shows good group separation despite overlap, with the banded samples intermediate to the finely laminated on the one hand, and the non-banded on the other. This relative placement of the lithologic types is consistent with visual appearance, as well as with interpretation of the post-depositional histories of the various lithologic types.

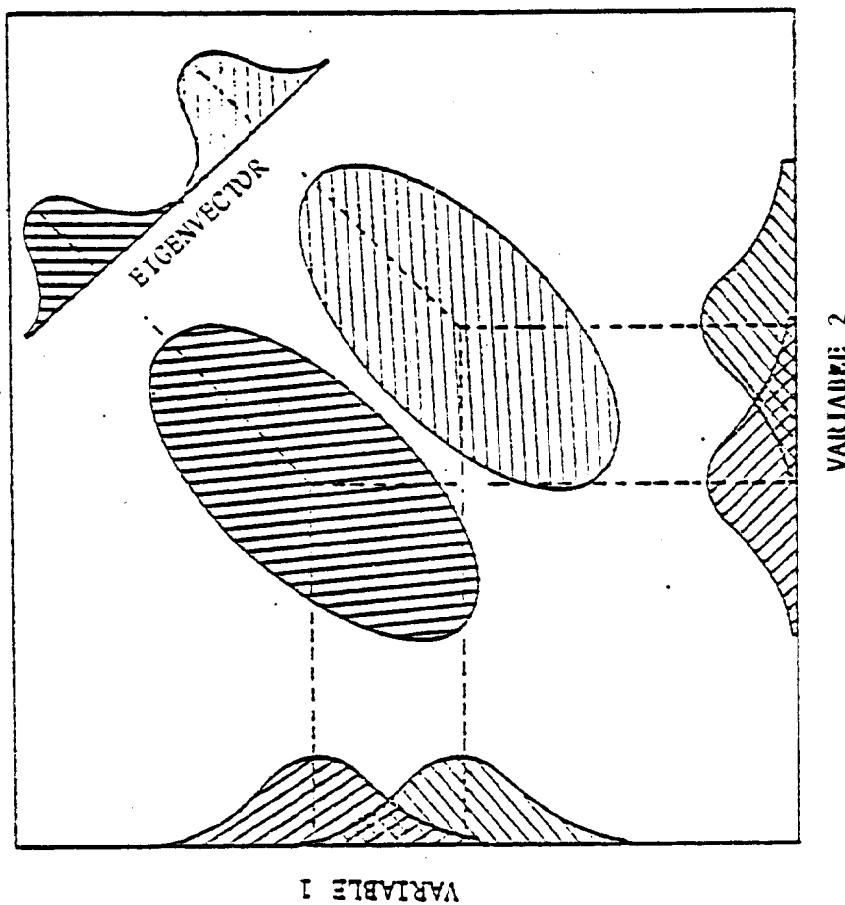


Figure 1. Pictorial example of hypothetical multivariate analysis of variance between two groups that overlap for each variable but show no overlap in multivariate space.

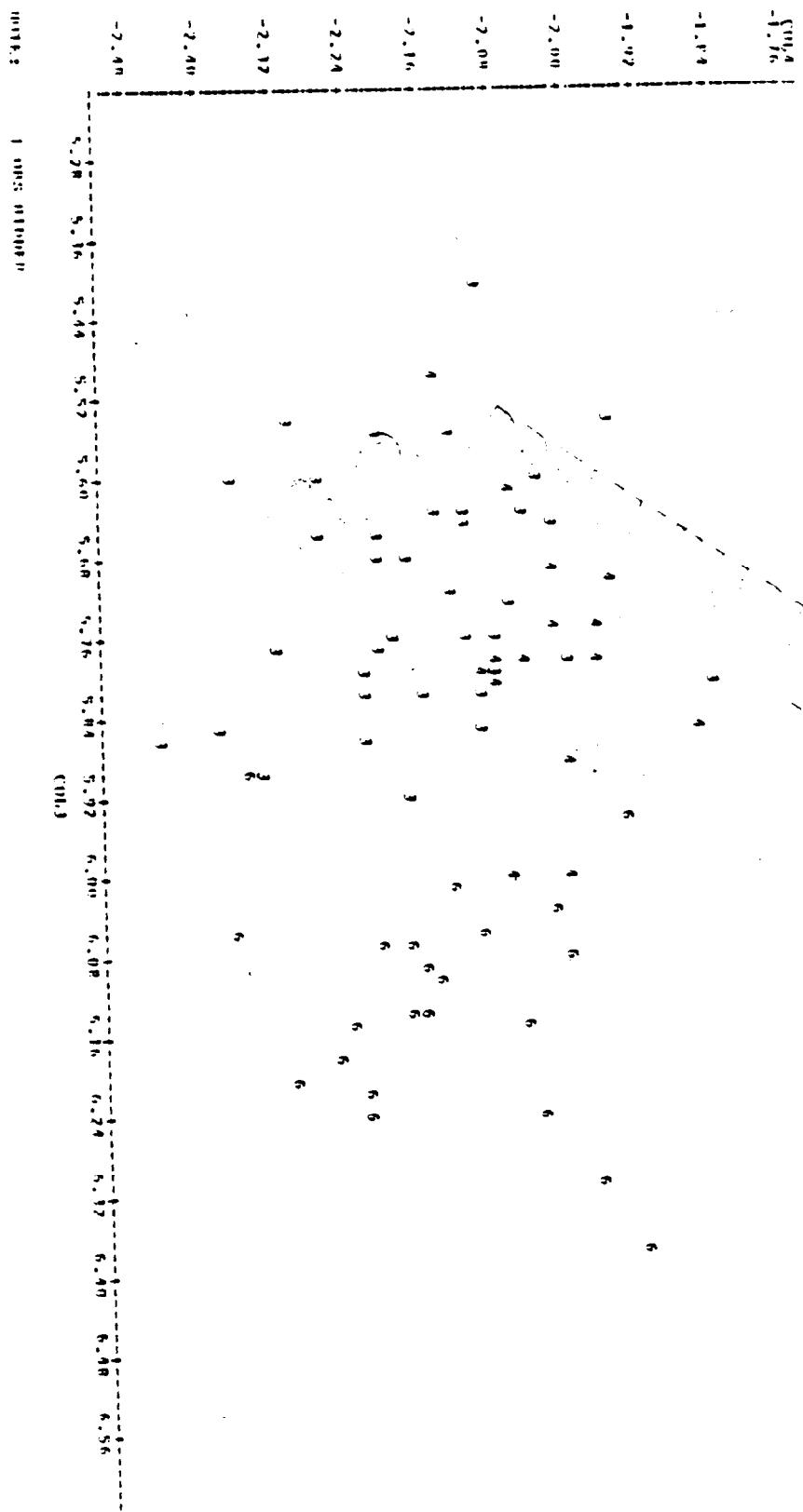


Figure 2. Scores of samples on eigenvectors calculated from lithologic effects model. 3 = finely laminated;

4 = banded; 6 = non-banded. First eigenvector is

horizontal axis ("COL,3") and second eigenvector is

vertical axis ("COL,4").

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GENERAL LINEAR MODELS PROCEDURE

DEPENDENT VARIABLE: LOSIG500	D.F.	SUM OF SQUARES	MEAN SQUARE	F VALUE	P>F	R-SQUARE	C.V.	
SOURCE	1	6.4043333	2.01479244	3.26	0.0260	0.121192	24.949	
ANSEL	3	46.4404267	0.63409046			1.0516500 MEAN		
FACTOR	71	52.9448000				1.24400000		
CORRECTED TOTAL	74					0.80875059		
SOURCE	D.F.	TYPE I SS	F VALUE	P>F	TYPE IV SS	F VALUE	P>F	
ANSEL	1	2.89665227	2.45	0.0235	1	1.53972406	1.93	0.1521
TYPE	2	1.55772406	5.56	0.0216				0.0216
Chart	1							

STATISTICAL ANALYSIS SYSTEM 11:04 FRIDAY, JANUARY 12, 1979 3
GENERAL LINEAR MODELS PROCEDURE

DEPENDENT VARIABLE: SULFOR	D.F.	SUM OF SQUARES	MEAN SQUARE	F VALUE	P>F	R-SQUARE	C.V.
SOURCE	1	15.71449655	5.23816552	4.91	0.0310	0.171076	47.1249
ANSEL	3	75.71357011	1.406639031			MEAN	
FACTOR	71	91.42866667				2.19103333	
CORRECTED TOTAL	74						
SOURCE	D.F.	TYPE I SS	F VALUE	P>F	TYPE IV SS	F VALUE	P>F
ANSEL	1	15.26822739	1.23	0.0311	18.14828937	1.11	0.0015
TYPE	2	0.24626935					
Chart	1						

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GENERAL LINEAR MODELS PROCEDURE

DEPENDENT VARIABLE: BULDEN	D.F.	SUM OF SQUARES	MEAN SQUARE	F VALUE	P>F	R-SQUARE	C.V.
SOURCE	1	0.29018699	0.09679566	3.51	0.001	0.517715	2.2755
ANSEL	3	0.24931167	0.083035394			MEAN	
FACTOR	71	0.54001067				2.6036667	
CORRECTED TOTAL	74						
SOURCE	D.F.	TYPE I SS	F VALUE	P>F	TYPE IV SS	F VALUE	P>F
ANSEL	1	0.24018699	0.09679566	3.51	0.001	0.24018699	11.41
TYPE	2	0.64122052	0.0905	0.0005	1	0.64122052	0.0005
Chart	1						

Table 1: Univariate analyses of variance of selected variables.

Type IV sums of squares and F-value gives significance of each effect when the other effect is partialled out.

STATISTICAL ANALYSIS SYSTEM
GENERAL LINEAR MODELS PROCEDURE

DEPENDENT VARIABLE: MATHDEN

SOURCE	DF	SUM OF SQUARES	MEAN SQUARE	F VALUE	PW > F	R-SQUARE	C.V.
MODEL	3	0.26189320	0.08729783	24.37	0.0001	0.507293	2.2561
ERROR	71	0.25437316	0.00358272			STD DEV	MATHDEN MEAN
CORRECTED TOTAL	74	0.51626667					2.65066667
						0.05945583	

STATISTICAL ANALYSIS SYSTEM
GENERAL LINEAR MODELS PROCEDURE

DEPENDENT VARIABLE: GAMMA

SOURCE	DF	SUM OF SQUARES	MEAN SQUARE	F VALUE	PW > F	R-SQUARE	C.V.
MODEL	3	50218.33472983	16746.11157662	6.04	0.0001	0.751665	17.4150
ERROR	71	147011.66527015	2081.85444042			STD DEV	GAMMA MEAN
CORRECTED TOTAL	74	198050.00000000				45.62714312	2622.00000000

STATISTICAL ANALYSIS SYSTEM
GENERAL LINEAR MODELS PROCEDURE

SOURCE	DF	SUM OF SQUARES	MEAN SQUARE	F VALUE	PW > F	R-SQUARE	C.V.
MODEL	3	0.29796130	0.09932043	16.79	0.0001	0.415081	14.6915
ERROR	71	0.41987818	0.00591378			STD DEV	BL. MEAN
CORRECTED TOTAL	74	0.71783949				0.790109	0.52347360

STATISTICAL ANALYSIS SYSTEM
GENERAL LINEAR MODELS PROCEDURE

SOURCE	DF	SUM OF SQUARES	MEAN SQUARE	F VALUE	PW > F	R-SQUARE	C.V.
MODEL	3	0.18256165	0.18256165	9.76	0.0002	0.16253165	1.78
ERROR	71	0.18256165	0.00263519	16.86	0.0001	0.16253165	0.0001
CORRECTED TOTAL	74	0.36512330					

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GENERAL LINEAR MODELS PROCEDURE

DEPENDENT VARIABLE: PHM	D.F.	SUM OF SQUARES	MEAN SQUARE	F VALUE	P>F	H-SQUARE	C.V.
SOURCE	3	0.0078170	0.00246057	6.09	0.0010	0.204606	145.7849
MODEL			0.00040417			STD DEV	NEW MEAN
ERROR	11	0.02869549				0.02010395	0.01379015
CORRECTED TOTAL	14	0.03667769					
SOURCE	DF	TYPE I SS	F VALUE	P>F	D.F.	TYPE IV SS	F VALUE
LTYPE	2	0.00294419	1.32	0.0349	2	0.00235773	3.6
CORR		0.00431152	11.23	0.0013	1	0.00433352	11.23

STATISTICAL ANALYSIS SYSTEM

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GENERAL LINEAR MODELS PROCEDURE

DEPENDENT VARIABLE: PHM	D.F.	SUM OF SQUARES	MEAN SQUARE	F VALUE	P>F	H-SQUARE	C.V.
SOURCE	3	0.01952449	0.00651003	7.07	0.0002	0.249478	51.5171
MODEL		0.05816095	0.00082762			STD DEV	PH MEAN
ERROR	11					0.02976037	0.05584237
CORRECTED TOTAL	14	0.07829344					
SOURCE	DF	TYPE I SS	F VALUE	P>F	D.F.	TYPE IV SS	F VALUE
LTYPE	2	0.01089621	5.25	0.0075	2	0.0059122	3.1
CORR		0.01081626	13.09	0.0006	1	0.01083626	13.09

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GENERAL LINEAR MODELS PROCEDURE

DEPENDENT VARIABLE: GROEN	D.F.	SUM OF SQUARES	MEAN SQUARE	F VALUE	P>F	H-SQUARE	C.V.
SOURCE	3	0.38904879	0.12964293	6.80	0.0005	0.221195	4.8190
MODEL		1.35404656	0.019001094			STD DEV	GROEN MEAN
ERROR	11					0.13009756	2.06569095
CORRECTED TOTAL	14	1.74404535					
SOURCE	DF	TYPE I SS	F VALUE	P>F	D.F.	TYPE IV SS	F VALUE
LTYPE	2	0.06687627	1.75	0.1606	2	0.03671251	1.04
CORR		0.322017251	16.89	0.0001	1	0.32217251	16.89

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GENERAL LINEAR MODELS PROCEDURE

DEPENDENT VARIABLE: EXP	DF	SUM OF SQUARES	MEAN SQUARE	F VALUE	FH > F	R-SQUARE	C.V.
SOURCE	3	0.00021168	0.00009256	17.23	0.0001	0.42145	21.0472
MODEL	3	0.00038851	0.00006537		STD DEV		EXP MEAN
ERROR	71	0.00055919					0.00851041
Corrected Total	74						
SOURCE	DF	TYPE I SS	F VALUE	*FH > F	TYPE IV SS	F VALUE	PW > F
MODEL	2	0.00006673	6.49	0.0029	1	0.0002469	2.30
ERROR	2	0.00020885	18.89	0.0001	1	0.00026895	19.49
Corr	1						0.0001

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GENERAL LINEAR MODELS PROCEDURE

DEPENDENT VARIABLE: QTZ	DF	SUM OF SQUARES	MEAN SQUARE	F VALUE	FH > F	R-SQUARE	C.V.
SOURCE	3	0.11874884	0.03958273	13.64	0.0001	0.365686	16.4457
MODEL	3	0.20597919	0.00290112		STD DEV		QTZ MEAN
ERROR	71	0.32472757					0.32751343
Corrected Total	74						
SOURCE	DF	TYPE I SS	F VALUE	*FH > F	TYPE IV SS	F VALUE	PW > F
MODEL	2	0.05352968	9.24	0.0003	1	0.02392396	4.13
ERROR	2	0.06515750	22.46	0.0001	1	0.06515750	22.46
Corr	1						0.0001

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GENERAL LINEAR MODELS PROCEDURE

DEPENDENT VARIABLE: PLA	DF	SUM OF SQUARES	MEAN SQUARE	F VALUE	FH > F	R-SQUARE	C.V.
SOURCE	3	0.0024583	0.00008194	1.24	0.3001	0.049921	31.0824
MODEL	3	0.00467858	0.00006590		STD DEV		PLA MEAN
ERROR	71	0.00492441					0.02611641
Corrected Total	74						
SOURCE	DF	TYPE I SS	F VALUE	*FH > F	TYPE IV SS	F VALUE	PW > F
MODEL	2	0.00017032	1.29	0.2810	1	0.00009965	0.76
ERROR	2	0.00067551	1.15	0.2860	1	0.00007551	1.15
Corr	1						0.2860

STATISTICAL ANALYSIS SYSTEM 1104 FRIDAY, JANUARY 12, 1979 14

GENERAL LINEAR MODELS PROCEDURE

DEPENDENT VARIABLE: LOSIG100		GENERAL LINEAR MODELS PROCEDURE					
SOURCE	DF	SUM OF SQUARES	MEAN SQUARE	F VALUE	P>F	R-SQUARE	C.V.
MODEL	3	131.11767724	43.70599241	5.56	0.009	0.190302	51.0152
ERROR	71	557.40010942	7.95746746			LOSIG100 MEAN	
CORRECTED TOTAL	74	688.99886667					5.49466667
SOURCE	DF	TYPE I SS	F VALUE	P>F	TYPE IV SS	F VALUE	P>F
TYPE	2	111.0974196	1.17	0.0014	105.50500476	6.71	0.0021
CORR	1	17.0193318	1.17	0.1155	105.01993319	2.17	0.1455

STATISTICAL ANALYSIS SYSTEM 1104 FRIDAY, JANUARY 12, 1979 15

GENERAL LINEAR MODELS PROCEDURE

DEPENDENT VARIABLE: POROSITY		GENERAL LINEAR MODELS PROCEDURE					
SOURCE	DF	SUM OF SQUARES	MEAN SQUARE	F VALUE	P>F	R-SQUARE	C.V.
MODEL	3	20.29123201	6.76441094	6.52	0.007	0.215946	36.4942
ERROR	71	73.68859919	1.01775492			POROSITY MEAN	
CORRECTED TOTAL	74	93.9793200				1.80120000	
SOURCE	DF	TYPE I SS	F VALUE	P>F	TYPE IV SS	F VALUE	P>F
TYPE	2	0.76889584	0.37	0.6666	1.172233230	0.84	0.4362
CORR	1	19.52113696	18.02	0.0001	1.172233230	18.83	0.0001

STATISTICAL ANALYSIS SYSTEM 1104 FRIDAY, JANUARY 12, 1979 16

GENERAL LINEAR MODELS PROCEDURE

DEPENDENT VARIABLE: QUANTZ		GENERAL LINEAR MODELS PROCEDURE					
SOURCE	DF	SUM OF SQUARES	MEAN SQUARE	F VALUE	P>F	R-SQUARE	C.V.
MODEL	3	0.02447141	0.00085714	4.40	0.009	0.156762	29.2037
ERROR	71	0.13161496	0.00185372			QUANTZ MEAN	
CORRECTED TOTAL	74	0.15600558				0.14742933	
SOURCE	DF	TYPE I SS	F VALUE	P>F	TYPE IV SS	F VALUE	P>F
TYPE	2	0.00617526	1.67	0.1964	0.0061626	0.98	0.3820
CORR	1	0.01829616	9.81	0.0025	0.01829616	9.87	0.4025

STATISTICAL ANALYSIS SYSTEM

11:04 FRIDAY, JANUARY 12, 1979 17

GENERAL LINEAR MODELS PROCEDURE

DEPENDENT VARIABLE LOG1EN	DF	SUM OF SQUARES	MEAN SQUARE	F VALUE	PR > F	PR-SQUARE	C.V.	
SOURCE	DF	SUM OF SQUARES	MEAN SQUARE	F VALUE	PR > F	PR-SQUARE	C.V.	
Model	3	0.11560310	0.03853437	1.318	0.0001	0.357674	2.1156	
ERROR	71	0.20760490	0.00292401		STD DEV	LOG1EN MEAN		
CORRECTED TOTAL	74	0.32320800			0.05401414	2.55840000		
SOURCE	DF	TYPE I SS	F VALUE	PR > F	PR	TYPE IV SS	F VALUE	PR > F
TYPE I	2	0.00632681	1.09	0.3439	1	0.00179492	0.3731	0.7364
TYPE II	1	0.10926429	1.37	0.0001		0.10926429		0.0001

Table 2: Multivariate analysis of variance on lithologic effect.

MANOVA TEST CRITERIA FOR THE HYPOTHESIS OF NO OVERALL LITHOLOGIC EFFECT

$H =$	TYPE IV SSCP MATRIX FROM LTYPE
$E =$	EXRON SSCP MATRIX
$P =$	NUMBER OF VARIABLES = 16
$Q =$	NUMBER OF H = 5
$N_E =$	DF OF E = 5
$S =$	$H^T W^{-1} H = 7.1$
$H =$	$154.8 (P-1) = 6.3$
$N =$	$.544E-P-1 = 27.6$

HOTELLING-LAWLEY TRACE = $T(H(E-1)) = 2.66571176$ (SEE PILLAI'S TABLE #1)
 F APPROXIMATION = $2(5N+1)T(H(E-1)) / (5S*(2M+S+1))$ WITH 5(2N+1) AND 2(SM+1) DF
 $F(32,110) = 4.58$ PROB > $F = 0.0001$

PILLAI'S TRACE $V = T(H \otimes I(N)(H)) = 0.00652756$ (SEE PILLAI'S TABLE #2)
 F APPROXIMATION = $(2N+S+1)/(2M+S+1) + V/(S-1)$
 $F(32,114) = 2.04$ PROB > $F = 0.0004$

WILKS' CRITERION $L = \det(E) / \det(H \otimes I(N)) = 0.21865007$ (SEE WILKS 1973 P 555)
 $EXACT F = (1-SORT(L)) / SORT(L) * (N(E-1)/P)$ WITH 2R AND 2(M+S+1) DF
 $F(32,112) = 3.66$ PROB > $F = 0.0001$

ROY'S MAXIMUM ROOT CRITERION = 2.45177547 (SEE AND VOL 31 P 625)
 FIRST CANONICAL VARIABLE YIELDS AN F UPPER BOUND
 $F(2,71) = 87.04$ (UPPER BOUND)

Table 3: Multivariate analysis of variance on core effect.

MANOVA TEST CRITERIA FOR THE HYPOTHESIS OF NO OVERALL CORE EFFECT

H = TYPE I X SSCP MATRIX FIRST CORE
E = ERROR X SSCP MATRIX
P = DEP. VARIABLES = 16
D = RANK OF H = 1
B = DF OF H = 15
S = RANK OF E = 7
N = 5 (ABOVE 0) = 7
n = .5(N-E-1) = 7.0

HOTELLING-LAWLEY TRACE = TRACE(1:NH) = 2.38485614 (SEE PILLAI'S TABLE #3)

F APPROXIMATION = 2(S+N+1)*TRACE(E+-1*N)/(S*S*(2N+S+1)) WITH 6(2N+S+1) AND 2(S+N+1) DF
 $F(16,56) = 0.15$ PROB > F = 0.0001

PILLAI'S TRACE V = TR(H*INV(H+E)) = 0.70456664 (SEE PILLAI'S TABLE #2)

F APPROXIMATION = (2N+S+1)*(2N+S+1) * V/(S-V) WITH 5(2N+S+1) AND 5(2N+S+1) DF
 $F(16,56) = 0.35$ PROB > F = 0.0001

WILKS' CRITERION L = DET(E)/DET(H+E) = 0.2954336 (SEE WAD 1973 P 555)
 EXACT F = (1-L)/(L*(N+E-P))/P WITH P AND N=0-P DF
 $F(16,56) = 0.15$ PROB > F = 0.0001

ROY'S MAXIMUM ROOT CRITERION = 2.38485614 (SEE AMS VOL 31 P 625)
 FIRST CANONICAL VARIABLE YIELDS AN F UPPER BOUND
 $F(1,71) = 169.12$ (UPPER BOUND)

RECORDED BY [Signature]

Table 4: Eigenvectors from MANCOVA of the hypothesis of core and lithologic effects.

Effect	'Litype'		"Core"
Eigenvector #	I	II	I
LOSIG500	-0.119	0.476	-0.315
Sulfur	-0.670	0.304	0.428
Bulkden	1.256	-0.118	-0.510
Matrxden	-0.099	-0.330	0.365
Gamma	0.040	-0.005	0.088
III	0.423	0.397	-0.033
Hem	-0.128	0.119	-0.168
Pyr	-0.352	-0.183	0.084
Grden	0.563	0.512	0.281
Exp	-0.246	-0.204	0.747
Qtz	0.436	-0.394	-0.210
Pla	0.087	0.670	-0.195
LOSIG100	-0.257	-0.656	0.367
Porosity	0.557	0.303	-0.674
Quartz	0.040	0.137	-0.255
Logden	-0.345	-0.240	0.586
Percent Variance	91.97	8.03	100.0

Multiple Range Test

Analysis of variance (ANOVA) shows that differences exist by lithotype and/or well for certain mineralogic and physical parameters. When such differences are indicated, the multiple range test can be used to group the means into subgroups of not significantly distinguishable means. The program utilized contained Kramer's extension which corrected for unequal population size. The lower Huron interval in Jac 1369 was compared to the lower Huron interval in Linc 1637 on the basis of lithotypes for selected parameters (Table 1). All means that fall within the same grouping are not significantly different.

Among mineralogic parameters, less total quartz and silt is present in the thinly laminated and lenticularly laminated lithotypes in Jac 1369. More illite is present in all lithotypes in Jac 1369 paralleling the decrease in quartz. The higher clay content is consistent with a postulated deep water environment for the lower Huron in Jackson County. Additionally, less pyrite occurs in the thinly laminated and non-banded lithotypes in Jac 1369. The lower pyrite content along with the lower quartz content may explain the lower mean porosity of Jac 1369. Bulk density, matrix density, and log density are higher in the thinly laminated and lenticularly laminated lithotypes in Jac 1369, probably reflecting the lower porosity and overall lower mean organic matter content. Expandable clay (14°A clay on diffractogram) is significantly higher in Jac 1369, but the amount of this clay is so low, generally 1% or less, that differences may be due to individual bias in interpreting diffractograms or slight matrix differences between

wells.

RECEIVED
SUBMITTED
MAY 1968

STATISTICAL ANALYSIS SYSTEM
DUNCAN'S MULTIPLE RANGE TEST FOR VARIABLE BULKDEN

12:00 MONDAY, JANUARY 15, 1979

MEANS WITH SAME LETTER ARE NOT SIGNIFICANTLY DIFFERENT.

ALPHA LEVEL=0.05

D.F.=71

M.S.=0.654

GROUPING

GROUPING	MEAN	N	LITHOTYPE	CORE
A	1.500000	25	3	12
A	3.400000	4	4	12
B	3.450000	12	6	12
B	3.215395	13	4	21
B	3.190909	11	4	21
B	2.490000	10	6	21
C				

STATISTICAL ANALYSIS SYSTEM
DUNCAN'S MULTIPLE RANGE TEST FOR VARIABLE SULFUR

12:00 MONDAY, JANUARY 15, 1979

MEANS WITH SAME LETTER ARE NOT SIGNIFICANTLY DIFFERENT.

ALPHA LEVEL=0.05

D.F.=71

M.S.=1.066

GROUPING

GROUPING	MEAN	N	LITHOTYPE	CORE
A	2.560400	25	3	12
A	2.519231	13	1	21
B	2.419091	11	4	21
B	1.990000	4	4	12
B	1.746667	12	6	12
B	1.206000	10	6	21
C				

STATISTICAL ANALYSIS SYSTEM
DUNCAN'S MULTIPLE RANGE TEST FOR VARIABLE RULDEN

12:00 MONDAY, JANUARY 15, 1979

MEANS WITH SAME LETTER ARE NOT SIGNIFICANTLY DIFFERENT.

ALPHA LEVEL=0.05

D.F.=71

M.S.=0.00152

GROUPING

GROUPING	MEAN	N	LITHOTYPE	CORE
A	2.706000	10	6	21
A	2.695433	12	6	12
B	2.625455	10	4	21
B	2.596154	13	3	21
B	2.542900	25	1	12
C	2.502500	4	4	12

Table 1. Results of multiple range test for selected parameters. Lithotype code 1s: 3-thin ~~shale~~ laminated shale, 4-lenticularly laminated shale, 6-non-banded shale. Core code 1s: 12-

STATISTICAL ANALYSIS SYSTEM
DUNCAN'S MULTIPLE RANGE TEST FOR VARIABLE KATHADIN

MEANS WITH THE SAME LETTER ARE NOT SIGNIFICANTLY DIFFERENT.

ALPHA LEVEL=.05

DF=71

MS=0.00358

GROUPING	MEAN	n	LATICE	CORE
A	2.746667	12	6	12
A	2.727000	10	6	21
B	2.663636	11	4	21
B	2.629231	13	3	21
C	2.592400	25	3	12
C	2.576600	4	4	12
C	2.576600	10	6	21

STATISTICAL ANALYSIS SYSTEM
DUNCAN'S MULTIPLE RANGE TEST FOR VARIABLE GAMMA

MEANS WITH THE SAME LETTER ARE NOT SIGNIFICANTLY DIFFERENT.

ALPHA LEVEL=.05

DF=71

MS=2.081185

GROUPING	MEAN	n	LATICE	CORE
A	297.916667	12	6	12
A	284.800000	25	3	21
B	252.727273	11	4	12
B	251.250000	4	4	12
B	237.107692	13	3	21
C	208.500000	10	6	21

STATISTICAL ANALYSIS SYSTEM
DUNCAN'S MULTIPLE RANGE TEST FOR VARIABLE ILG

MEANS WITH THE SAME LETTER ARE NOT SIGNIFICANTLY DIFFERENT.

ALPHA LEVEL=.05

DF=71

MS=0.00591

GROUPING	MEAN	n	LATICE	CORE
A	0.612216	11	4	21
A	0.582244	10	6	21
B	0.539102	13	3	21
B	0.539102	12	6	12
C	0.50514	4	4	12
C	0.445552	15	1	12

STATISTICAL ANALYSIS SYSTEM
DUNCAN'S MULTIPLE RANGE TEST FOR VARIABLE DEM

MEANS WITH THE SAME LETTER ARE NOT SIGNIFICANTLY DIFFERENT.

ALPHA LEVEL=.05 DF=71

$MS=4.0E-04$

GROUPING	MEAN	n	LTYPE	CORE
A	0.037919	12	6	12
A	0.017894	4	4	12
B	0.013022	25	3	12
B	0.005730	13	3	21
B	0.005634	10	6	21
B	0.004653	11	4	21

STATISTICAL ANALYSIS SYSTEM
DUNCAN'S MULTIPLE RANGE TEST FOR VARIABLE PTH

MEANS WITH THE SAME LETTER ARE NOT SIGNIFICANTLY DIFFERENT.

ALPHA LEVEL=.05 DF=71

$MS=0.3E-04$

GROUPING	MEAN	n	LTYPE	CORE
A	0.071559	25	3	12
A	0.060471	12	6	12
B	0.060296	4	4	12
B	0.052806	13	3	21
B	0.040312	11	4	21
B	0.025178	10	6	21

STATISTICAL ANALYSIS SYSTEM
DUNCAN'S MULTIPLE RANGE TEST FOR VARIABLE PTHN

MEANS WITH THE SAME LETTER ARE NOT SIGNIFICANTLY DIFFERENT.

ALPHA LEVEL=.05 DF=71

$MS=0.9191$

GROUPING	MEAN	n	LTYPE	CORE
A	3.011552	12	6	12
A	2.891531	25	3	12
B	2.891981	4	4	12
B	2.842151	13	3	21
B	2.702921	11	4	21
B	2.761490	10	6	21

STATISTICAL ANALYSIS SYSTEM 12:00 MONDAY, JANUARY 15, 1979 10
 DUNCAN'S MULTIPLE RANGE TEST FOR VARIABLE EXP

MEANS WITH THE SAME LETTER ARE NOT SIGNIFICANTLY DIFFERENT.

ALPHA LEVEL=.05 DF=71 MS=5.4E-06

GROUPING	MEAN	N	LTYPE	CURE
A	0.010809	10	6	21
A	0.010664	11	4	21
A	0.010352	13	3	21
B	0.008437	12	6	12
B	0.007379	4	4	12
C	0.006276	25	3	12

STATISTICAL ANALYSIS SYSTEM 12:00 MONDAY, JANUARY 15, 1979 11
 DUNCAN'S MULTIPLE RANGE TEST FOR VARIABLE OTZ

MEANS WITH THE SAME LETTER ARE NOT SIGNIFICANTLY DIFFERENT.

ALPHA LEVEL=.05 DF=71 MS=0.0029

GROUPING	MEAN	N	LTYPE	CURE
A	0.376141	3	12	
B	0.354205	4	12	
B	0.327923	12	6	12
B	0.306824	4	12	21
B	0.293445	10	4	21
C	0.262215	4	4	21

STATISTICAL ANALYSIS SYSTEM 12:00 MONDAY, JANUARY 15, 1979 12
 DUNCAN'S MULTIPLE RANGE TEST FOR VARIABLE PLA

MEANS WITH THE SAME LETTER ARE NOT SIGNIFICANTLY DIFFERENT.

ALPHA LEVEL=.05 DF=51 MS=6.6E-05

GROUPING	MEAN	N	LTYPE	CURE
A	0.030943	11	4	21
A	0.029347	10	6	21
A	0.028450	25	3	12
A	0.025491	4	4	12
B	0.023966	13	3	21
B	0.022342	12	6	12

STATISTICAL ANALYSIS SYSTEM
DUNCAN'S MULTIPLE RANGE TEST FOR VARIABLE GOSIG160

12:00 MONDAY, JANUARY 15, 1979 13

MEANS WITH THE SAME LETTER ARE NOT SIGNIFICANTLY DIFFERENT.

ALPHA LEVEL=.05 DF=7 MS=7.857

GROUPING	MEAN	N	LTYPE	CORE
A	6.964000	25	3	12
A	6.100000	4	4	12
B	5.784615	13	3	21
B	5.109091	11	4	21
B	3.983333	12	6	12
B	3.360000	10	6	21

STATISTICAL ANALYSIS SYSTEM
DUNCAN'S MULTIPLE RANGE TEST FOR VARIABLE POROSITY

12:00 MONDAY, JANUARY 15, 1979 14

MEANS WITH THE SAME LETTER ARE NOT SIGNIFICANTLY DIFFERENT.

ALPHA LEVEL=.05 DF=7 MS=1.0378

GROUPING	MEAN	N	LTYPE	CORE
A	2.645000	4	12	12
A	2.249600	25	3	12
A	2.212500	14	4	12
A	1.504545	11	3	21
B	1.255385	13	6	21
B	0.987090	10	6	21

STATISTICAL ANALYSIS SYSTEM
DUNCAN'S MULTIPLE RANGE TEST FOR VARIABLE SURFACE

12:00 MONDAY, JANUARY 15, 1979 15

MEANS WITH THE SAME LETTER ARE NOT SIGNIFICANTLY DIFFERENT.

ALPHA LEVEL=.05 DF=7 MS=6.00095

GROUPING	MEAN	N	LTYPE	CORE
A	0.171944	25	3	12
A	0.170200	4	4	12
B	0.140550	12	6	12
B	0.132000	10	6	21
B	0.130000	11	4	21
B	0.126154	13	3	21

STATISTICAL ANALYSIS SYSTEM 12:00 MONDAY, JANUARY 15, 1979 16

BONNER'S MULTIPLE RANGE TEST FOR VARIABLE LOGDFH

MEANS WITH THE SAME LETTER ARE NOT SIGNIFICANTLY DIFFERENT.

ALPHA LEVEL=.05 DF=71 MS=0.00292

COMPUTER RUN	MEAN	N	LTYPE	CORE
A	2.629000	10	6	24
A	2.594545	11	4	21
A	2.585185	13	3	21
B	2.511200	25	1	12
B	2.510000	4	4	12
B	2.510000	12	6	12

SUBJECT TO PRELIMINARY
 AND UNAUDITED REPORT

Kolmogorov-Smirnov Test

In comparing means or variances, some properties of the distribution must be known to select the appropriate statistical test. Testing for normality can be quickly accomplished and should be done before comparing data from different lithotypes or wells. The Kolmogorov-Smirnov one sample test for normality compares the sample distribution to a hypothetical normal distribution. Results for the lower Huron interval by lithotype for Linc 1637 and Jac 1369 are given in table I. Generally, most parameters are normally distributed indicating that parametric statistical tests such as the multiple range test are generally applicable to the data. Log density and bulk density commonly show a non-normal distribution indicating that a two sample non-parametric goodness of fit test should probably be used for these parameters. Further research on the shape of sample populations by lithotype and core is in progress.

STATISTICAL ANALYSIS CONE=12 SYSTEM

VARIABLE	N	0-MAX	PROB	SKEWNESS	G1/SERG1	P-LEVEL	KURTOSIS	G2/SERG2	P-LEVEL	MEAN	ST DEV
LOSIG500	25	0.1098	>.20	0.148	0.320	0.719	0.084	0.093	0.926	3.080	0.475
SULFUR	25	0.1554	>.20	0.589	0.230	0.004	0.212	0.193	0.193	2.664	0.679
BULKDEN	25	0.1554	>.20	0.603	0.230	0.004	0.212	0.193	0.193	2.628	0.671
MATHXDEN	25	0.1554	>.20	0.985	-0.001	0.000	0.000	0.000	0.000	2.924	0.671
GAMMA	25	0.1554	>.20	0.203	-0.001	0.000	0.000	0.000	0.000	2.914	0.671
LIL	25	0.1554	>.20	0.203	-0.001	0.000	0.000	0.000	0.000	2.914	0.671
EXP	25	0.1554	>.20	0.444	-0.001	0.000	0.000	0.000	0.000	2.914	0.671
GRDN	25	0.1554	>.20	0.237	-0.001	0.000	0.000	0.000	0.000	2.914	0.671
EXP	25	0.1554	>.20	0.597	0.524	0.000	0.000	0.000	0.000	2.914	0.671
OTZ	25	0.1554	>.20	0.106	0.237	0.000	0.000	0.000	0.000	2.914	0.671
PLA	25	0.1554	>.20	0.633	-0.001	0.000	0.000	0.000	0.000	2.914	0.671
LOSIG100	25	0.1554	>.20	0.861	-0.001	0.000	0.000	0.000	0.000	2.914	0.671
QUARTZ	25	0.1554	>.20	0.986	-0.001	0.000	0.000	0.000	0.000	2.914	0.671
LOGDEN	25	0.1554	>.20	0.144	-0.001	0.000	0.000	0.000	0.000	2.914	0.671

STATISTICAL ANALYSIS CONE=12 SYSTEM

VARIABLE	N	0-MAX	PROB	SKEWNESS	G1/SERG1	P-LEVEL	KURTOSIS	G2/SERG2	P-LEVEL	MEAN	ST DEV
LOSIG500	12	0.1678	>.20	0.186	0.102	0.763	0.709	0.588	0.193	2.514	0.462
SULFUR	12	0.1678	>.20	0.260	-0.260	0.423	-0.551	-0.302	0.193	2.519	0.462
BULKDEN	12	0.1678	>.20	0.129	-0.210	0.789	-0.421	-0.320	0.193	2.562	0.468
MATHXDEN	12	0.1678	>.20	0.556	-0.064	0.814	-0.104	-0.320	0.193	2.529	0.468
GAMMA	12	0.1678	>.20	0.144	-0.654	0.289	-0.104	-0.320	0.193	2.519	0.468
LIL	12	0.1678	>.20	0.150	-0.695	0.990	-0.104	-0.320	0.193	2.519	0.468
HIL	12	0.1678	>.20	0.159	-0.695	0.990	-0.104	-0.320	0.193	2.519	0.468
YIL	12	0.1678	>.20	0.154	-0.695	0.990	-0.104	-0.320	0.193	2.519	0.468
GABE	12	0.1678	>.20	0.222	-0.001	0.222	-0.421	-0.318	0.193	2.512	0.465
EXP	12	0.1678	>.20	0.643	-0.001	0.562	-0.293	-0.318	0.193	2.512	0.465
OTZ	12	0.1678	>.20	0.747	-0.001	0.524	-0.293	-0.318	0.193	2.512	0.465
PLA	12	0.1678	>.20	0.442	-0.001	0.762	-0.446	-0.318	0.193	2.512	0.465
LOSIG100	12	0.1678	>.20	0.244	-0.001	0.442	-0.241	-0.318	0.193	2.512	0.465
QUARTZ	12	0.1678	>.20	0.642	-0.001	0.964	-0.462	-0.318	0.193	2.512	0.465
LOGDEN	12	0.1678	>.20	0.153	-0.001	0.862	-0.195	-0.318	0.193	2.512	0.465

STATISTICAL ANALYSIS CONE=12 SYSTEM

VARIABLE	N	0-MAX	PROB	SKEWNESS	G1/SERG1	P-LEVEL	KURTOSIS	G2/SERG2	P-LEVEL	MEAN	ST DEV
LOSIG500	12	0.1646	>.05	0.232	-0.001	0.052	0.141	0.452	0.152	4.000	0.416
SULFUR	12	0.1646	>.05	0.294	-0.412	0.589	-0.616	0.532	0.152	3.909	0.407
BULKDEN	12	0.1646	>.05	0.284	-0.412	0.589	-0.616	0.532	0.152	3.925	0.407
MATHXDEN	12	0.1646	>.05	0.273	-0.719	0.754	-0.777	0.532	0.152	3.970	0.407
GAMMA	12	0.1646	>.05	0.199	-0.194	0.205	-0.239	0.435	0.152	3.500	0.407
LIL	12	0.1646	>.05	0.199	-0.924	0.924	-0.059	0.435	0.152	3.095	0.407
HIL	12	0.1646	>.05	0.199	-0.924	0.924	-0.059	0.435	0.152	3.095	0.407
YIL	12	0.1646	>.05	0.199	-0.924	0.924	-0.059	0.435	0.152	3.095	0.407
GABE	12	0.1646	>.05	0.227	-0.495	0.184	-0.468	0.626	0.152	4.000	0.416
EXP	12	0.1646	>.05	0.273	-0.493	0.462	-0.622	0.532	0.152	3.974	0.407
OTZ	12	0.1646	>.05	0.244	-0.493	0.462	-0.622	0.532	0.152	3.542	0.407
PLA	12	0.1646	>.05	0.199	-0.153	0.153	-0.479	0.435	0.152	3.055	0.407
LOSIG100	12	0.1646	>.05	0.199	-0.467	0.467	-0.493	0.435	0.152	3.499	0.407
QUARTZ	12	0.1646	>.05	0.199	-0.595	0.595	-0.697	0.435	0.152	4.000	0.416
LOGDEN	12	0.1646	>.05	0.199	-0.215	0.215	-0.212	0.354	0.152	4.000	0.416

Table 1. Results of Kolmogorov-Smirnov one sample test for normality on selected parameters in Jac 1369 and Line 1637 for the Lower Huron interval by 11th-type. Lithotype code 1s; 3 - thinly laminated shale, 4 - laminated shale, 6 - non-banded shale. Core code 1s; 12 - Line 1637
21 - Jac 1369.

STATISTICAL ANALYSIS SYSTEM CURE=21

9:12 TUESDAY, JANUARY 16, 1979

VARIABLE	μ	D-MAX	PROB	SKWNESS	G1/SENG1	P-LEVEL	KURTOSIS	G2/StRG2	P-LEVEL	MEAN	ST DEV
LOSIG500	0.1524	>.20	-0.391	-0.376	0.565	0.067	0.052	0.558	0.009	2.419	0.1013
SULFUR2	0.1066	>.01	-0.251	-0.024	0.058	0.690	0.017	0.017	0.017	2.625	0.581
HULKORN	0.1492	>.20	-0.442	-0.219	0.665	0.463	0.362	0.655	0.055	2.663	0.0692
MATRIXDN	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0570
GAMMA	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0530
ILL	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0545
HEM	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0545
PTK	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0545
GRDEN	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0545
EXP	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0545
OTZ	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0545
PLA	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0545
LOSIG500	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0545
QUARTZ	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0545
LOGDEN	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0545

STATISTICAL ANALYSIS SYSTEM CURE=12

9:12 TUESDAY, JANUARY 16, 1979

VARIABLE	μ	D-MAX	PROB	SKWNESS	G1/SENG1	P-LEVEL	KURTOSIS	G2/StRG2	P-LEVEL	MEAN	ST DEV
LOSIG500	0.1524	>.20	-0.391	-0.376	0.565	0.067	0.052	0.558	0.009	2.419	0.1013
SULFUR2	0.1066	>.01	-0.251	-0.024	0.058	0.690	0.017	0.017	0.017	2.625	0.581
HULKORN	0.1492	>.20	-0.442	-0.219	0.665	0.454	0.419	0.419	0.021	2.727	0.0570
MATRIXDN	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0530
GAMMA	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0545
ILL	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0545
HEM	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0545
PTK	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0545
EXP	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0545
OTZ	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0545
PLA	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0545
LOSIG500	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0545
QUARTZ	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0545
LOGDEN	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0545

STATISTICAL ANALYSIS SYSTEM CURE=21

9:12 TUESDAY, JANUARY 16, 1979

VARIABLE	μ	D-MAX	PROB	SKWNESS	G1/SENG1	P-LEVEL	KURTOSIS	G2/StRG2	P-LEVEL	MEAN	ST DEV
LOSIG500	0.1524	>.20	-0.391	-0.376	0.565	0.067	0.052	0.558	0.009	2.419	0.1013
SULFUR2	0.1066	>.01	-0.251	-0.024	0.058	0.690	0.017	0.017	0.017	2.625	0.581
HULKORN	0.1492	>.20	-0.442	-0.219	0.665	0.454	0.419	0.419	0.021	2.727	0.0570
MATRIXDN	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0530
GAMMA	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0545
ILL	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0545
HEM	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0545
PTK	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0545
EXP	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0545
OTZ	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0545
PLA	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0545
LOSIG500	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0545
QUARTZ	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0545
LOGDEN	0.1492	>.20	-0.442	-0.219	0.664	0.454	0.419	0.419	0.021	2.727	0.0545

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Summary of Contractural Fulfillment

<u>Parameter</u>	<u>Required by Contract</u>	<u>Fulfilled</u>
Thin Section Mineralogy	Yes	Yes
X-Ray Diffraction Mineralogy	Yes	Yes
Texture-fabric from thin sections	Yes	Yes
Texture-fabric from X-radiography	No	Yes
Electron Microscopy of selected samples	Yes	Yes
Organic Matter from LOI	No	Yes
Bulk Density	Yes	Yes
Matrix Density	No	Yes
Porosity Measurement	No	Yes
Material Balance Density	No	Yes
Correlation Analyses Whole Well	Yes	Yes
Correlation Analyses by Lithotype	No	Yes
Strip Log Presentations	Yes	Yes
Relate petrology to log data	(major parameters) Yes	(all parameters) Yes
Multivariate Analysis	No	Yes

Contributors by Alphabetical Order

J.L. Clagett - Preparation of radiographs, staining of thin sections, photography.

J.E. Florence - Initial sample preparation, thin-slabbing of shales for X-radiography, preparation of archive material.

M.E. Hohn - Computer generation of strip log profiles; linear correlation analyses; multivariate analysis.

R.E. Larese - Sample selection, initiation of study.

D.W. Neal - Stratigraphy

E.B. Nuhfer - Design of investigation; methodology, fabric classification of lithotypes by X-radiography and thin section prints, X-ray diffraction study, density and porosity evaluation, scanning electron microscopy, log analysis, petrographic interpretation of correlation analyses, organization of data, summary and interpretation, conclusions and recommendations, organization of report, photography.

J.J. Renton - X-ray diffraction analyses.

R.A. Smosna - Coordination and supervision.

R.J. Vinopal - Thin section point count analyses, fabric classification of lithotypes from X-radiography, thin section prints, and thin sections, density-porosity evaluation, loss on ignition determinations, density-porosity measurements, organization of data, petrographic interpretation of correlation analyses, conclusions and recommendations, organization of report, sample selection.